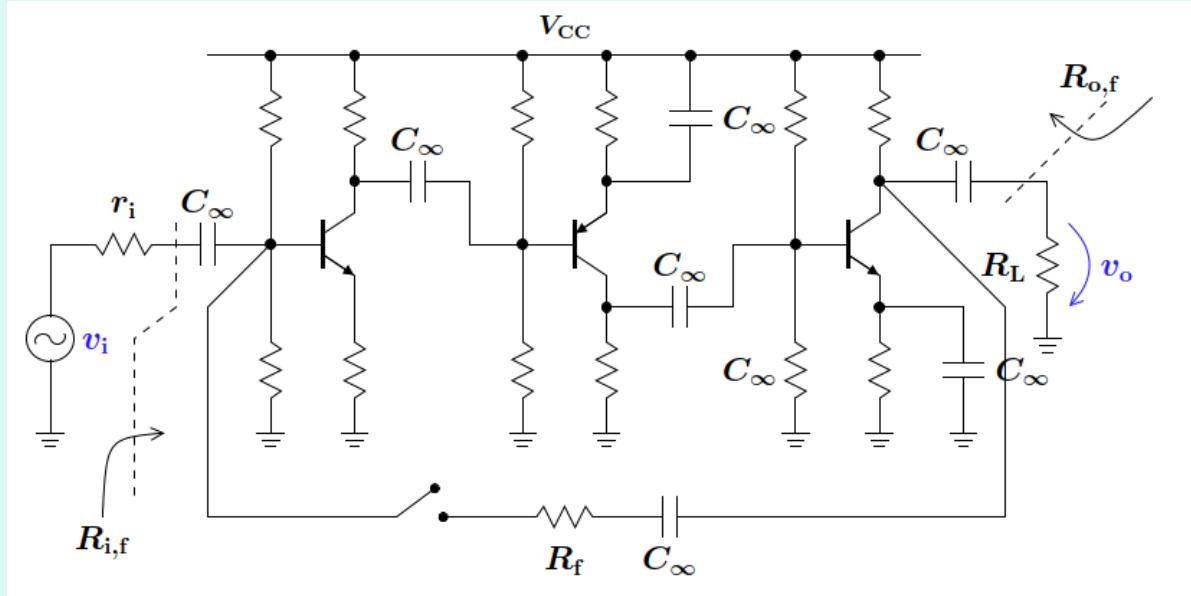
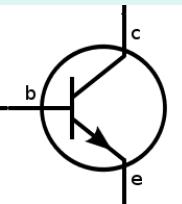


# ELEC 301 - Electronic Circuits

L04 - Sep 11

Instructor: Edmond Cretu

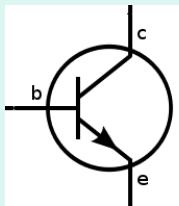




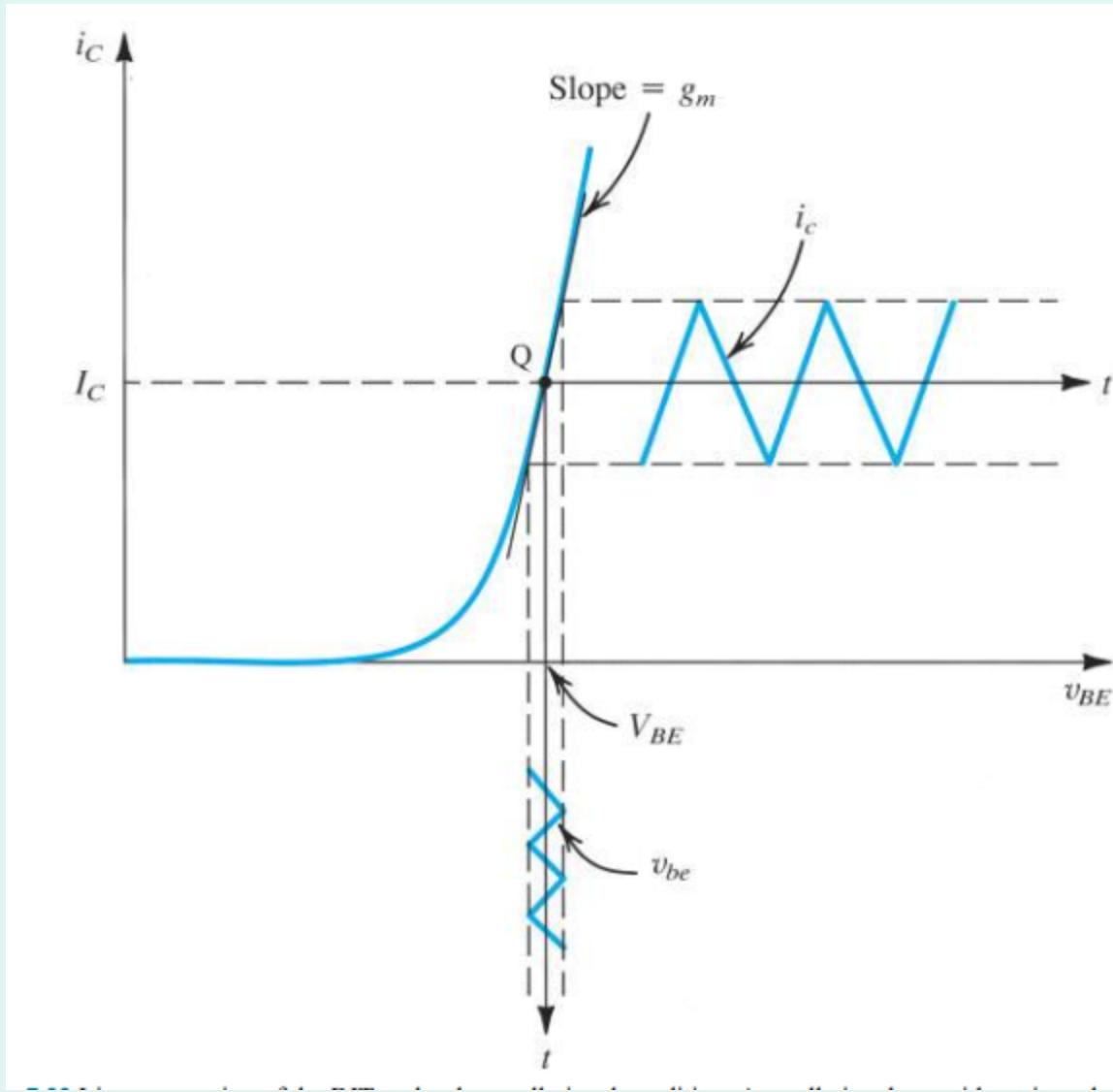
# Last time

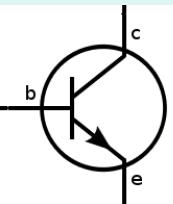
- Trends and design strategy: PCB vs. ASIC
- Amplification principles: diports, nonlinear device transfer characteristics
- Energy transfer from DC (power supply) to signal energy





# Amplification





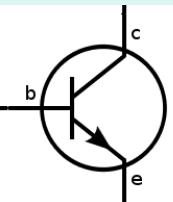
# Amplification principle

- We need separate input output ports
- Energy is transferred from DC (battery) to signal through the inherent nonlinearity of the device
- **Question:** is this the best we can do? DC levels are very prone to noise
- Comparison BJT vs MOSFET:

$$i_C(t) = I_S e^{v_{BE}/V_T} \Rightarrow i_C \approx \underbrace{I_S e^{V_{BE}/V_T}}_{I_{C0}} + \underbrace{\frac{I_S e^{V_{BE}/V_T}}{V_T} v_{be}(t)}_{g_m = I_{C0}/V_T}$$

$$i_D(t) = \frac{1}{2} k' \frac{W}{L} (v_{GS}(t) - V_T)^2 \approx \underbrace{\frac{1}{2} k' \frac{W}{L} (V_{GS} - V_T)^2}_{I_{D0}} + \underbrace{k' \frac{W}{L} (V_{GS} - V_T) \cdot v_{gs}(t)}_{g_m}$$

