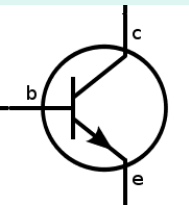


Last time

- The open-circuit (OCT) and short-circuit (SCT) time constants method
- SCT - used to approximate the LF cut-off frequency
- OCT - used to approximate the HF cut-off frequency

$$\omega_{L3dB} \approx \omega_{Lp1} + \omega_{Lp2} + \dots + \omega_{LpN} = \frac{1}{\tau_{C_1}^{sc}} + \frac{1}{\tau_{C_2}^{sc}} + \dots + \frac{1}{\tau_{C_3}^{sc}}$$

$$\frac{1}{\omega_{H3dB}} \approx \frac{1}{\omega_{Hp1}} + \frac{1}{\omega_{Hp2}} + \dots + \frac{1}{\omega_{HpM}} = \tau_{C_1}^{oc} + \tau_{C_2}^{oc} + \dots + \tau_{C_M}^{oc}$$

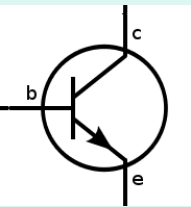


Today - Amplifiers with BJT

- Small-signal model for BJT (“hybrid- π ” model)
- Notation conventions:
 - capital I’s and V’s with capital subscripts denote d.c. values
 - capital I’s and V’s with lowercase subscripts denote complex values (phasors)
 - lowercase i’s and v’s with capital subscripts denote instantaneous values, and
 - lowercase i’s and v’s with lowercase subscripts denote small signal values

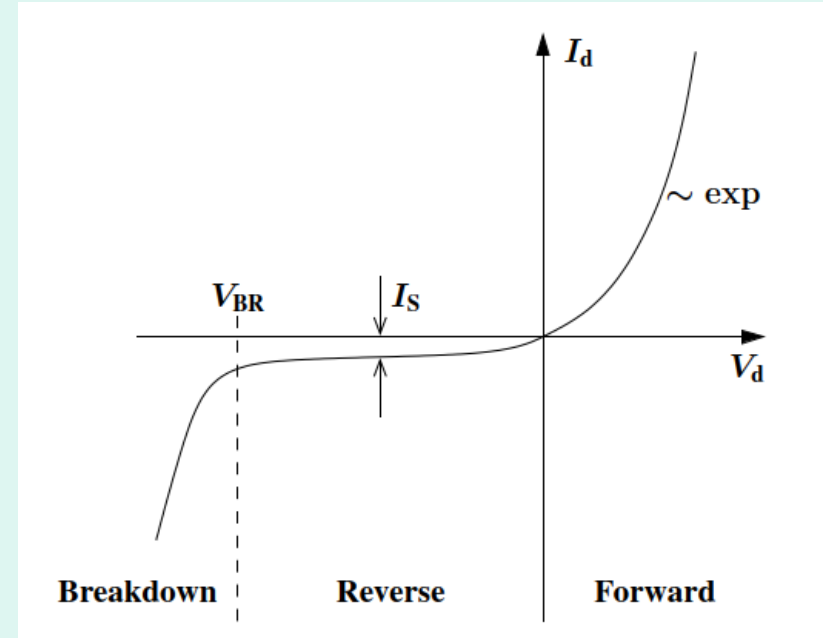
$$i_C = I_C + i_c$$



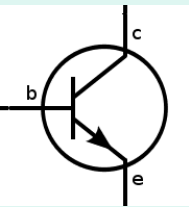


Diodes - recall

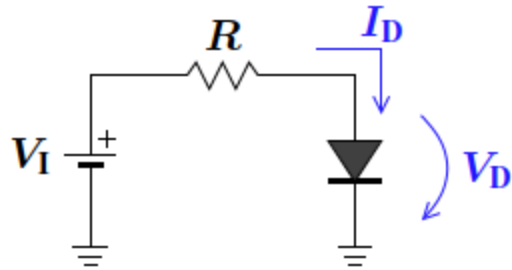
- Three operating regions:
 - Forward-bias region ($v_D > 0$)
 - Reverse-bias region ($V_{BR} < v_D < 0$)
 - Breakdown region ($v_D < V_{BR}$)
- Diode law (Shockley diode eqn.
 - I_S = reverse-bias saturation current
 - n = ideality factor (1..2)
 - $V_T = kT/q$ = thermal voltage



$$i_D = I_s \left(e^{v_D / nV_T} - 1 \right)$$



Biasing - quiescent point



$$\begin{cases} V_I = R \cdot I_D + V_D \\ I_D = I_S \exp \frac{V_D}{V_T} \end{cases} \rightarrow \begin{cases} \text{No closed-form solution} \\ \text{To be solved numerically} \end{cases}$$

