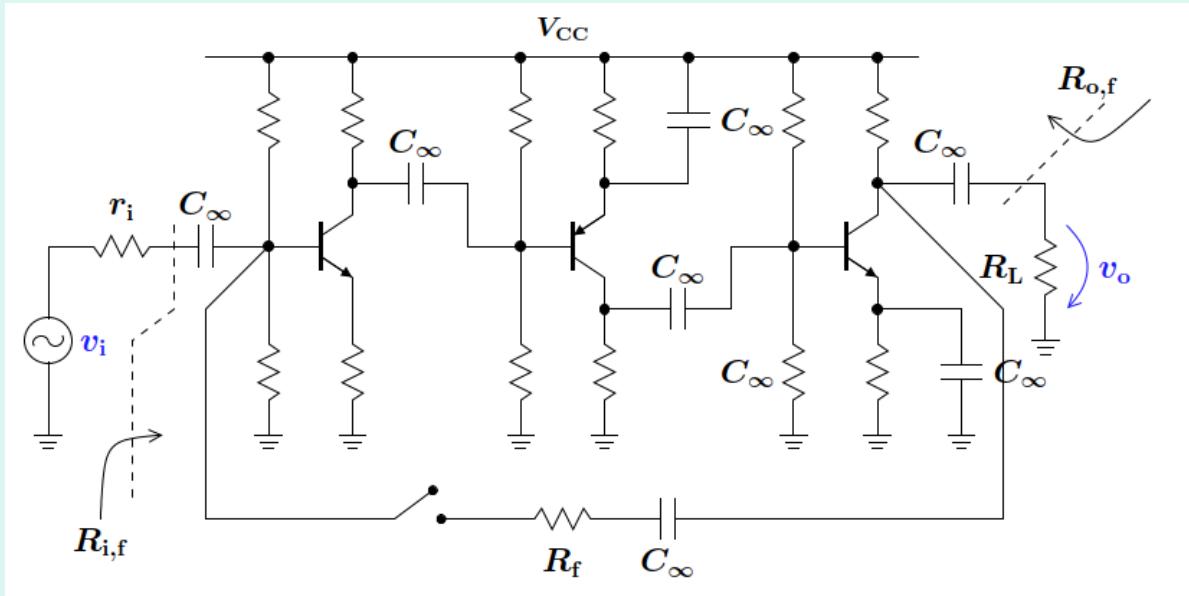
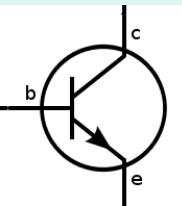


# ELEC 301 - BJT small signal model

L10 - Sep 25

Instructor: Edmond Cretu





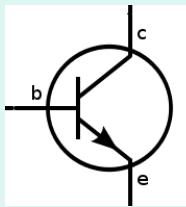
# Last time

- The open-circuit (OCT) and short-circuit (SCT) time constants method
- SCT - used to approximate the LF cut-off frequency
- OCT - used to approximate the HF cut-off frequency

$$\omega_{L3dB} \approx \omega_{Lp1} + \omega_{Lp2} + \dots + \omega_{LpN} = \frac{1}{\tau_{C_1}^{sc}} + \frac{1}{\tau_{C_2}^{sc}} + \dots + \frac{1}{\tau_{C_3}^{sc}}$$

$$\frac{1}{\omega_{H3dB}} \approx \frac{1}{\omega_{Hp1}} + \frac{1}{\omega_{Hp2}} + \dots + \frac{1}{\omega_{HpM}} = \tau_{C_1}^{oc} + \tau_{C_2}^{oc} + \dots + \tau_{C_M}^{oc}$$



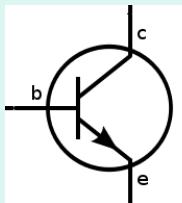


# Today - Amplifiers with BJT

- Small-signal model for BJT (“hybrid- $\pi$ ” model)
- Notation conventions:
  - capital I’s and V’s with capital subscripts denote d.c. values
  - capital I’s and V’s with lowercase subscripts denote complex values (phasors)
  - lowercase i’s and v’s with capital subscripts denote instantaneous values, and
  - lowercase i’s and v’s with lowercase subscripts denote small signal values