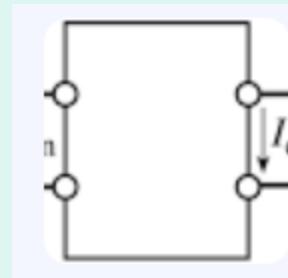




# BJT vs. MOSFET

## BJT

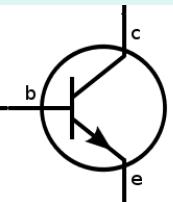
- Transconductance  $g_m = 1..400\text{mS}$  (exponential relation  $i_c - v_{be}$ ) (40mS for  $I_C = 1\text{uA}$ , 385mS for  $I_C = 10\text{mA}$ ), linear dependence on  $I_C$
- **higher gain applications in discrete circuits**
- higher output power than MOS
- HF performance  $f_T > 300\text{GHz}$
- lower low-frequency noise than MOS



## MOSFET

- Transconductance  $gm = 10\mu\text{S}...30\text{mS}$ , Square-root dependency on  $I_D$
- higher input impedance than BJT
- better geometric control (W/L), more predictable performance
- $f_T > 200\text{GHz}$  for <20nm technologies
- higher 1/f noise (surface effects)

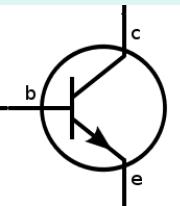




# Problems in electronic circuit

- **Design:** given a functional specification, design an appropriate electronic circuit
- **Analysis:** given a circuit, provide thorough analysis of its performance
- **Optimization:** combine design and analysis in iterative cycles to improve the operation w.r.t. defined set of goals
- **Synthesis:** use EDA tools to generate an electronic circuit from a set of specifications
- **Approximation:** use approximations for doing fast analytical computation in analysis

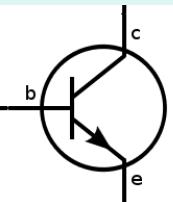




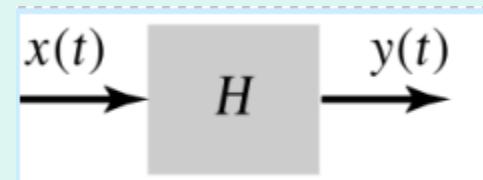
# Review - Linear circuits

- Goal: simplification techniques for circuit analysis - reduced representations through iterative/global transformations
- Linear time-invariant (LTI) circuits/systems
- **Linearity** = superposition + homogeneity
- **Time-invariant** system - the structure of the system does not change in time (no matter when we apply an input, we get the same output response)
- LTI allows the design and analysis in either time or frequency domain
- Often the right feedback allows the **linearization** of a system





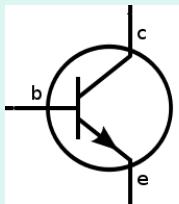
# Time-invariant systems



- A system is **time invariant**  $\leftrightarrow$  a time shift in the input signal produces an identical time shift in the output
- Heuristics: the structure of the system remains the same, it responds identically **no matter when the input signal is applied**
- **What counts is the relative difference of time between the input signal and the output one**

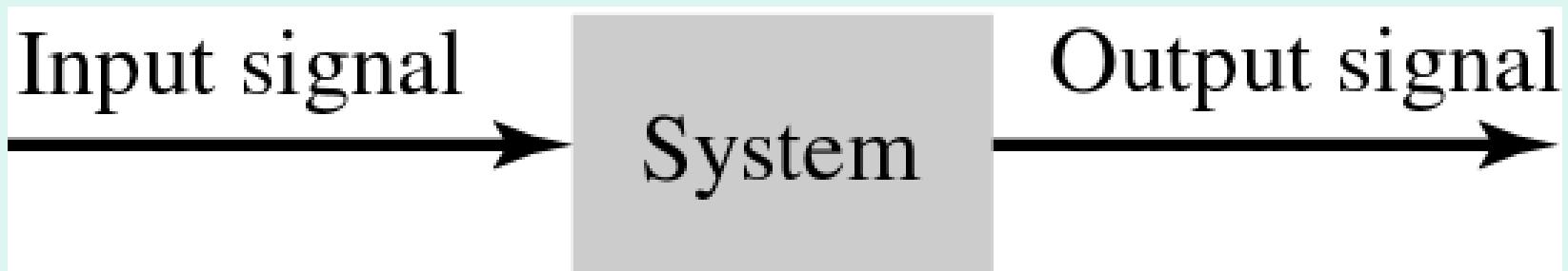
$H\{\}$  is **time invariant** iff  $\left[ y(t) = H\{x(t)\} \Rightarrow y(t - t_0) = H\{x(t - t_0)\}, \text{any } t_0 \right]$

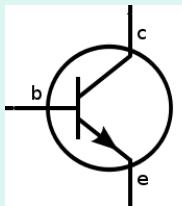




# Causality in systems

- A physical system is causal: the effect of an input signal comes only after the signal occurs!
- **Causal system** = a system where the output  $y(t)$  at some specific instant  $t_0$  only depends on the input  $x(t)$  for values of  $t$  less than or equal to  $t_0$ . Therefore these kinds of systems have outputs and internal states that depends only on the current and previous input values.
- Modern physics have shaken the image of a strictly causal nature (quantum entanglement)

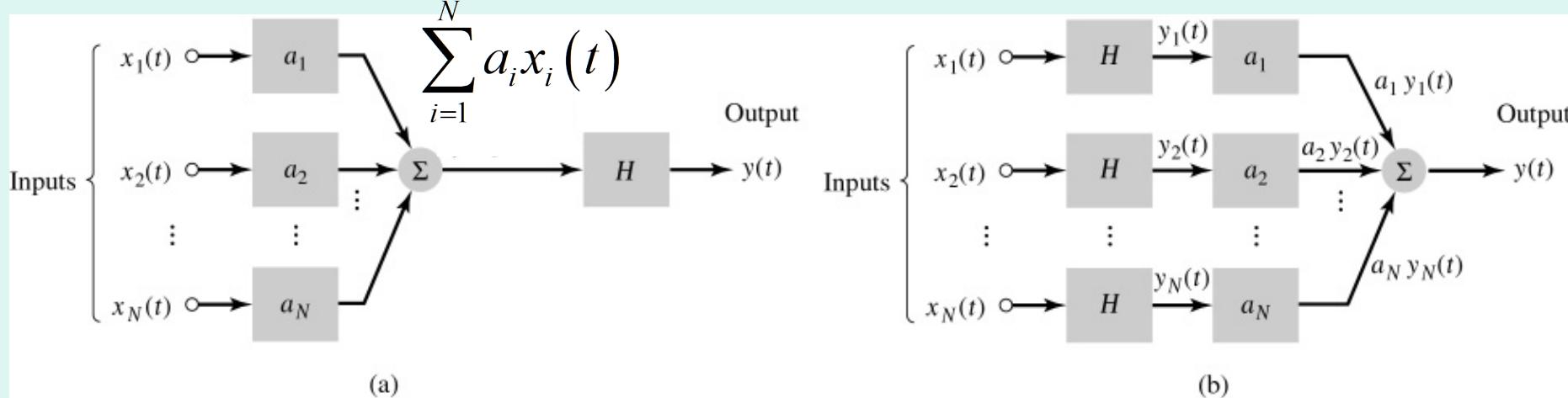




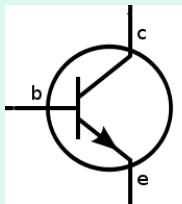
# Linear systems

- Linearity of a system means that its action can be described by a **linear operator  $H$**
- **Superposition + homogeneity properties**

$$H \left\{ a_1 x_1(t) + a_2 x_2(t) \right\} = a_1 H \left\{ x_1(t) \right\} + a_2 H \left\{ x_2(t) \right\}$$