- DC level biasing - (V_D, I_D) is called the quiescent point
- $V_D = V_T \ln(I_D/I_S) \approx 0.6..0.7\text{V}$ for a large range of currents

$$I_{D0} = \frac{V_I - 0.6\text{V}}{R}$$

$$V_{D0} = 0.6\text{V}$$

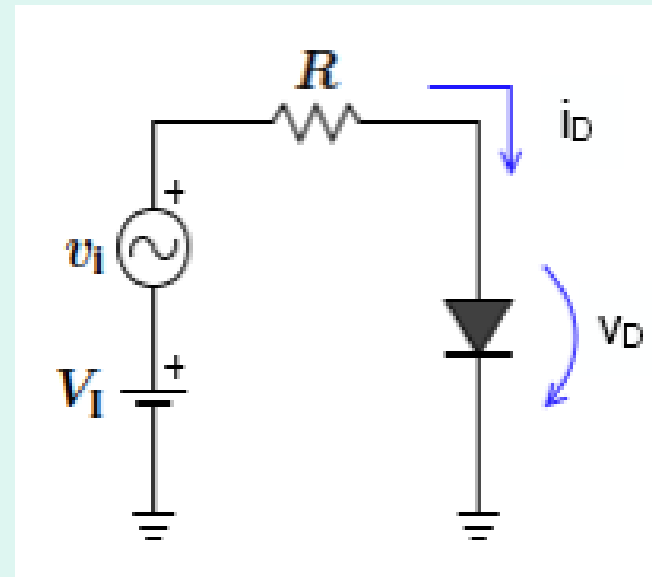


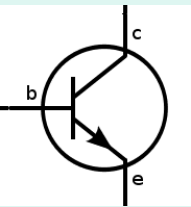
L10 Q01 - diode model

- Can we apply superposition to compute the total current through the circuit?

A. Yes

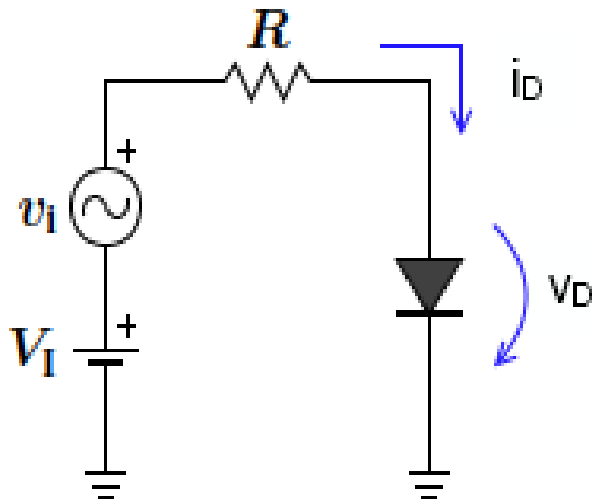
B. No





Diode - small signal model

- DC+ small AC voltages
- nonlinear circuit => no superposition!

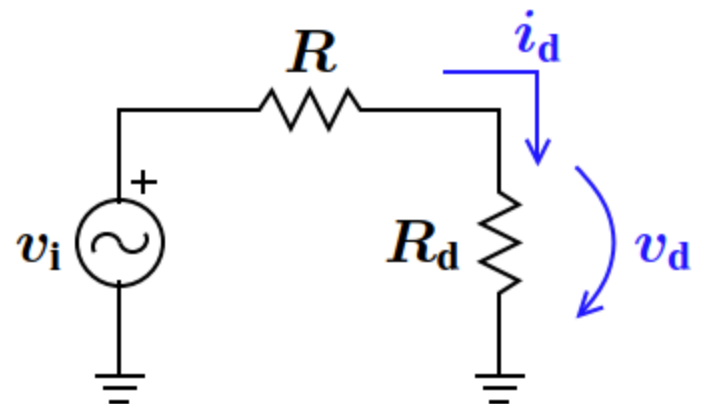


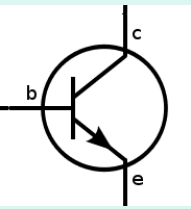
$$i_D = I_s \left(e^{v_D/V_T} - 1 \right) \approx I_s e^{\frac{V_D + v_d}{V_T}} = \underbrace{I_s e^{\frac{V_D}{V_T}}}_{I_D} e^{\frac{v_d}{V_T}} = I_D e^{\frac{v_d}{V_T}} \quad v_d \ll V_T \approx I_D \left(1 + \frac{v_d}{V_T} \right)$$

