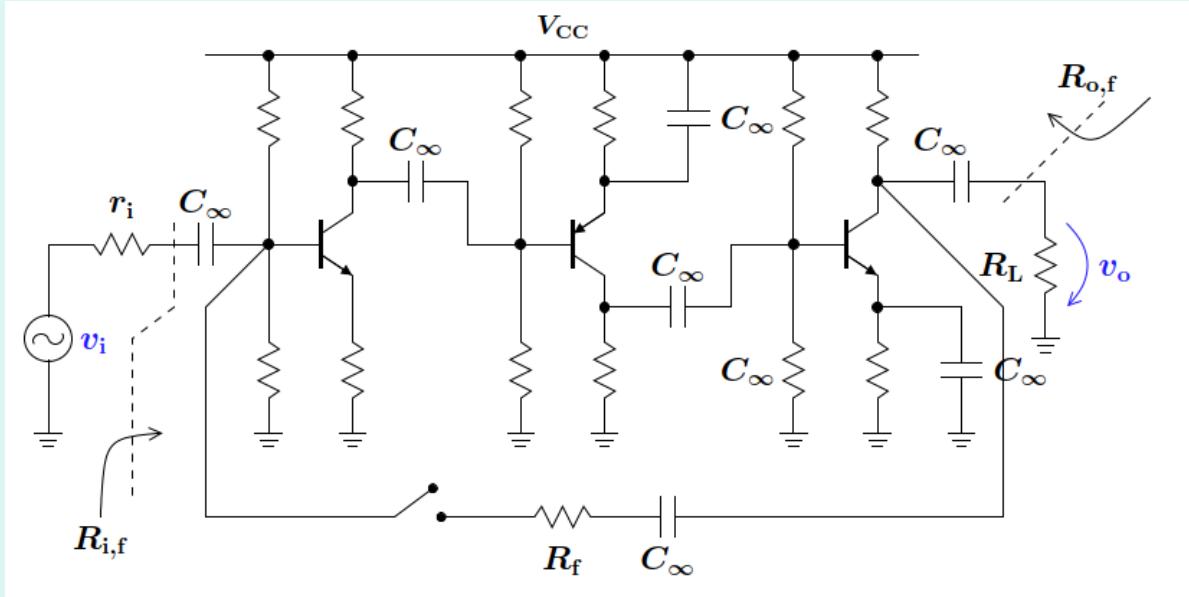
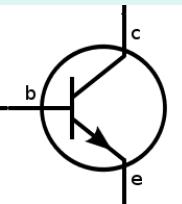


# ELEC 301 - Switched- capacitor filters

L33 - Dec 1, 2025

Instructor: Edmond Cretu

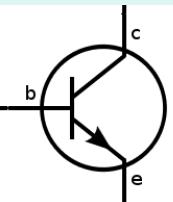




# Last time

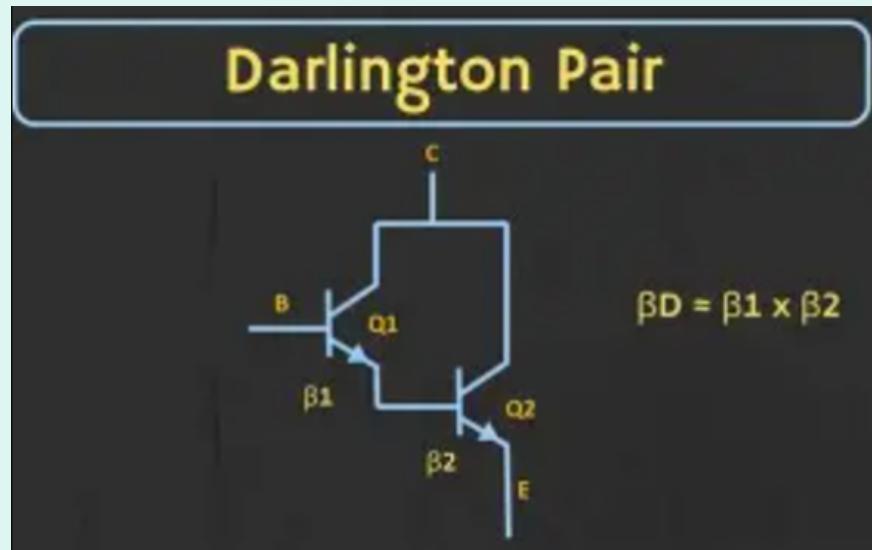
- Oscillators - design perspective, phase and gain conditions. frequency stability
- RLC oscillators
- Wien-bridge oscillators
- Amplitude control loop for oscillators