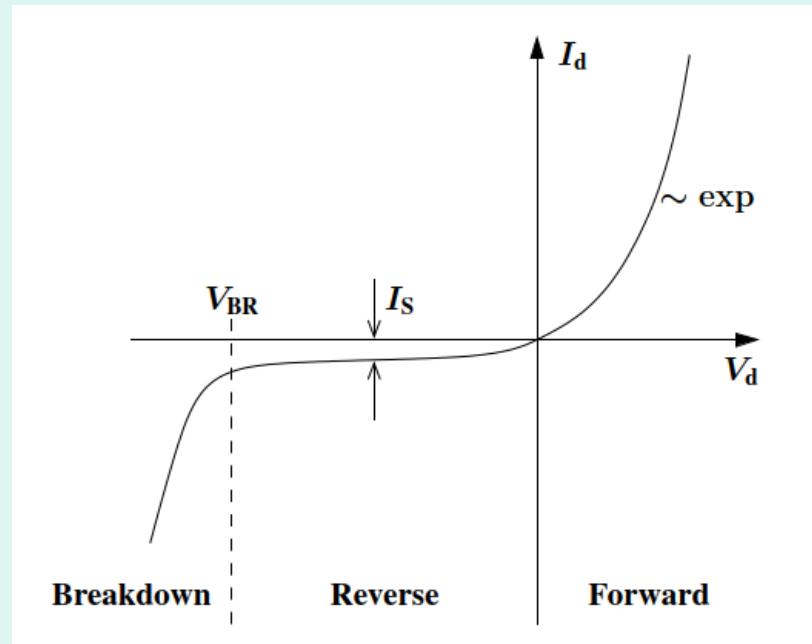
$$i_C = I_C + i_c$$



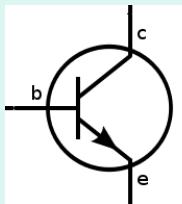


# Diodes - recall

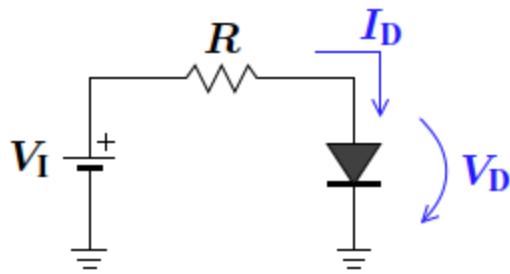
- Three operating regions:
  - Forward-bias region ( $v_D > 0$ )
  - Reverse-bias region ( $V_{BR} < v_D < 0$ )
  - Breakdown region ( $v_D < V_{BR}$ )
- Diode law (Shockley diode eqn.
  - $I_S$ =reverse-bias saturation current
  - $n$  = ideality factor (1..2)
  - $V_T = kT/q$ =thermal voltage



$$i_D = I_S \left( e^{\frac{v_D}{nV_T}} - 1 \right)$$



# Biassing - quiescent point



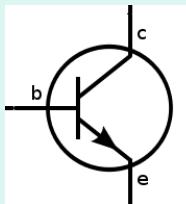
$$\begin{cases} V_I = R \cdot I_D + V_D \\ I_D = I_S \exp \frac{V_D}{V_T} \end{cases} \rightarrow \begin{cases} \text{No closed-form solution} \\ \text{To be solved numerically} \end{cases}$$

- DC level biasing -  $(V_D, I_D)$  is called the quiescent point
- $V_D = V_T \ln(I_D/I_S) \approx 0.6..0.7V$  for a large range of currents