$$I_D + i_d \approx I_D \left(1 + \frac{v_d}{V_T} \right) \Rightarrow i_d \approx \frac{I_D}{V_T} v_d = \frac{v_d}{r_d}$$

$r_d = r_d(I_D)$ = dynamic resistance of the diode

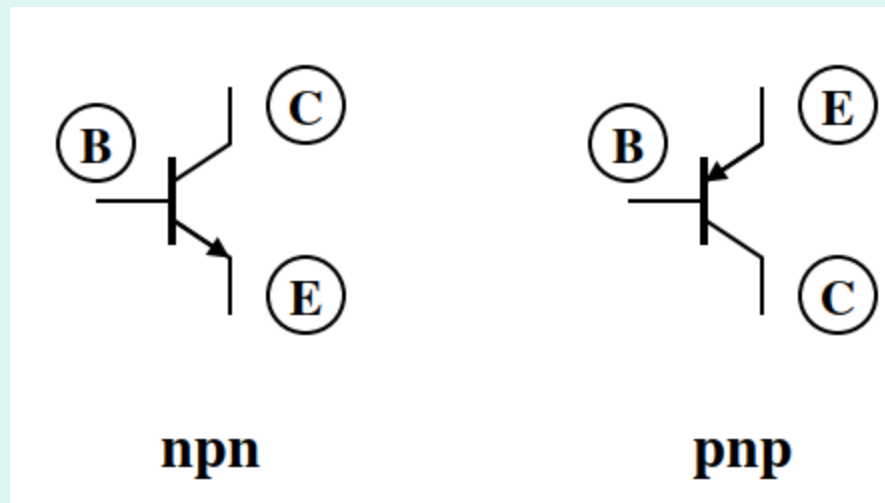
$$i_D = I_D + i_d \approx \frac{V_1 - 0.6V}{R} + \frac{v_i}{R + r_d}$$

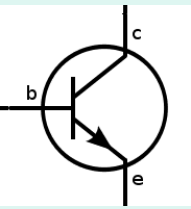




Bipolar junction transistors (BJTs)