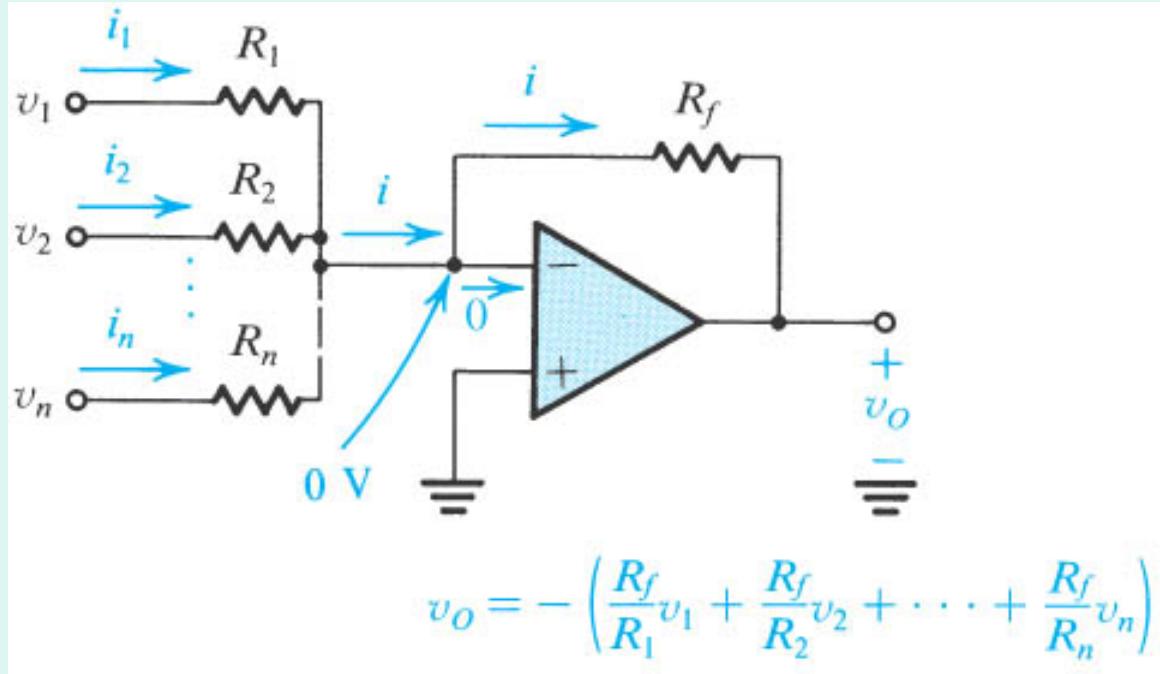


If these two configurations produce the same output  $y(t)$ , the operator  $H$  is linear.



# Use of superposition as an analysis tool

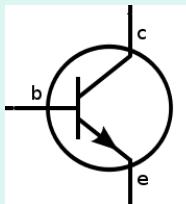
- Exm: the weighted summer



$$v_o = - \left( \frac{R_f}{R_1} v_1 + \frac{R_f}{R_2} v_2 + \cdots + \frac{R_f}{R_n} v_n \right)$$

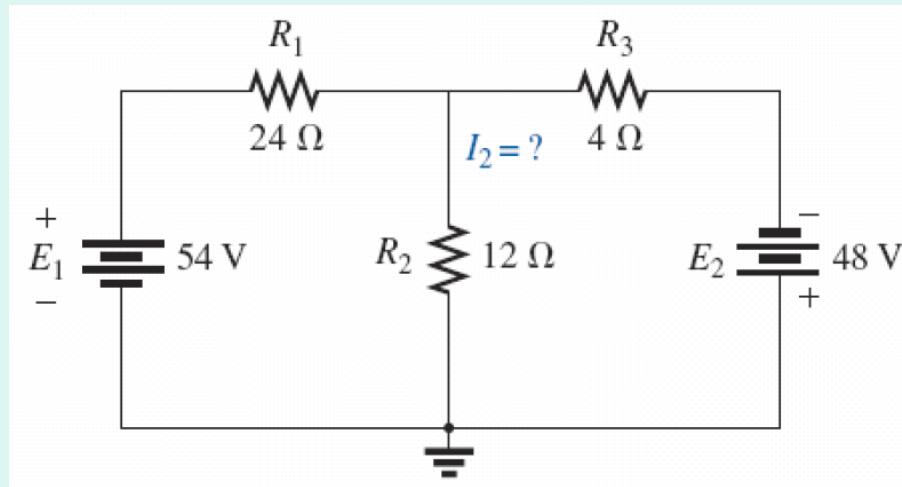
Total effect = sum of partial effects

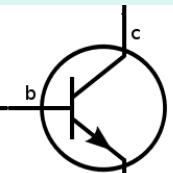




## Exm - homework

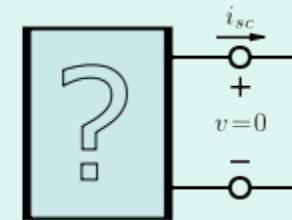
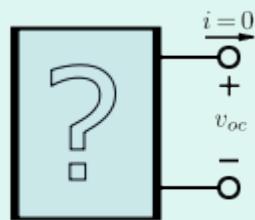
- Use superposition to determine the current through the  $12\Omega$  resistor





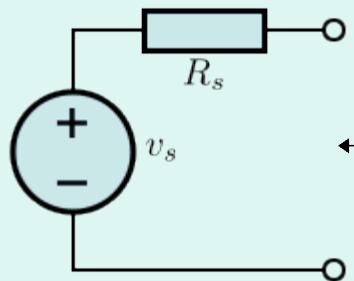
# Circuit transformations

- Recall Thevenin/Norton equivalent circuit theorems for linear uniports
- Application: graphical reduction of branches



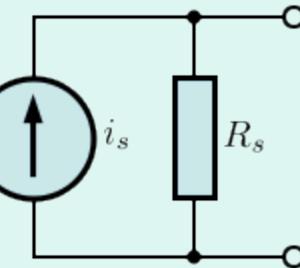
$$v_s = v_{oc}$$

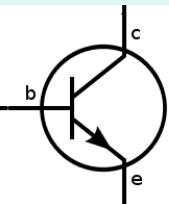
$$i_s = i_{sc}$$



$$i_s$$

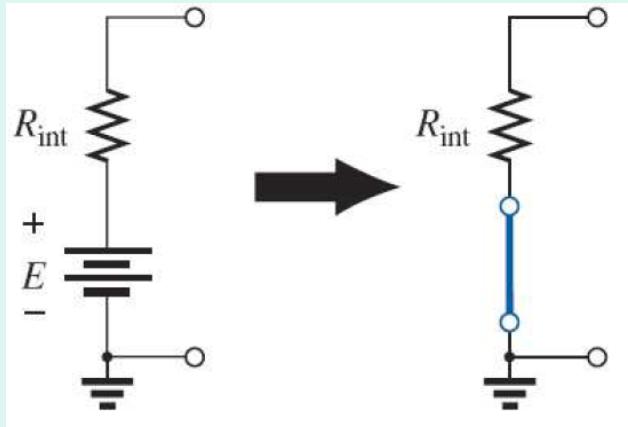
$$= \frac{v_s}{R_s}$$



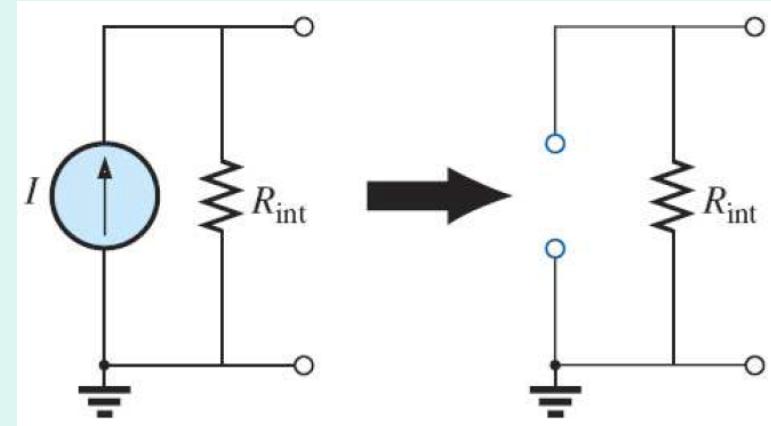


# Circuit reduction techniques (1)

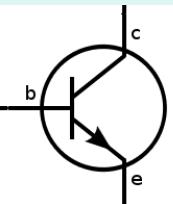
- Superposition theorem: the current through, or voltage across, any element of a network is equal to the algebraic sum of the currents and voltages produced independently by each source (with all other sources removed)