$$I_{D0} = \frac{V_I - 0.6V}{R}$$

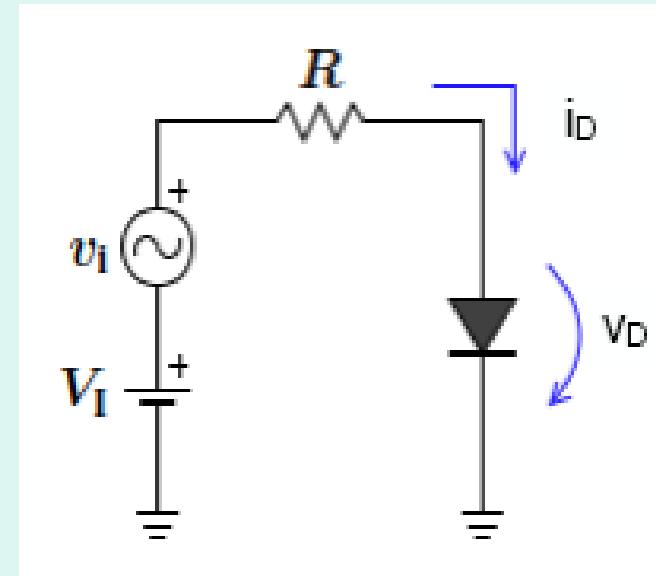
$$V_{D0} = 0.6V$$

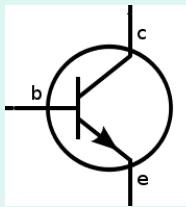




# L10 Q01 - diode model

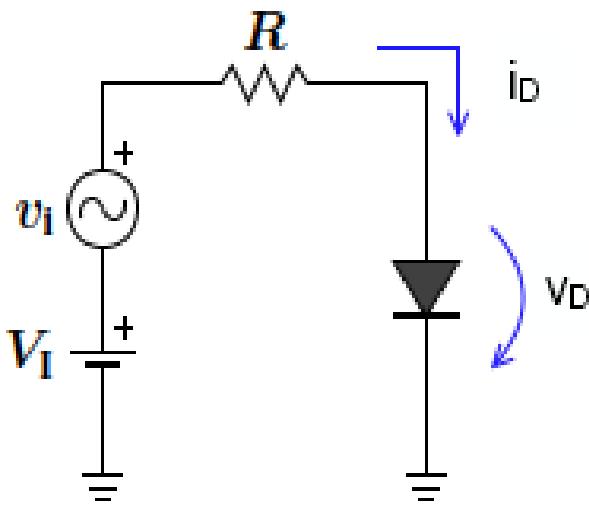
- Can we apply superposition to compute the total current through the circuit?  
A. Yes  
B. No





# Diode - small signal model

- DC+ small AC voltages
- nonlinear circuit => no superposition!

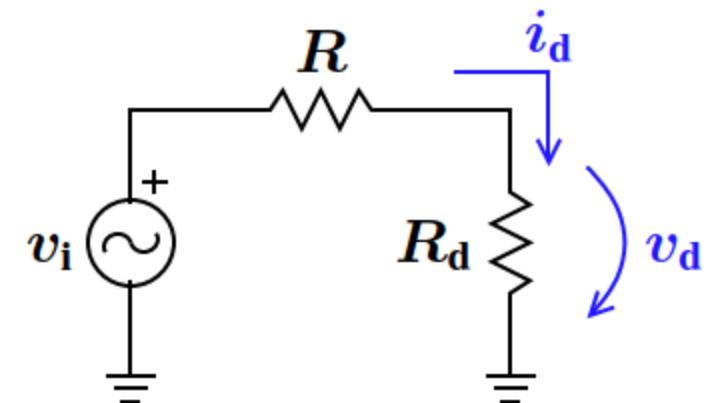


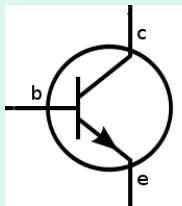
$$i_D = I_s \left( e^{\frac{v_D + v_d}{V_T}} - 1 \right) \approx I_s e^{\frac{v_d}{V_T}} = \underbrace{I_s e^{\frac{V_D}{V_T}}}_{I_D} e^{\frac{v_d}{V_T}} = I_D e^{\frac{v_d}{V_T}} \quad v_d \ll V_T \approx I_D \left( 1 + \frac{v_d}{V_T} \right)$$

$$I_D + i_d \approx I_D \left( 1 + \frac{v_d}{V_T} \right) \Rightarrow i_d \approx \frac{I_D}{V_T} v_d = \frac{v_d}{r_d}$$