- Two types: npn, pnp
- Three terminals: emitter, base, collector



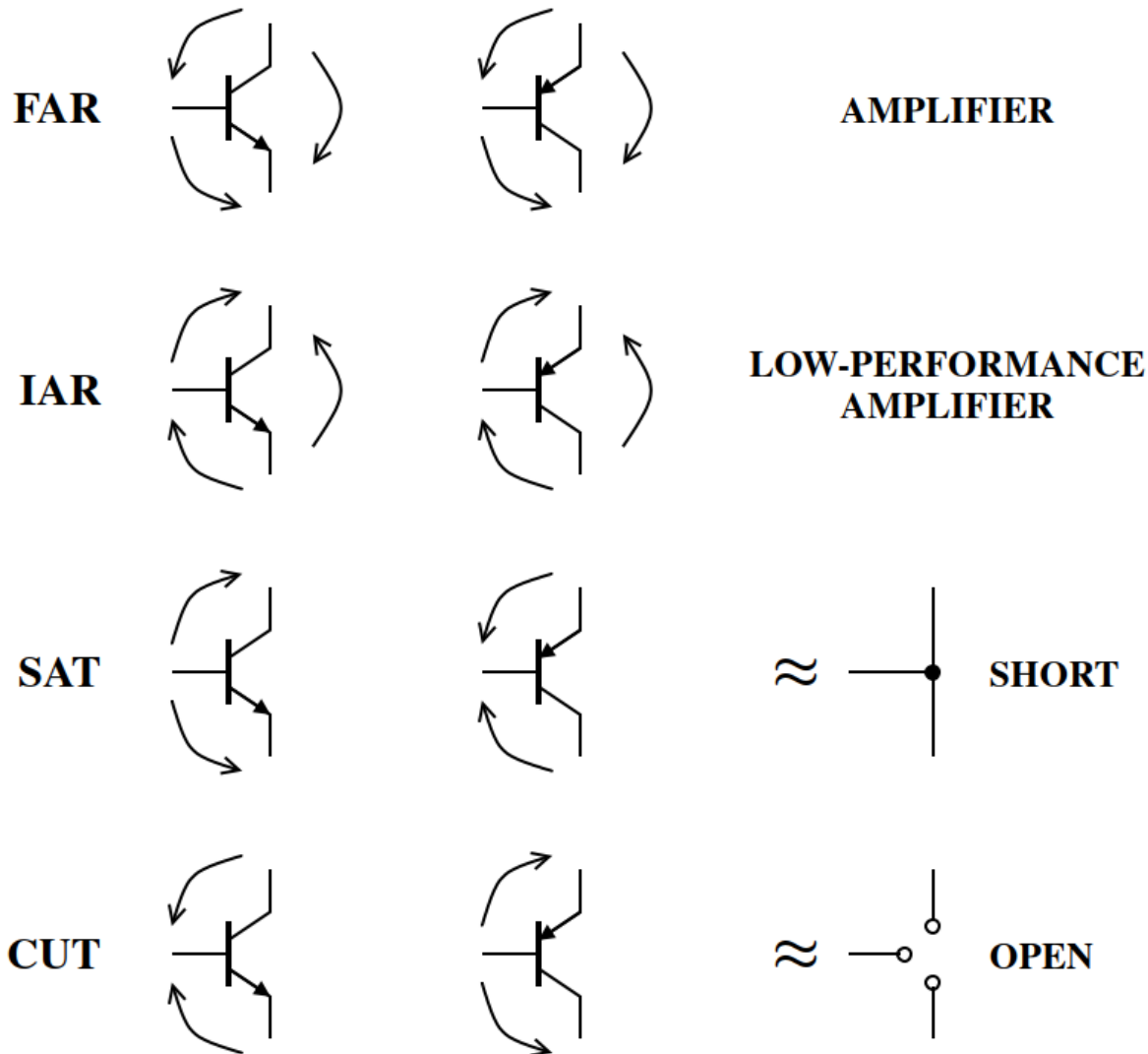


BJT operating modes

- Four transistor operating modes:
 - **Saturation** -- The transistor acts like a short circuit. Current freely flows from collector to emitter.
 - **Cut-off** -- The transistor acts like an open circuit. No current flows from collector to emitter.
 - **Active** -- The current from collector to emitter is proportional to the base current.
 - **Inverse-Active** -- Like active mode, the current is proportional to the base current, but it flows in reverse. Current flows from emitter to collector (not, exactly, the purpose transistors were designed for)



BJT operating modes



- FAR = forward active region
- IAR = inverse active region (poor β)
- SAT = saturation
- CUT = cut-off



BJT in active operating mode

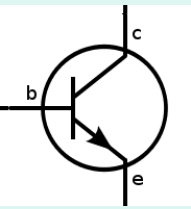
- EB junction must be forward biased ($V_{BE} \sim 0.6V$ for a npn transistor)
- CB junction must be reversed biased ($V_{CB} > 0V$ for npn)

- DC model:

$$i_C = I_C + i_c$$

$$I_C = \alpha I_E = \beta I_B$$

- α =common base current gain factor
- β =common emitter current gain factor
- V_T =thermal voltage (average thermal energy available to charge carriers)= $kT/q \sim 25mV$ at 25deg
- I_S = reverse saturation current