Removing a voltage

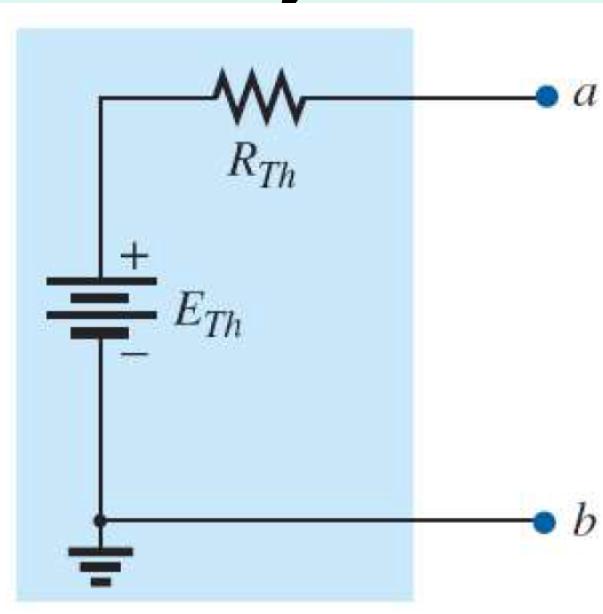


Removing a current



# Thevenin's theorem (internal view)

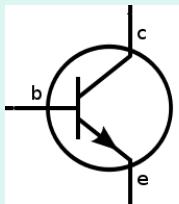
- Any 2-terminal (unipolar) linear network can be replaced by an equivalent circuit consisting solely of a voltage source and series impedance



- $Z_{th}(s)$  is calculated setting all sources to zero (including initial conditions on  $L, C$ )
- $E_{th}(s)$  is calculated by returning all sources to their original position and finding the open-circuit voltage between  $a-b$

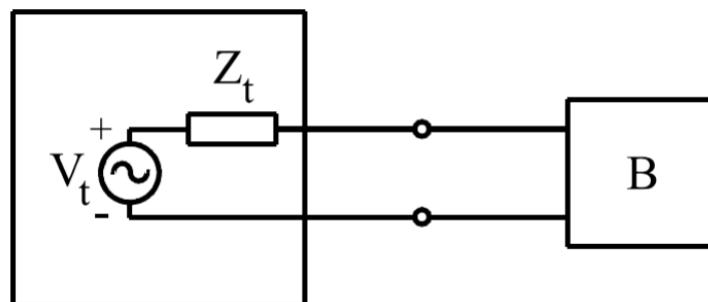
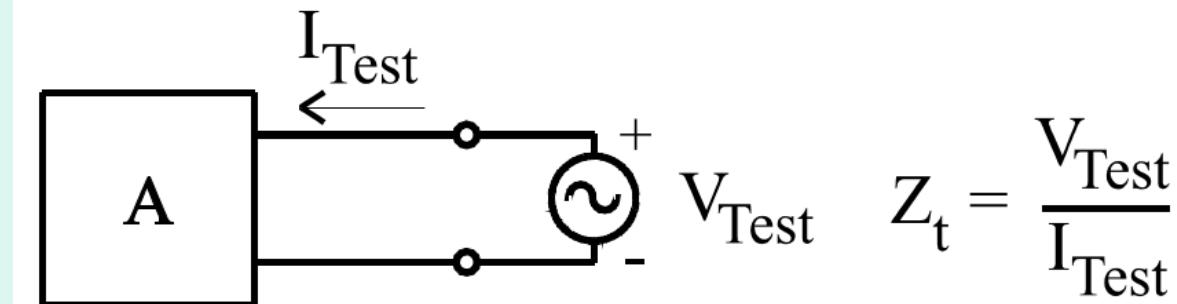
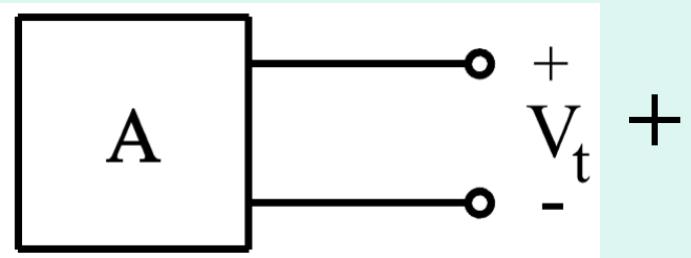
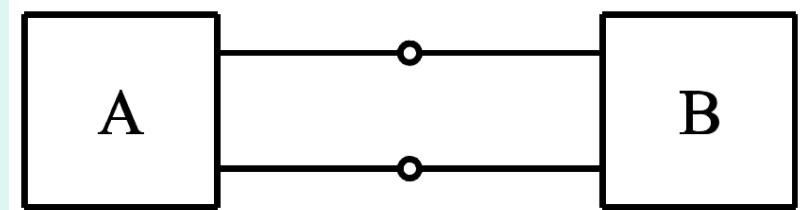
Thevenin equivalent circuit (DC case)

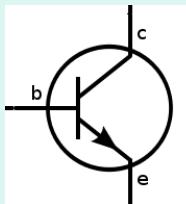




# Thevenin's theorem - external view

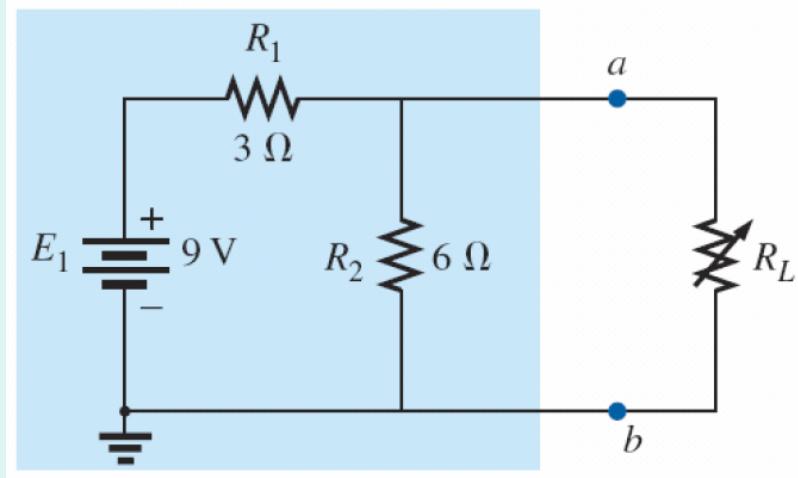
- Any portion of a linear circuit can be reduced, w.r.t. to a port, to an equivalent Thevenin equivalent source  $V_t$  and an equivalent impedance  $Z_t$
- Attention to hidden coupling between ports (e.g. magnetic energy)