$r_d = r_d(I_D)$  = dynamic resistance of the diode

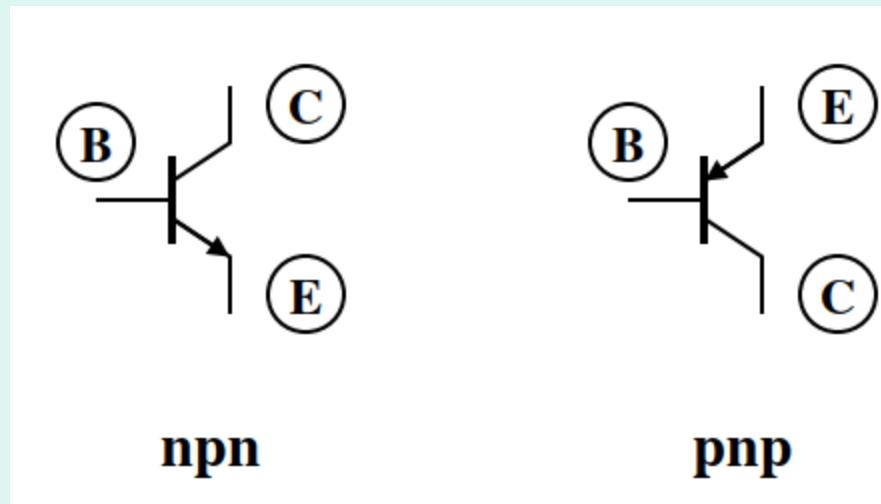
$$i_D = I_D + i_d \approx \frac{V_1 - 0.6V}{R} + \frac{v_i}{R + r_d}$$