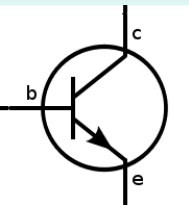
BJT DC model

$$I_E = I_B + I_C$$

$$I_C = \alpha I_E = \beta I_B$$

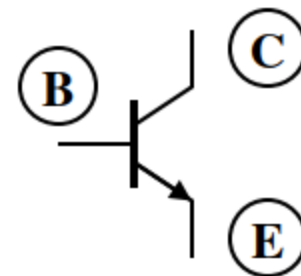
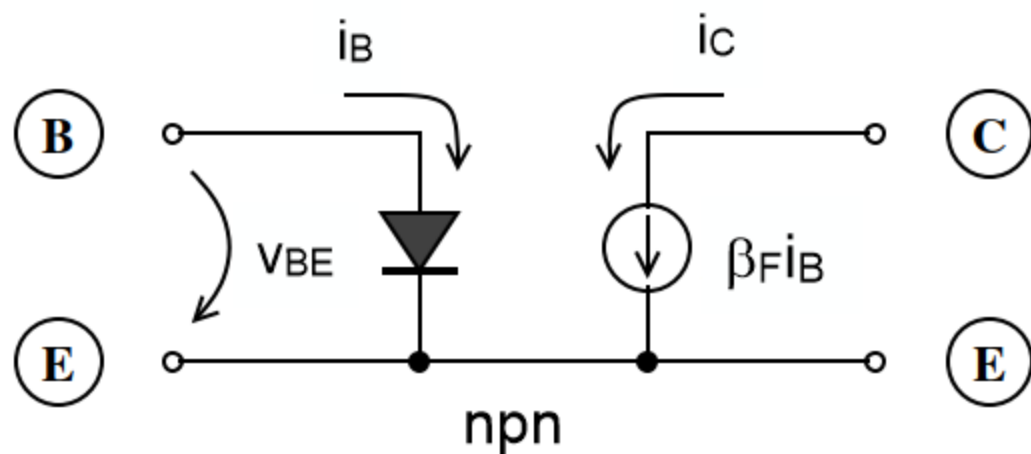
$$I_C = I_S e^{V_{BE}/V_T}$$

$$\alpha = \frac{\beta}{\beta + 1} \Leftrightarrow \beta = \frac{\alpha}{1 - \alpha}$$

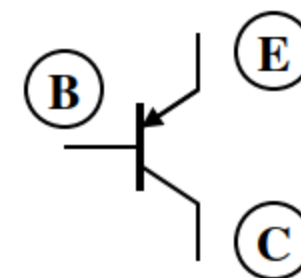
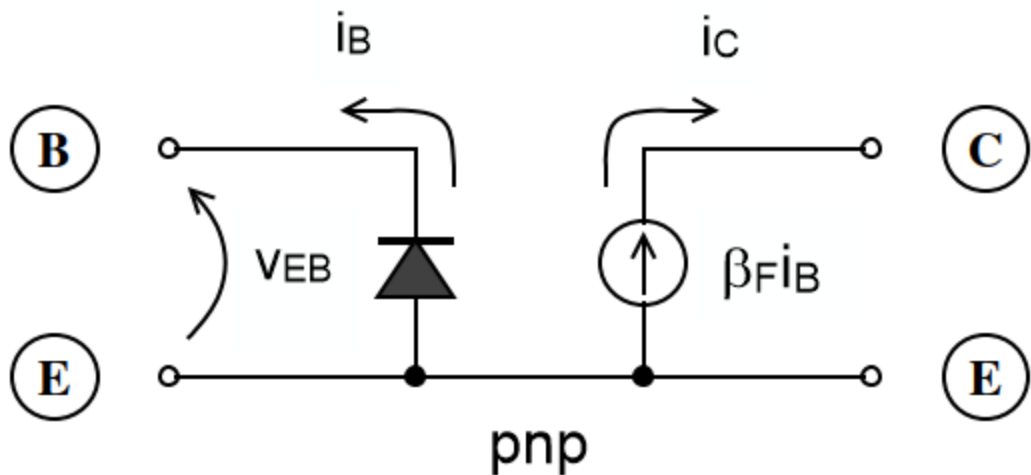


Large-signal model for BJT

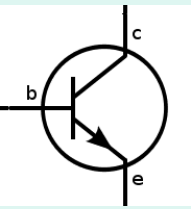
- REM: coupled junctions



$$i_C = I_S e^{\frac{v_{BE}}{V_T}}, i_B = \frac{I_S}{\beta} e^{\frac{v_{BE}}{V_T}}$$

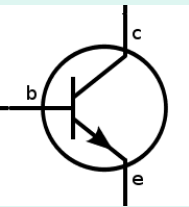


$$i_C = I_S e^{\frac{v_{EB}}{V_T}}, i_B = \frac{I_S}{\beta} e^{\frac{v_{EB}}{V_T}}$$



BJT parameters

- Saturation current: $I_S = 10^{-16} \dots 10^{-14} \text{ A}$
- Thermal voltage: $V_T = kt/q \approx 25 \text{ mV}$ at 25°C
- Forward current gain $\beta_F = \beta$ (assumed constant):
 - $\beta_{F, \text{nnp}} = 50 \dots 500$ (technology optimized for npn)
 - $\beta_{F, \text{pnp}} = 10 \dots 100$