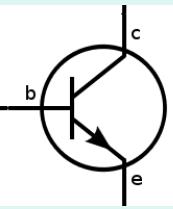




# History bits

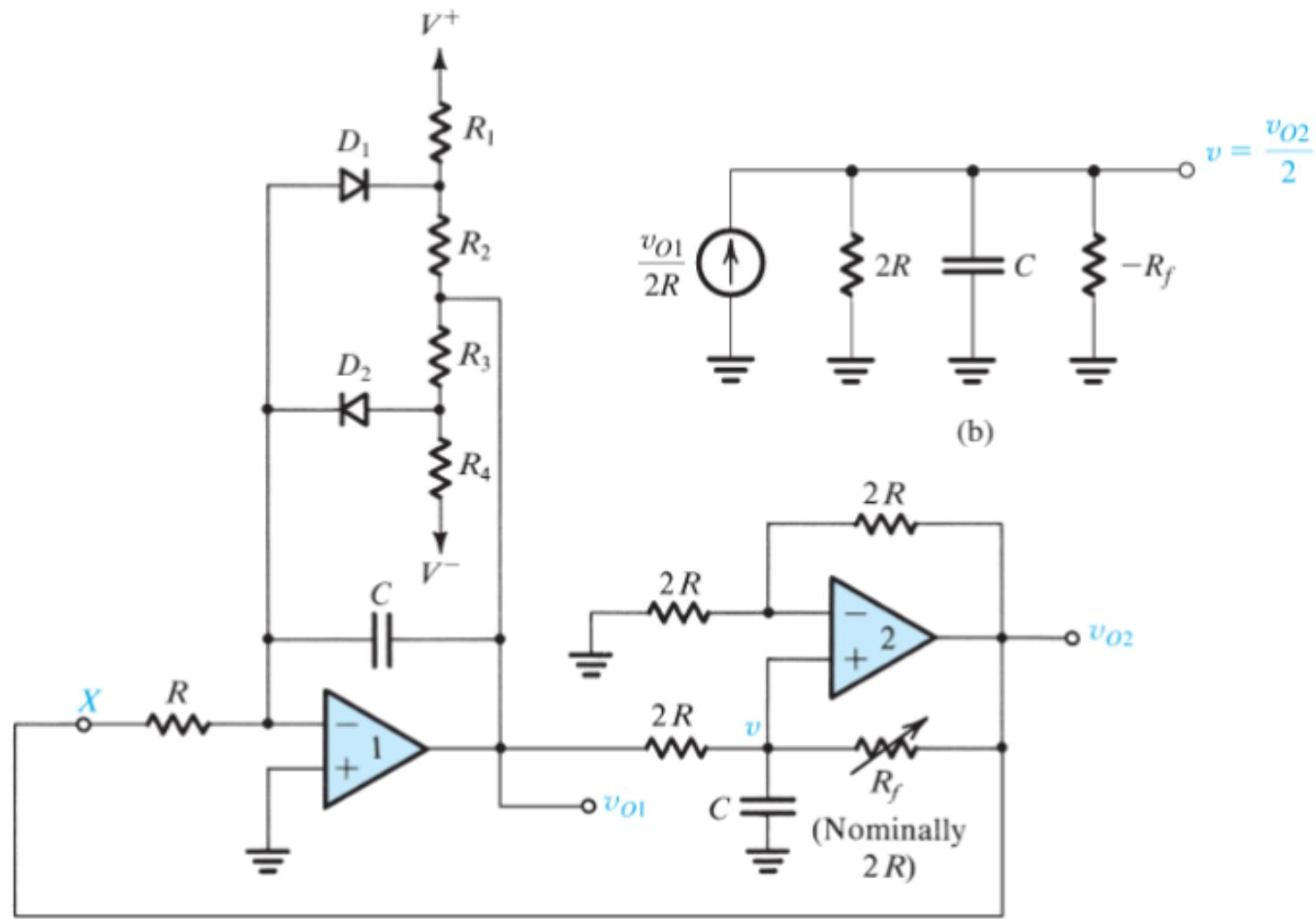
- Wilhelm Cauer (1900-1945) - used Chebyshev polynomials in an approach that unified the design of filters transfer functions + significant contributions to LC filter synthesis
- Sidney Darlington (1906-1997)- developed a complete design theory for LC filters, but better known for the transistor Darlington pair circuit