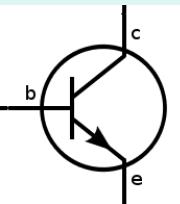




# Bipolar junction transistors (BJTs)

- Two types: npn, pnp
- Three terminals: emitter, base, collector

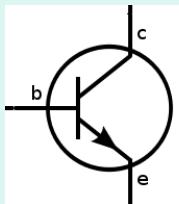




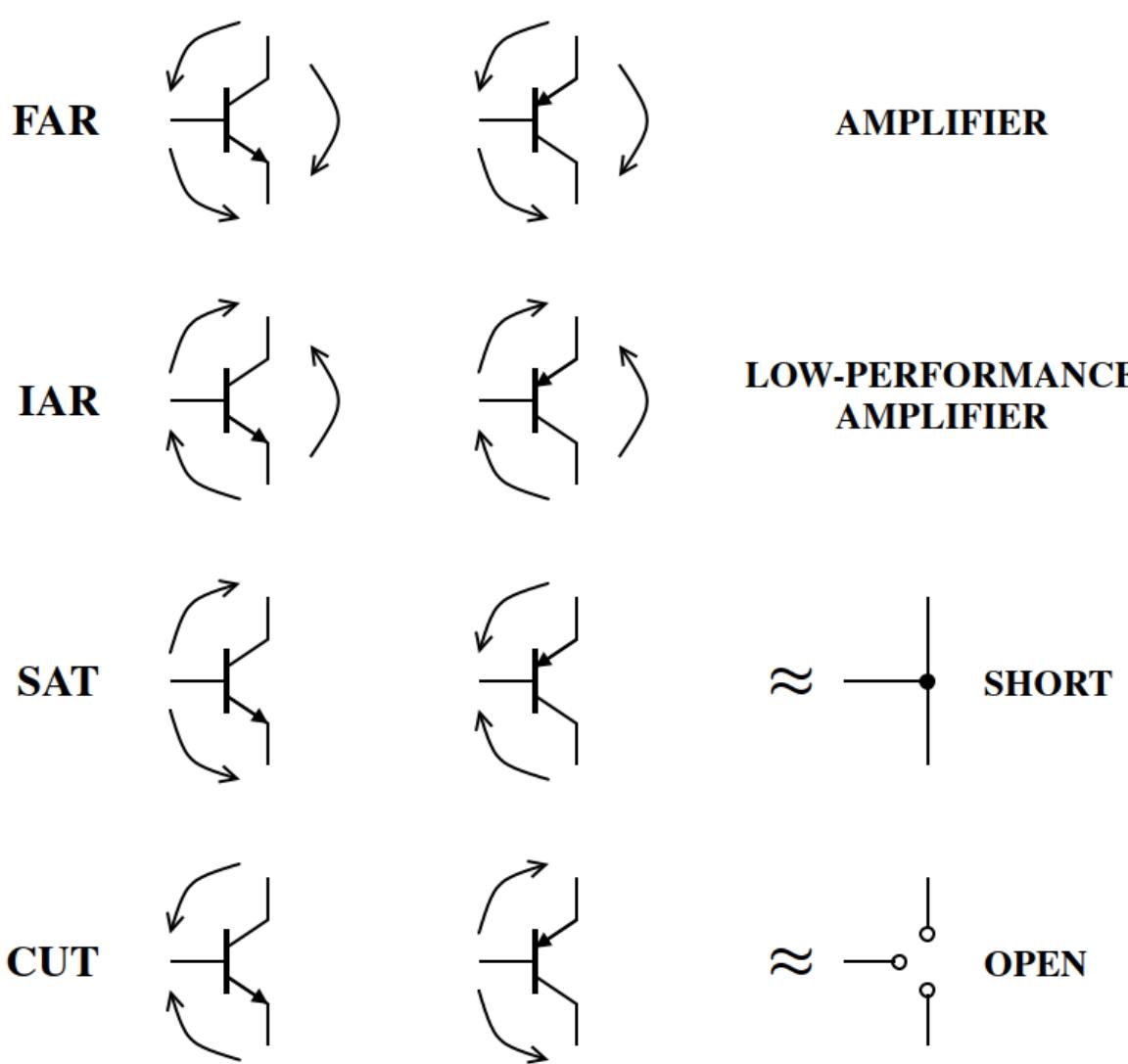
# BJT operating modes

- Four transistor operating modes:
  - **Saturation** -- The transistor acts like a short circuit. Current freely flows from collector to emitter.
  - **Cut-off** -- The transistor acts like an open circuit. No current flows from collector to emitter.
  - **Active** -- The current from collector to emitter is proportional to the base current.
  - **Inverse-Active** -- Like active mode, the current is proportional to the base current, but it flows in reverse. Current flows from emitter to collector (not, exactly, the purpose transistors were designed for)

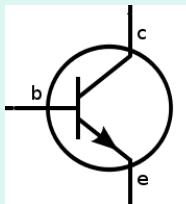




# BJT operating modes



- FAR = forward active region
- IAR = inverse active region (poor  $\beta$ )
- SAT = saturation
- CUT = cut-off



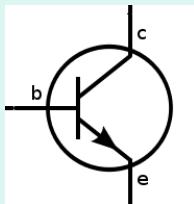
# BJT in active operating mode

- EB junction must be forward biased ( $V_{BE} \sim 0.6V$  for a npn transistor)
- CB junction must be reversed biased ( $V_{CB} > 0V$  for npn)
- DC model:

$$i_C = I_C + i_c$$
$$I_C = \alpha I_E = \beta I_B$$

- $\alpha$ =common base current gain factor
- $\beta$ =common emitter current gain factor
- $V_T$ =thermal voltage (average thermal energy available to charge carriers)= $kT/q \sim 25mV$  at 25deg
- $I_S$ = reverse saturation current