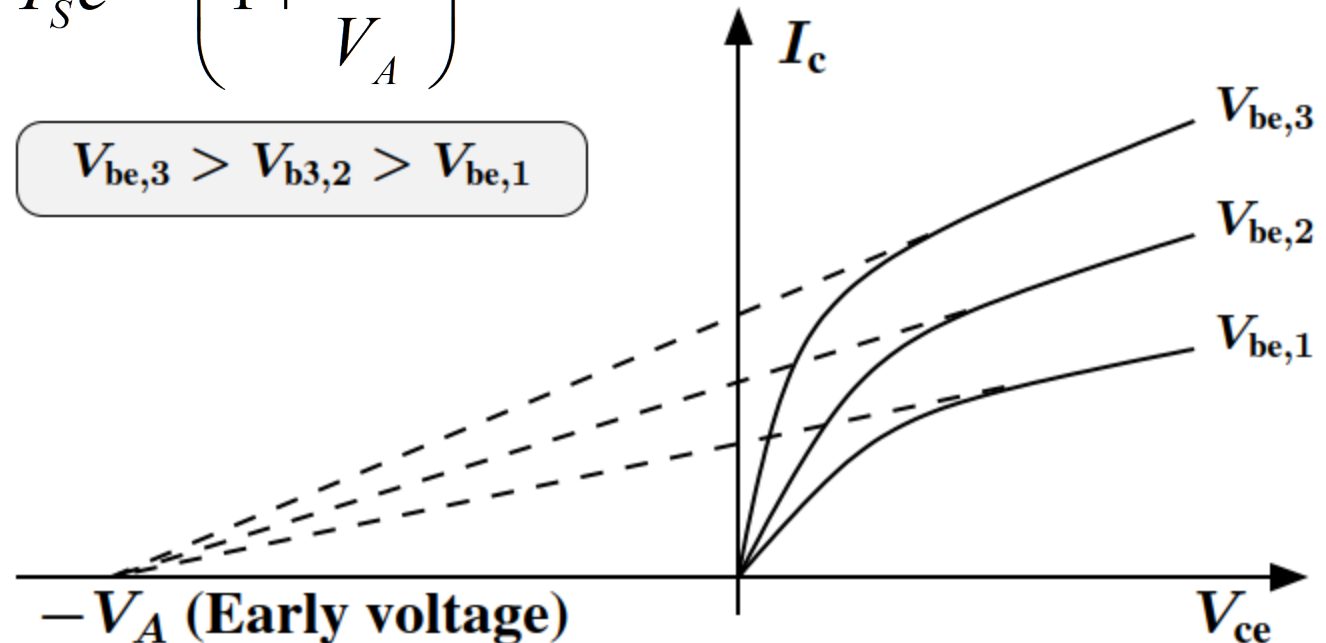


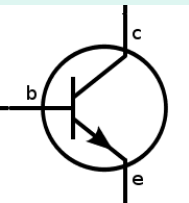
BJT current-voltage relations

- Early effect (discovered by James Early): $v_{CE} \nearrow \Rightarrow i_C \nearrow$
- Early voltage V_A - models the Early effect
- $V_{A,typ} = 50..100V$ (larger is better)

$$i_C = i_C(v_{BE}, v_{CE}) = I_S e^{\frac{v_{BE}}{V_T}} \left(1 + \frac{v_{CE}}{V_A} \right)$$

$$V_{be,3} > V_{b3,2} > V_{be,1}$$





Small variations around the DC bias values

- Consider a small variation v_{be} around the DC bias value V_{BE}

$$v_{BE} = V_{BE} + v_{be} \Rightarrow i_C = I_S e^{v_{BE}/V_T} = I_S e^{V_{BE}/V_T} e^{v_{be}/V_T} = I_C e^{v_{be}/V_T}$$