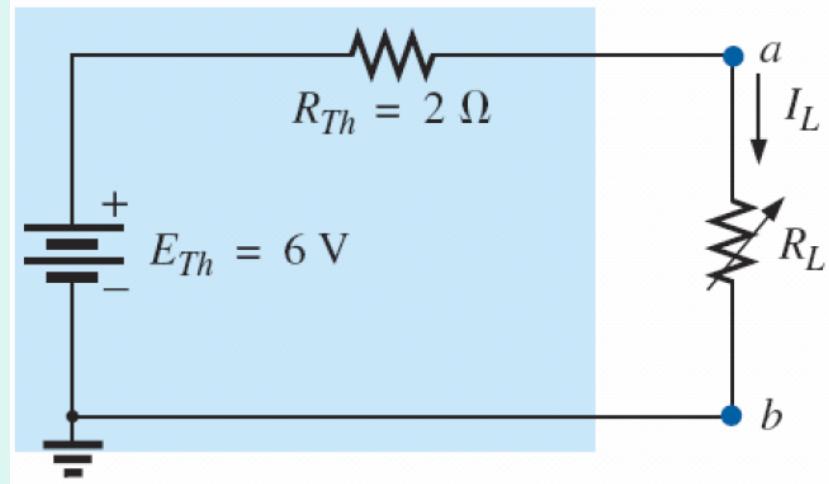
# Useful for simplification of circuits

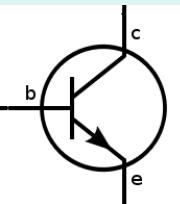
- Find the Thevenin equivalent between terminals a-b



$$R_{TH} = R_1 \parallel R_2 = \frac{R_1 R_2}{R_1 + R_2}$$

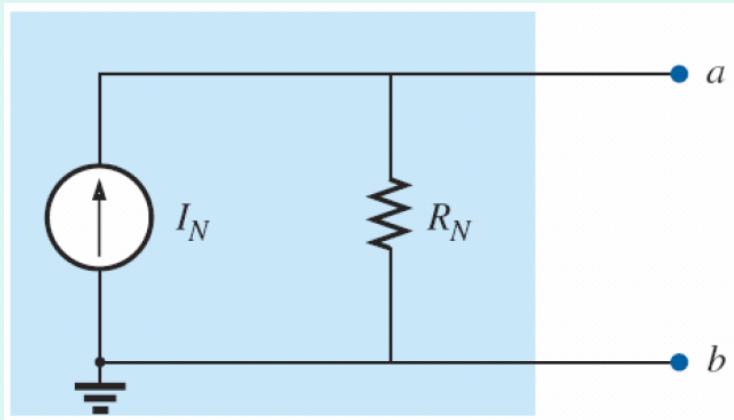
$$V_{TH} = E_1 \frac{R_2}{R_1 + R_2}$$





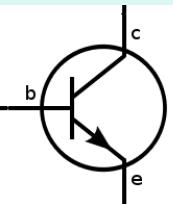
# Norton's theorem

- Any linear 2-terminal network can be replaced by an equivalent circuit consisting of a current source and a parallel impedance



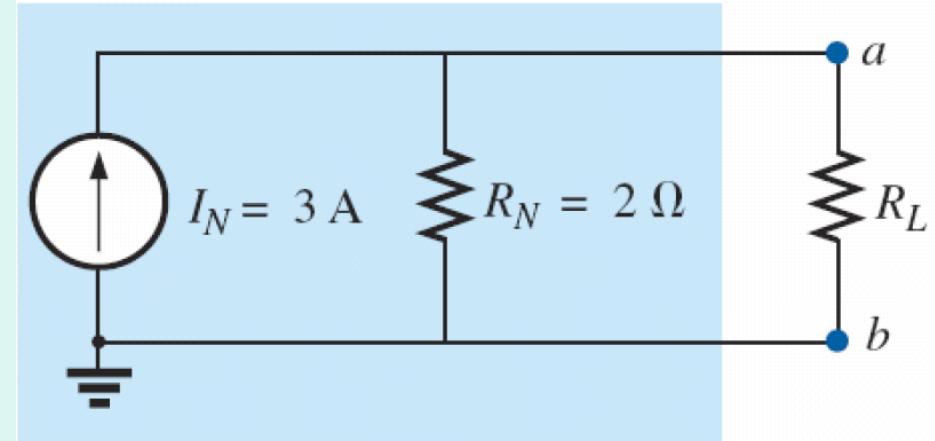
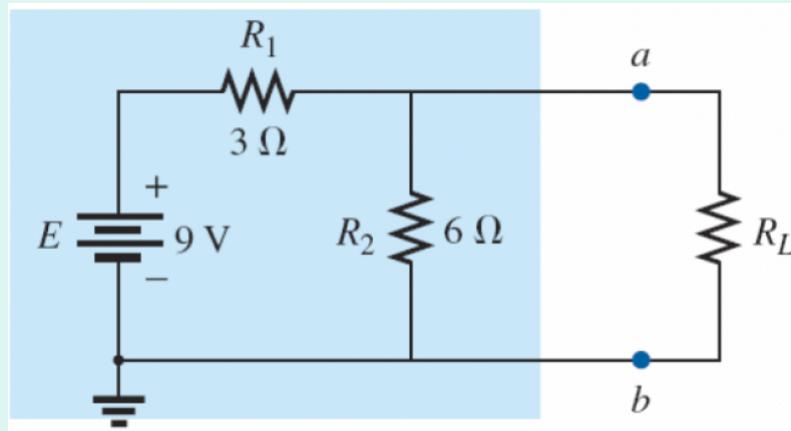
Norton equivalent circuit

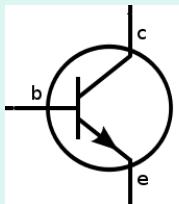
1.  $Z_N(s)$  is computed by setting all sources to zero (including all ICs) and then finding the resultant impedance between a-b ( $Z_N(s)=Z_{th}(s)$ )
2. Calculate  $I_N(s)$  by returning all sources to their original position and then finding the short-circuit current between a-b



## Exm

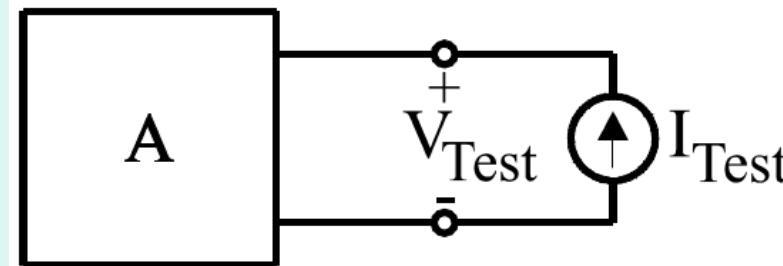
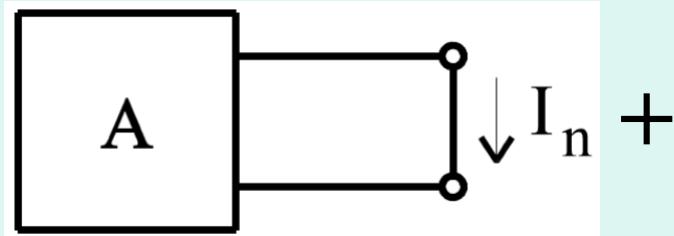
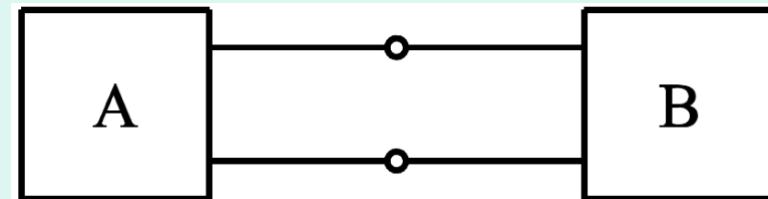
- Find the Norton equivalent circuit between a-b terminals