# BJT DC model

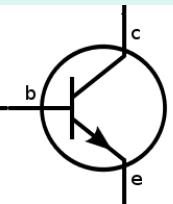
$$I_E = I_B + I_C$$

$$I_C = \alpha I_E = \beta I_B$$

$$I_C = I_S e^{V_{BE}/V_T}$$

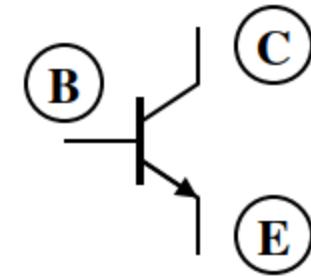
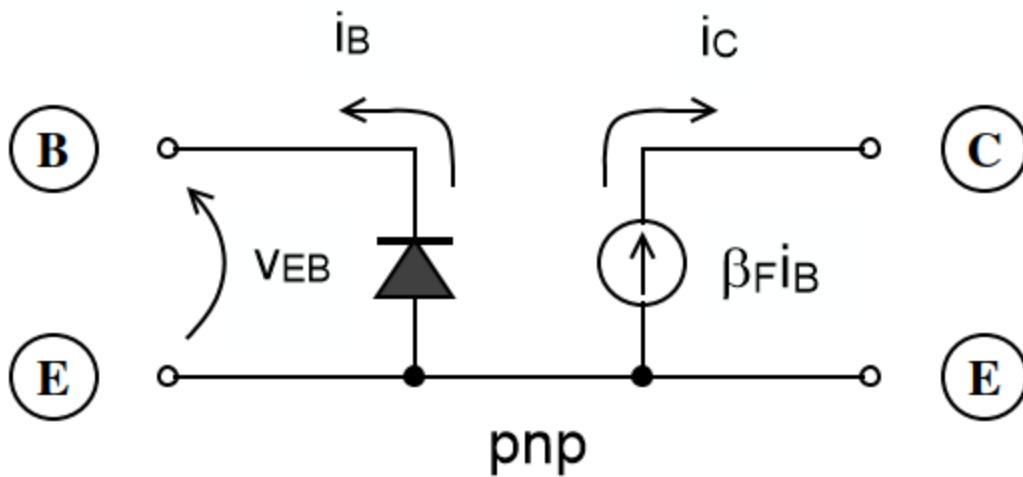
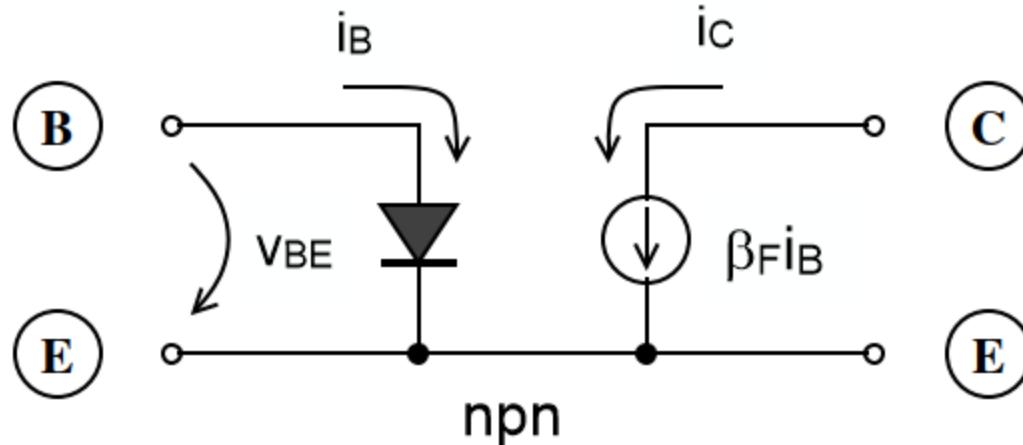
$$\alpha = \frac{\beta}{\beta + 1} \Leftrightarrow \beta = \frac{\alpha}{1 - \alpha}$$



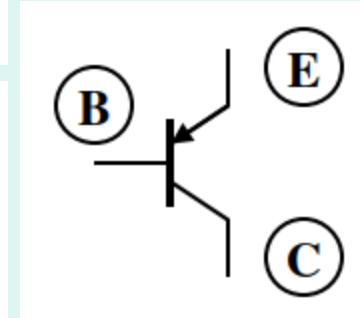


# Large-signal model for BJT

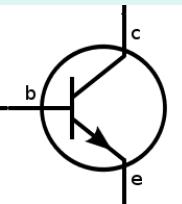
- REM: coupled junctions



$$i_C = I_S e^{\frac{v_{BE}}{V_T}}, i_B = \frac{I_S}{\beta} e^{\frac{v_{BE}}{V_T}}$$



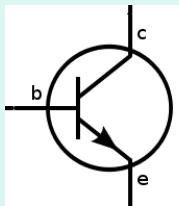
$$i_C = I_S e^{\frac{v_{EB}}{V_T}}, i_B = \frac{I_S}{\beta} e^{\frac{v_{EB}}{V_T}}$$



# BJT parameters

- Saturation current:  $I_S = 10^{-16} \dots 10^{-14} \text{ A}$
- Thermal voltage:  $V_T = kT/q \approx 25 \text{ mV}$  at  $25^\circ\text{C}$
- Forward current gain  $\beta_F = \beta$  (assumed constant):
  - $\beta_{F, \text{npn}} = 50 \dots 500$  (technology optimized for npn)
  - $\beta_{F, \text{pnp}} = 10 \dots 100$