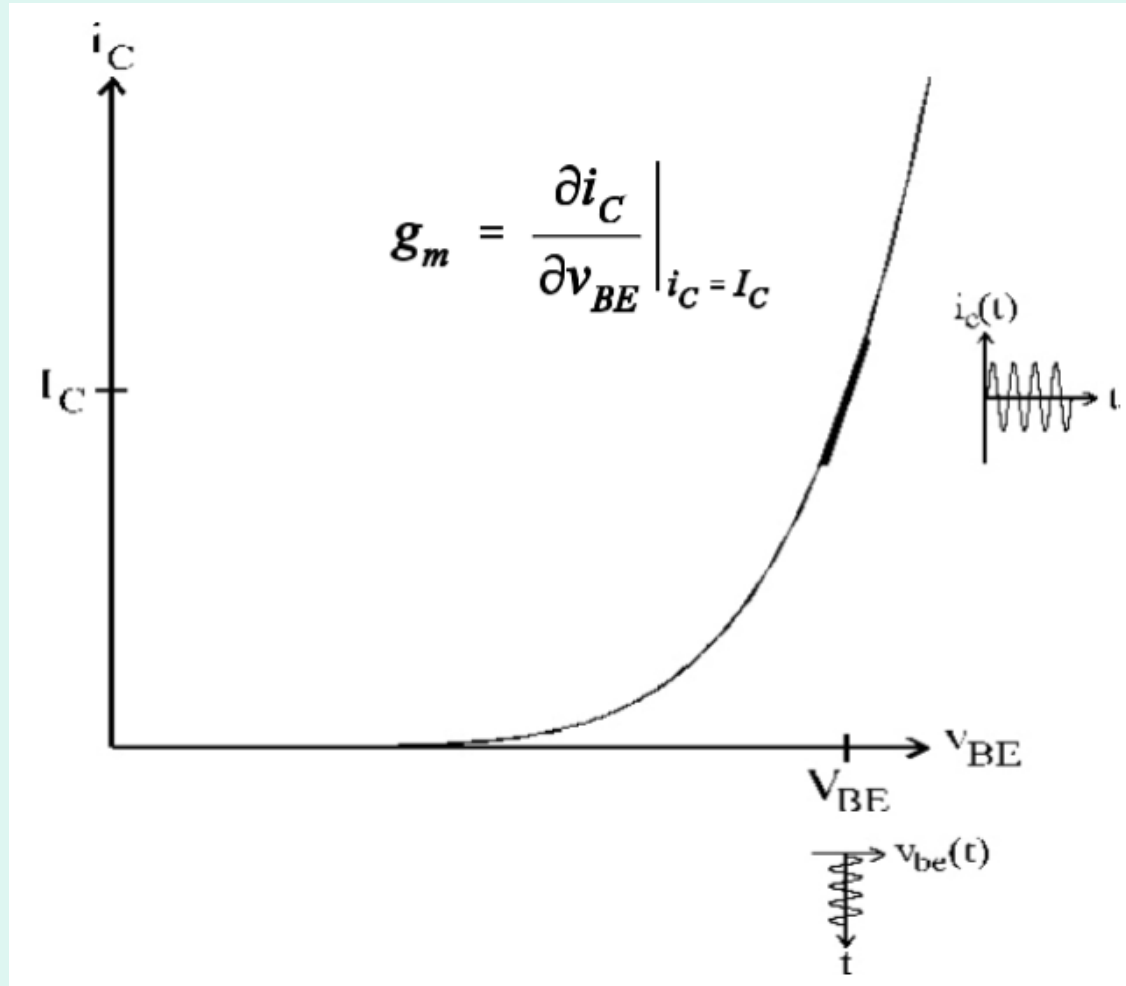
$$i_C = I_C + i_c \quad v_{be} \ll V_T \approx I_C \left(1 + \frac{v_{be}}{V_T} \right) = I_C + \frac{I_C}{V_T} v_{be}$$

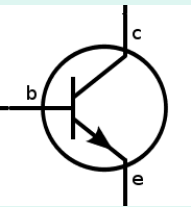
$$i_c = \underbrace{\frac{I_C}{V_T}}_{g_m} v_{be} \quad g_m = \text{small signal transconductance}$$



Transconductance g_m

- g_m = the slope of the $i_C(v_{BE})$ curve





BE input port

$$i_B = I_B + i_b = \frac{i_C}{\beta} = \frac{I_C + i_c}{\beta} = \frac{I_C}{\beta} + \frac{g_m}{\beta} v_{be} \Rightarrow i_b = \frac{g_m}{\beta} v_{be}$$

- Small-signal input resistance:

$$r_\pi = \frac{v_{be}}{i_{be}} = \frac{\beta}{g_m} = \beta \frac{V_T}{I_C} = \frac{V_T}{I_B}$$



Basic Hybrid- π model for BJT

- Small signal model without considering capacitive effects, nor the Early effect