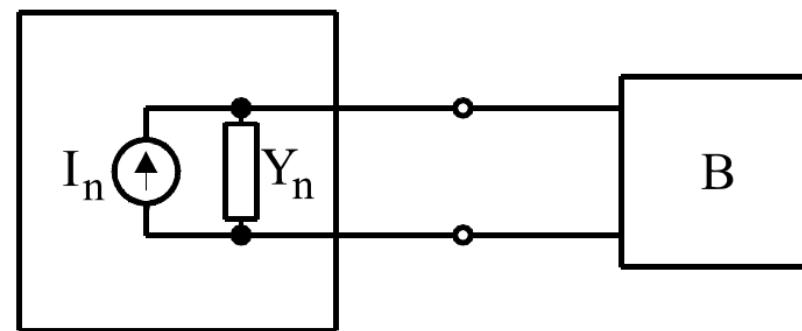


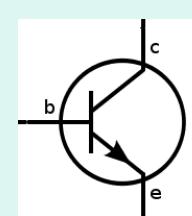
# Norton's theorem - external view

- A portion of linear network may be represented at an electrical port by an equivalent circuit source  $I_n$  and an equivalent admittance  $Y_n$

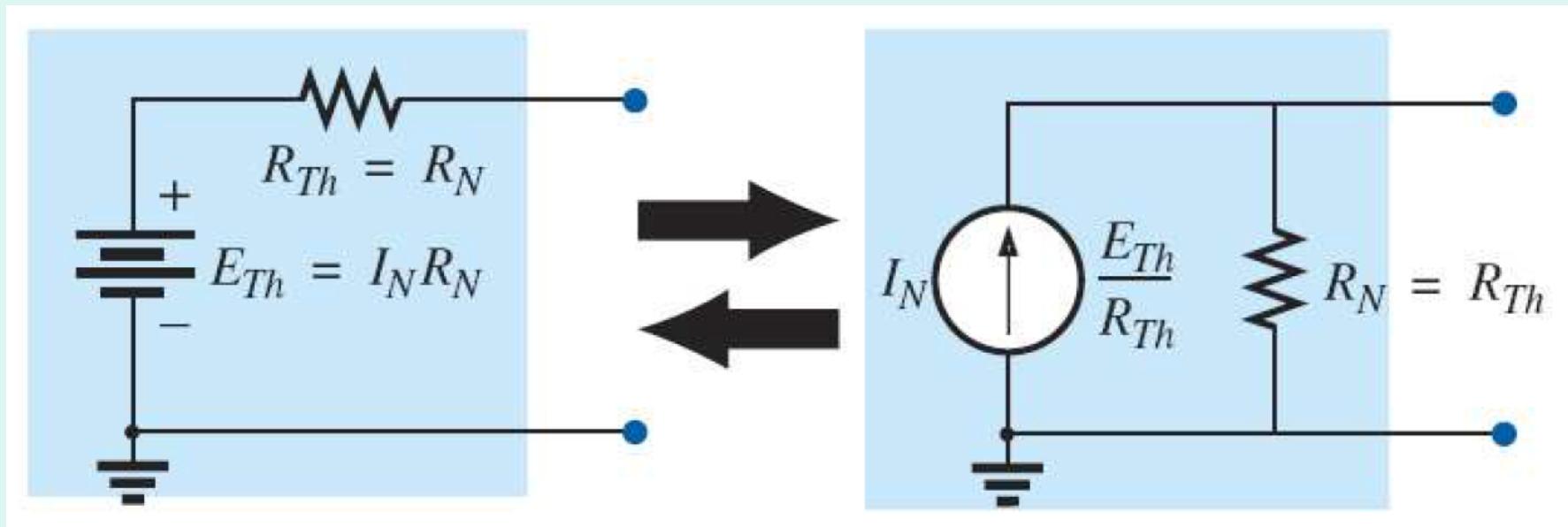


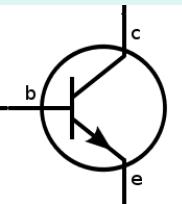
$$Y_n = \frac{I_{\text{Test}}}{V_{\text{Test}}}$$





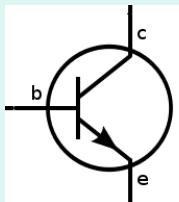
# Converting between Thevening and Norton equivalent uniports





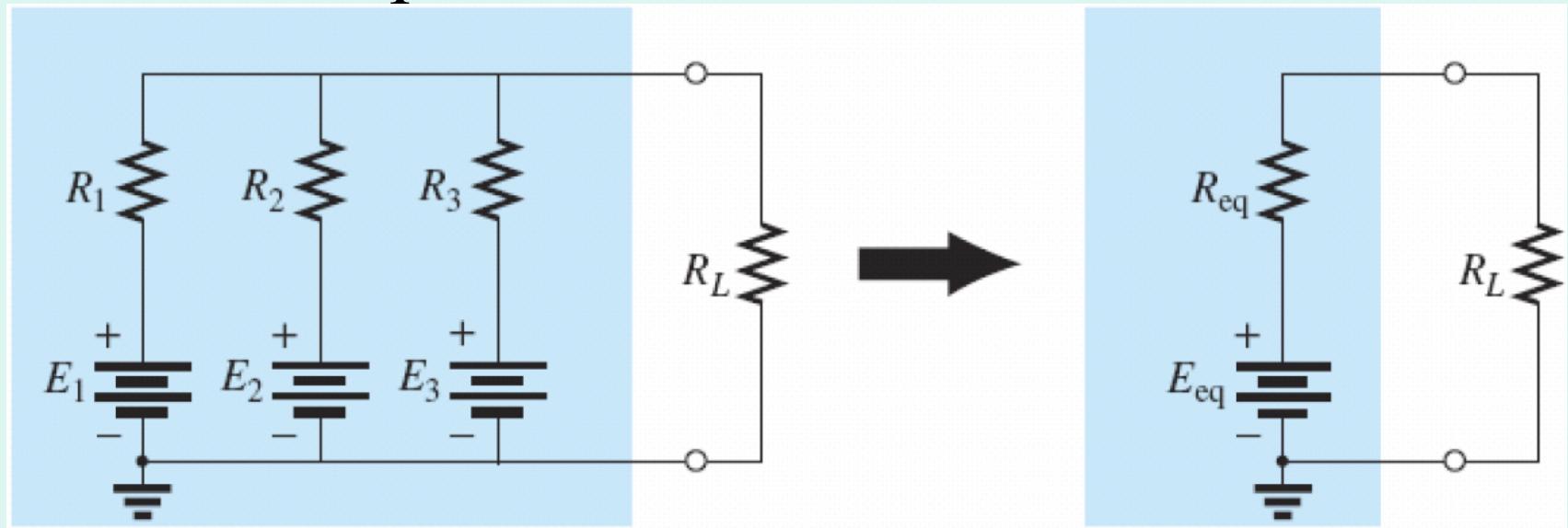
# Question

- What to do if do not have access to the inner circuit (only to the port of A)? How do you determine the Thevenin/Norton equivalent?