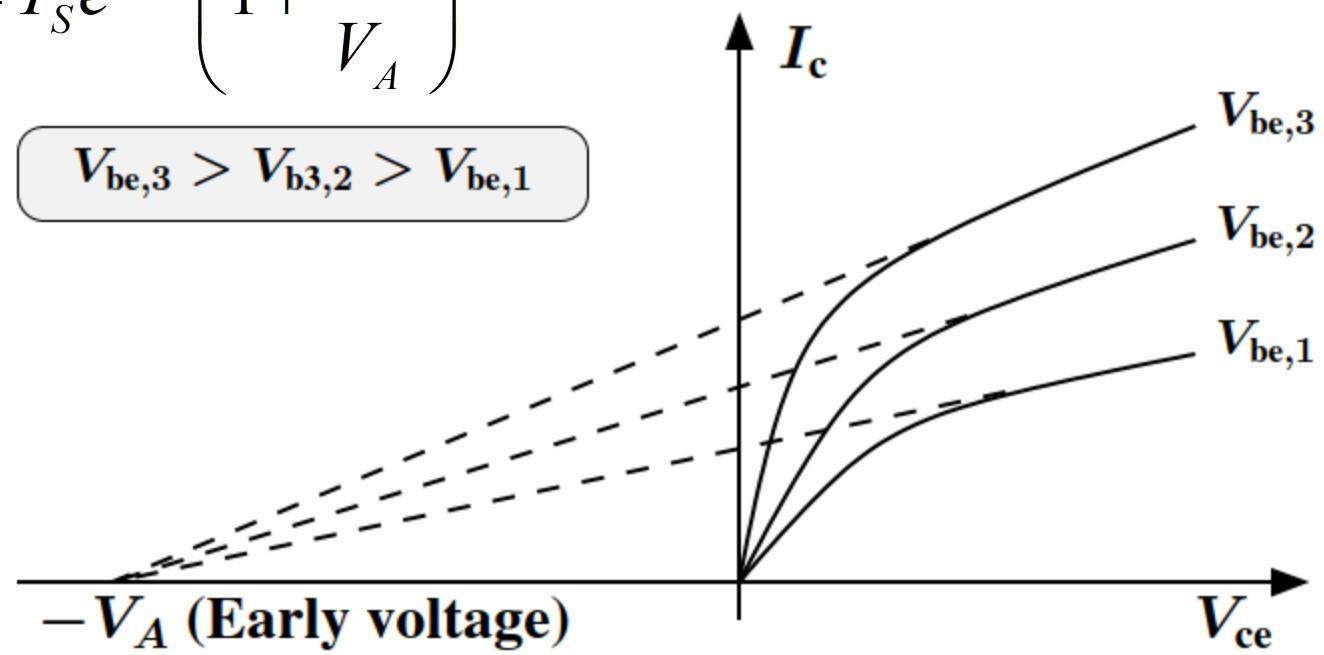


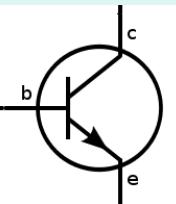
# BJT current-voltage relations

- Early effect (discovered by James Early):  $v_{CE} \nearrow \Rightarrow i_C \nearrow$
- Early voltage  $V_A$  - models the Early effect
- $V_{A,typ}=50..100V$  (larger is better)

$$i_C = i_C(v_{BE}, v_{CE}) = I_S e^{\frac{v_{BE}}{V_T}} \left( 1 + \frac{v_{CE}}{V_A} \right)$$

$$V_{be,3} > V_{be,2} > V_{be,1}$$





# Small variations around the DC bias values

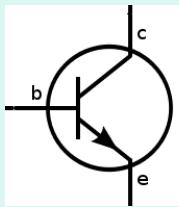
- Consider a small variation  $v_{be}$  around the DC bias value  $V_{BE}$

$$v_{BE} = V_{BE} + v_{be} \Rightarrow i_C = I_S e^{v_{BE}/V_T} = I_S e^{V_{BE}/V_T} e^{v_{be}/V_T} = I_C e^{v_{be}/V_T}$$

$$i_C = I_C + i_c \stackrel{v_{be} \ll V_T}{\approx} I_C \left( 1 + \frac{v_{be}}{V_T} \right) = I_C + \frac{I_C}{V_T} v_{be}$$