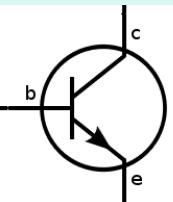
# Circuit reduction techniques (2)

- **Millman's theorem** (for parallel branches) – any number of parallel branches can be reduced to one



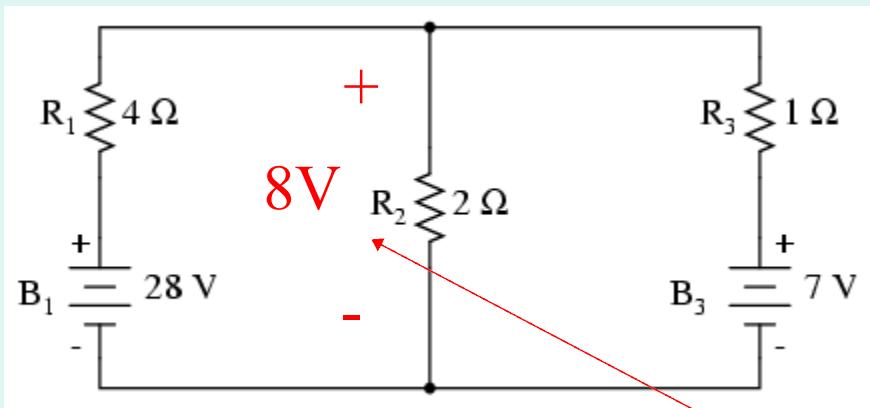
$$Y_{eq}(s) = Y_1 + Y_2 + Y_3 \left( \frac{1}{Z_{eq}(s)} = \frac{1}{Z_1} + \frac{1}{Z_2} + \frac{1}{Z_3} \right)$$

$$E_{eq}(s) = \frac{Y_1 E_1 + Y_2 E_2 + Y_3 E_3}{Y_1 + Y_2 + Y_3}$$



# Exm

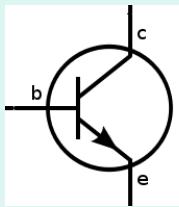
- Circuit computation through Millman's theorem



*Millman's Theorem Equation*

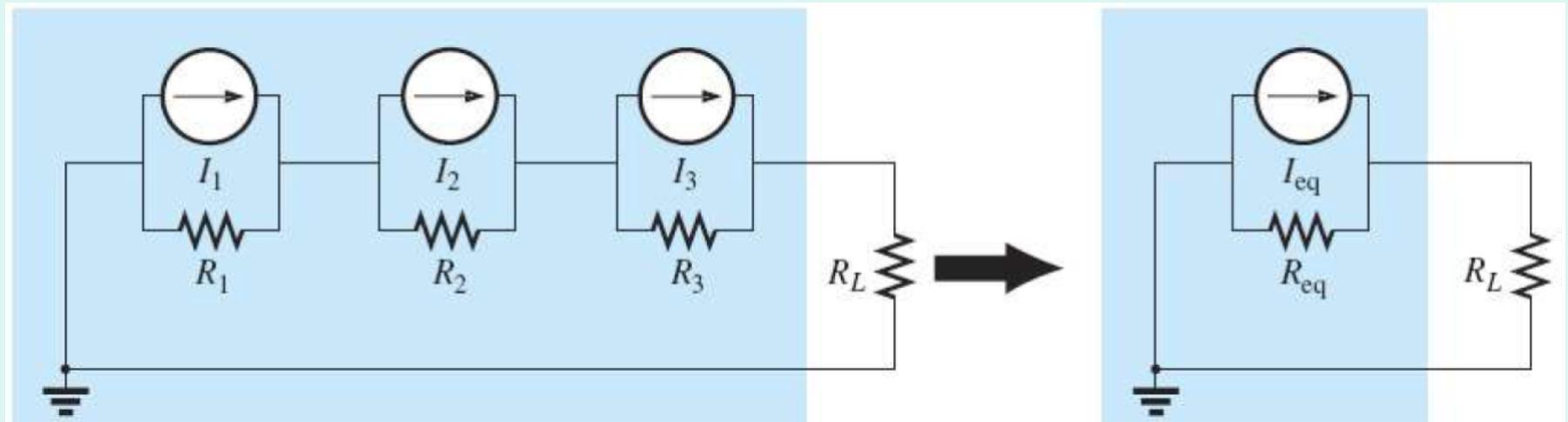
$$\frac{E_{B1}}{R_1} + \frac{E_{B2}}{R_2} + \frac{E_{B3}}{R_3} = \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} \quad \text{Voltage across all branches}$$

$$\frac{\frac{28 \text{ V}}{4 \Omega} + \frac{0 \text{ V}}{2 \Omega} + \frac{7 \text{ V}}{1 \Omega}}{\frac{1}{4 \Omega} + \frac{1}{2 \Omega} + \frac{1}{1 \Omega}} = 8 \text{ V}$$



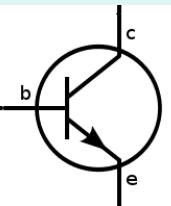
# Dual of Millman's theorem

- Reduces branches in series



$$Z_{eq}(s) = Z_1 + Z_2 + Z_3$$

$$I_{eq}(s) = \frac{Z_1 I_1 + Z_2 I_2 + Z_3 I_3}{Z_1 + Z_2 + Z_3}$$

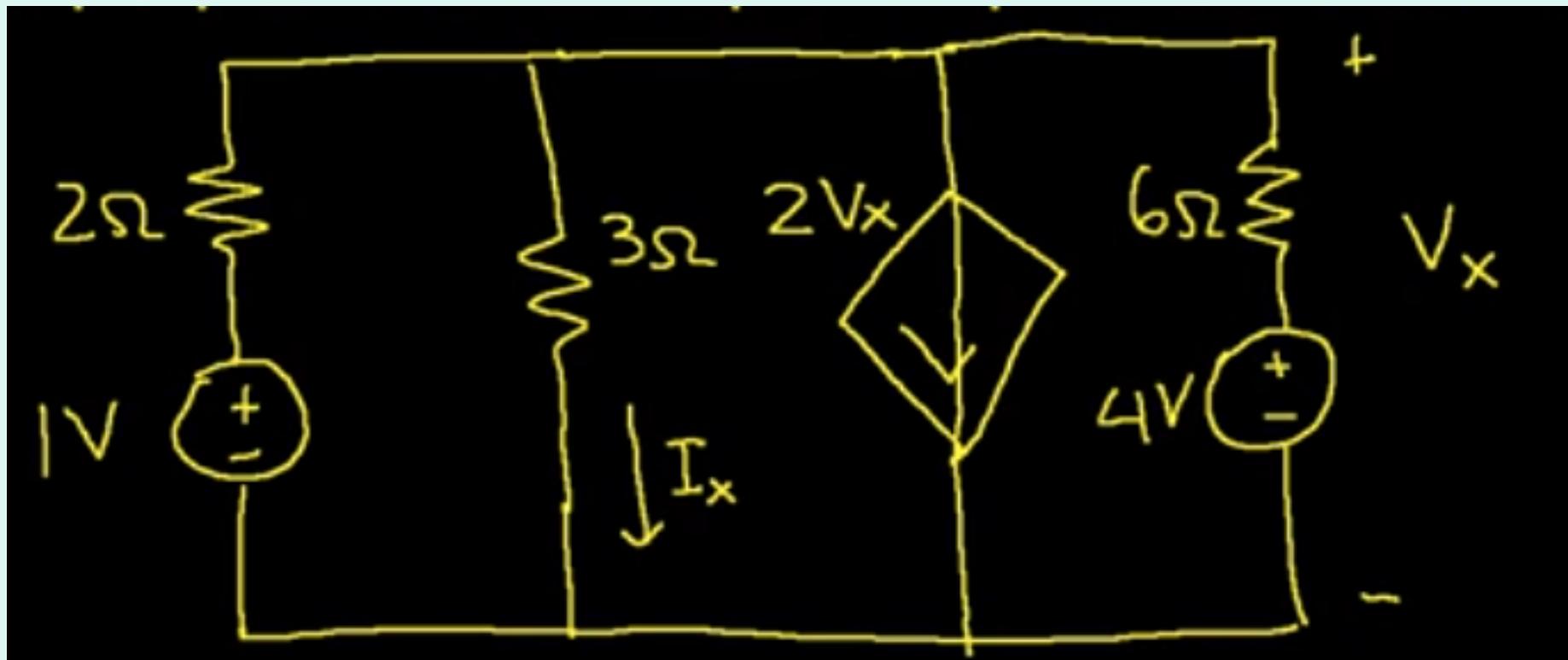


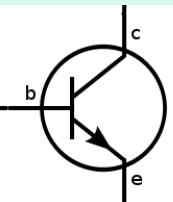
# More subtle case: superposition with linear dependent sources

- Steps:
  1. Identify sources: distinguish between independent and controlled sources in the circuit
  2. Activate one independent source (replace the independent V sources with SC and Independent I sources with OC). Do not deactivate any controlled sources => analyze the circuit to find the partial output(s)
  3. Repeat step 2 for all independent sources
  4. Sum the partial contribution to get the total response



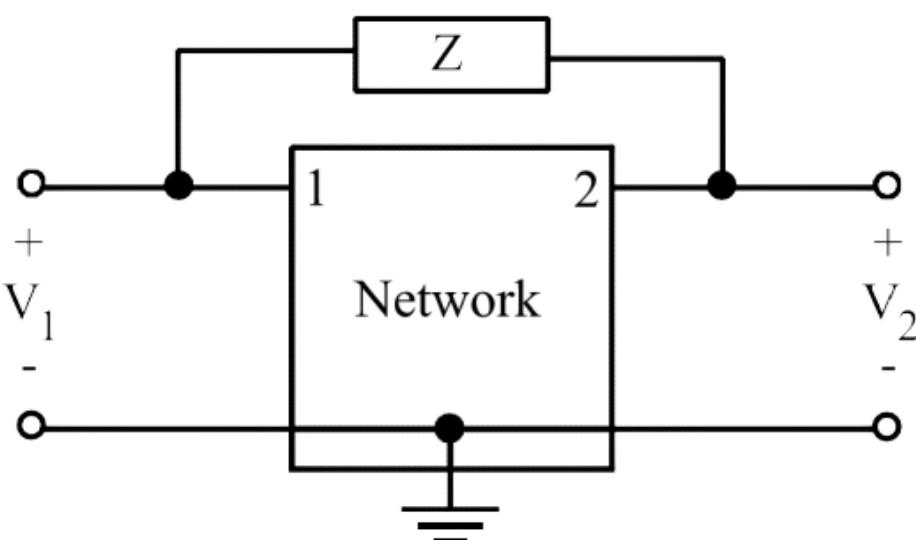
# Homework example



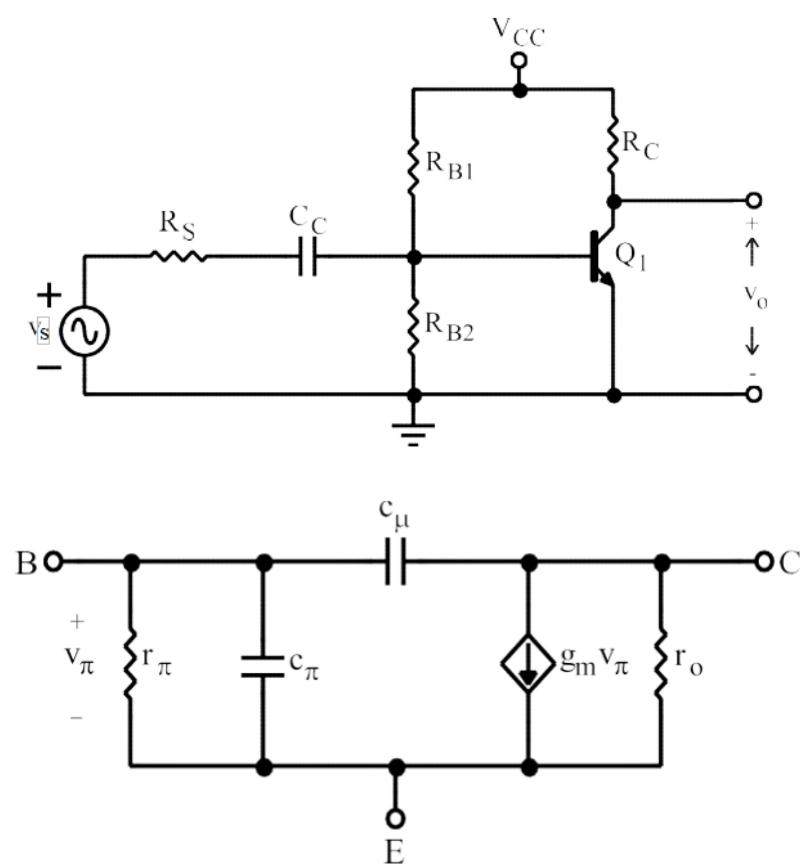


# Miller's theorem

- Helps in analysis by eliminating the feedback

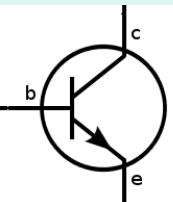


$$V_2 = kV_1$$



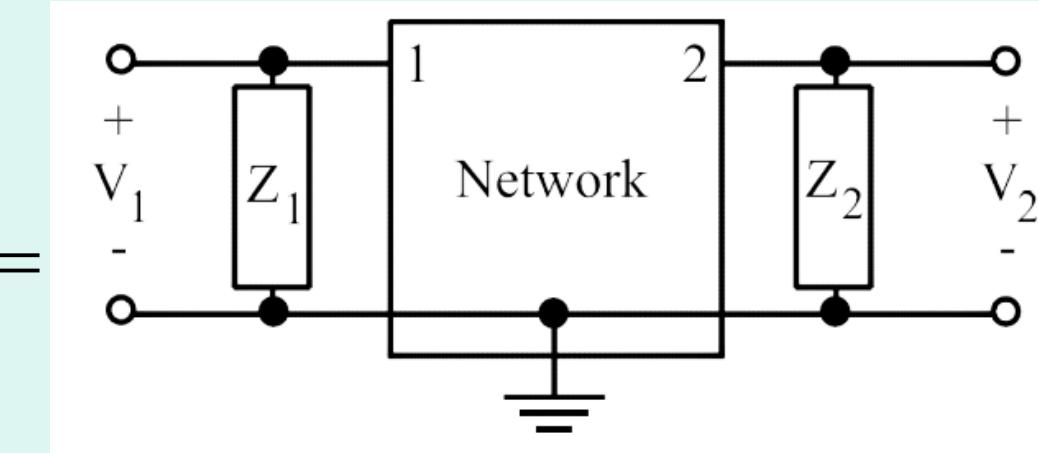
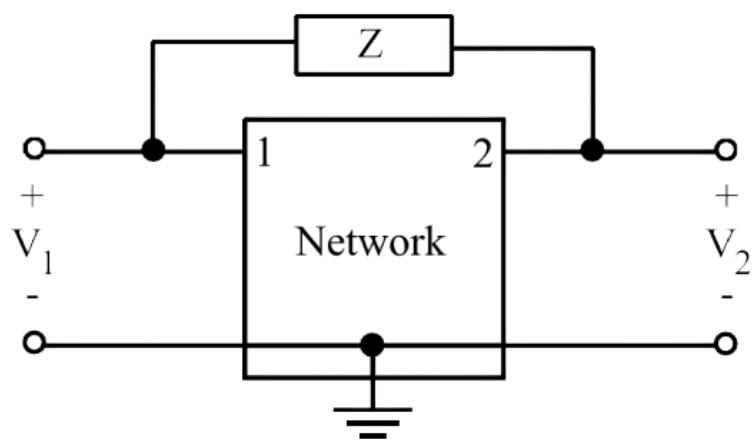
hybrid- $\pi$  small signal model





## Miller's theorem (2)

- Replace the Z feedback with two impedances Z1 and Z2



$$V_2 = kV_1$$

$$V_2 = kV_1$$

$$Z_1 = Z \frac{1}{1-k}$$

$$Z_2 = Z \frac{k}{k-1}$$