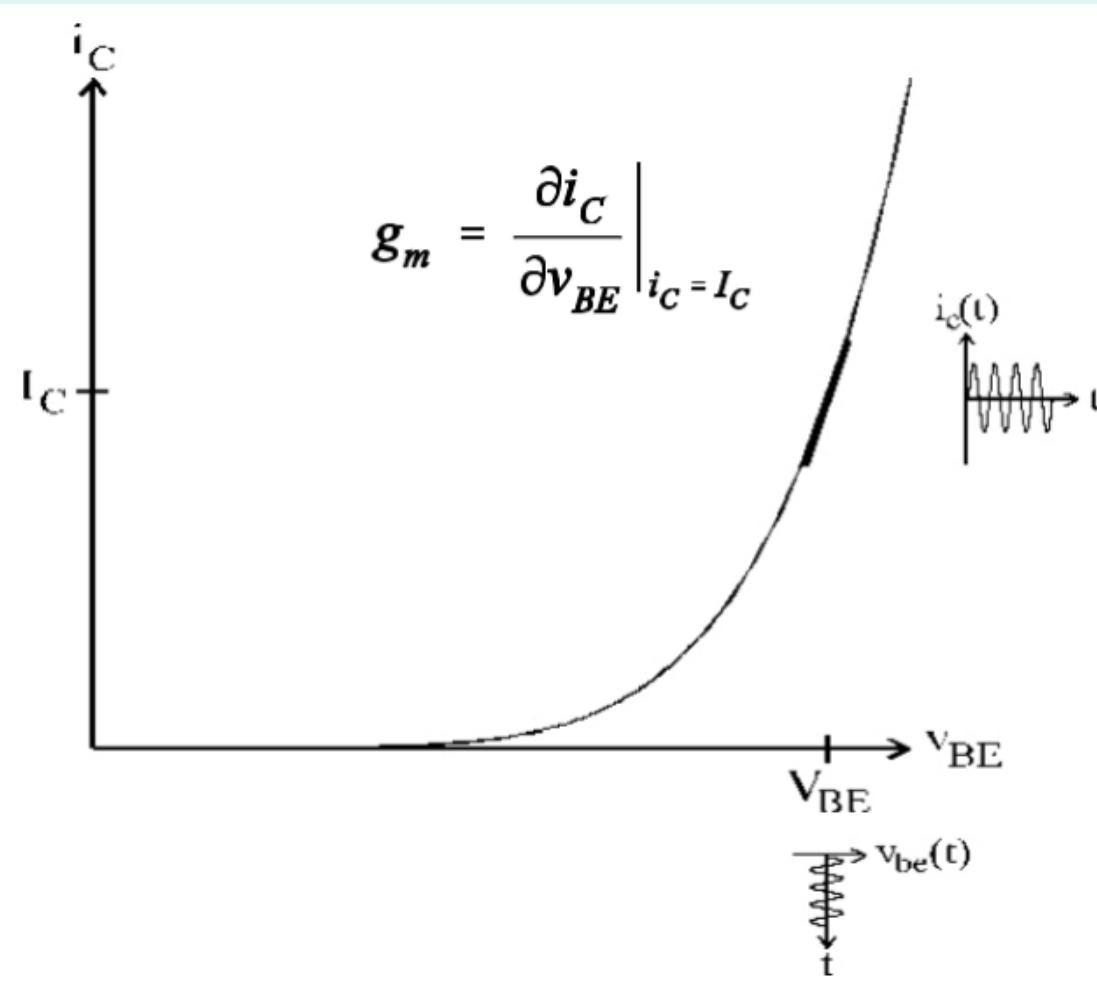
$$i_c = \underbrace{\frac{I_C}{V_T}}_{g_m} v_{be} \quad g_m = \text{small signal transconductance}$$

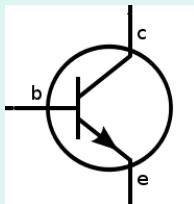




# Transconductance $g_m$

- $g_m = \text{the slope of the } i_C(v_{BE}) \text{ curve}$





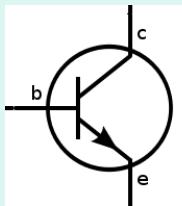
# BE input port

$$i_B = I_B + i_b = \frac{i_C}{\beta} = \frac{I_C + i_c}{\beta} = \frac{I_C}{\beta} + \frac{g_m}{\beta} v_{be} \Rightarrow i_b = \frac{g_m}{\beta} v_{be}$$

- Small-signal input resistance:

$$r_\pi = \frac{v_{be}}{i_{be}} = \frac{\beta}{g_m} = \beta \frac{V_T}{I_C} = \frac{V_T}{I_B}$$





# Basic Hybrid- $\pi$ model for BJT

- Small signal model without considering capacitive effects, nor the Early effect