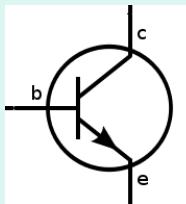




# Quadrature oscillator

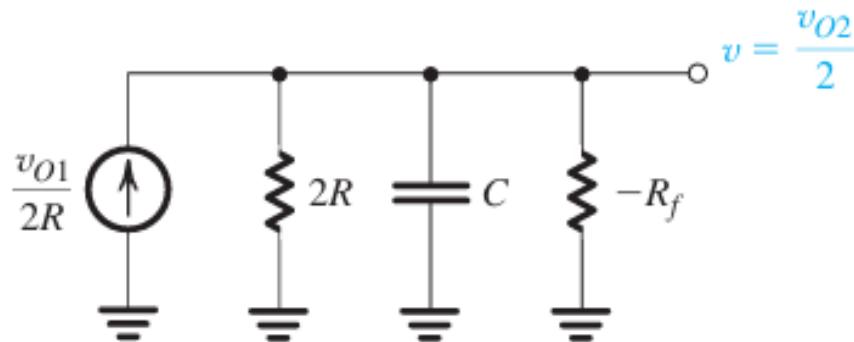
- Two op-amps - two series integrators: inverting integrator +non-inverting integrator





# Quadrature oscillator analysis

- equivalent model (linear region, no limiter)



$$\frac{v}{2} = \frac{v_{o2}}{2} \quad \frac{V_{o2}}{2} = \frac{V_{o1}}{2R} \frac{1}{sC} \Rightarrow V_{o2} = -\frac{V_x}{sRC} \frac{1}{sRC}$$

The loop gain:

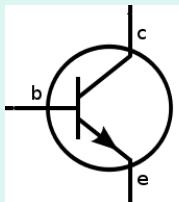
$$L(s) = \frac{V_{o2}}{V_x} = -\frac{1}{s^2 (RC)^2}$$

The oscillation frequency:

$$\omega_0 = \frac{1}{RC}$$

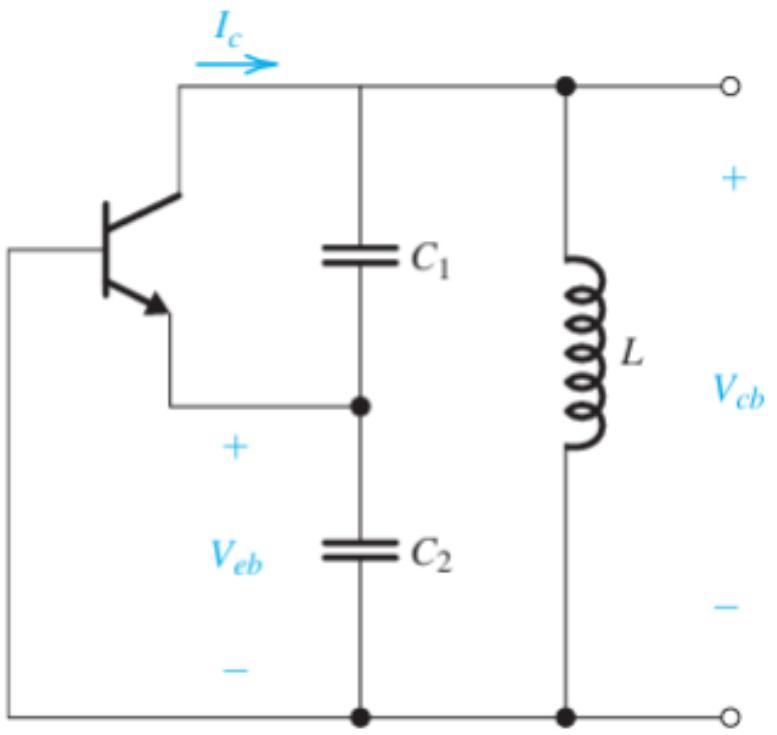
Remark:  $V_{o1}, V_{o2}$  have  $90^\circ$  phase shifts - used in many applications (e.g. Hilbert transform, quadrature modulation/demodulation)





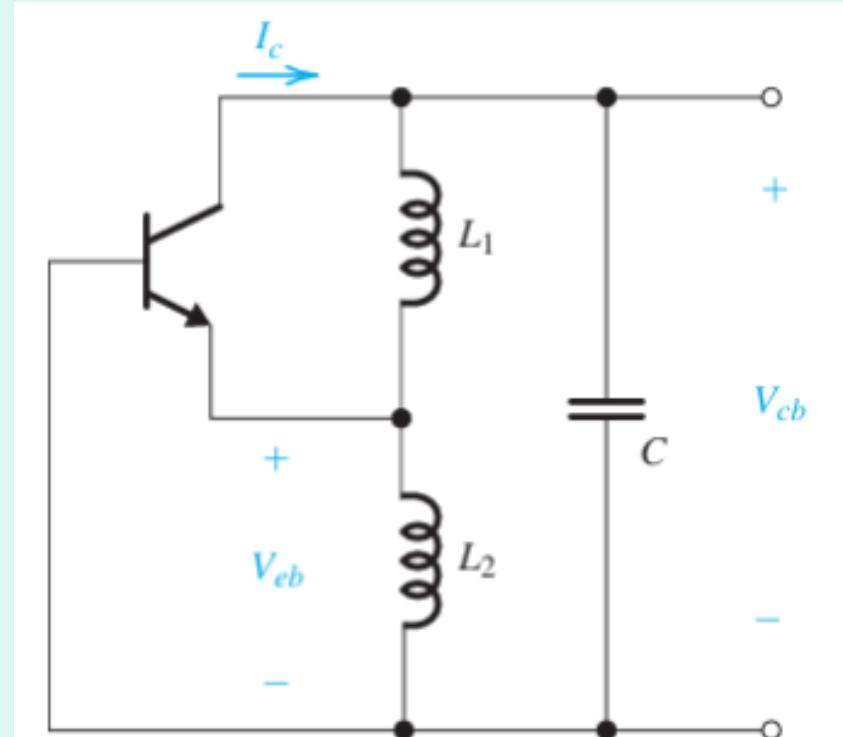
# LC oscillators

- Difficult to tune over wide ranges
- see ch. 18.13 in Sedra&Smith



Colpitts oscillator

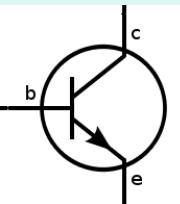
$$\omega_{0,Colpitts} = \frac{1}{\sqrt{L \frac{C_1 C_2}{C_1 + C_2}}}$$



Hartley oscillator

$$\omega_{0,Hartley} = \frac{1}{\sqrt{(L_1 + L_2)C}}$$

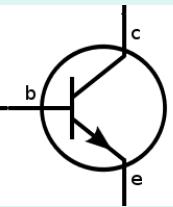




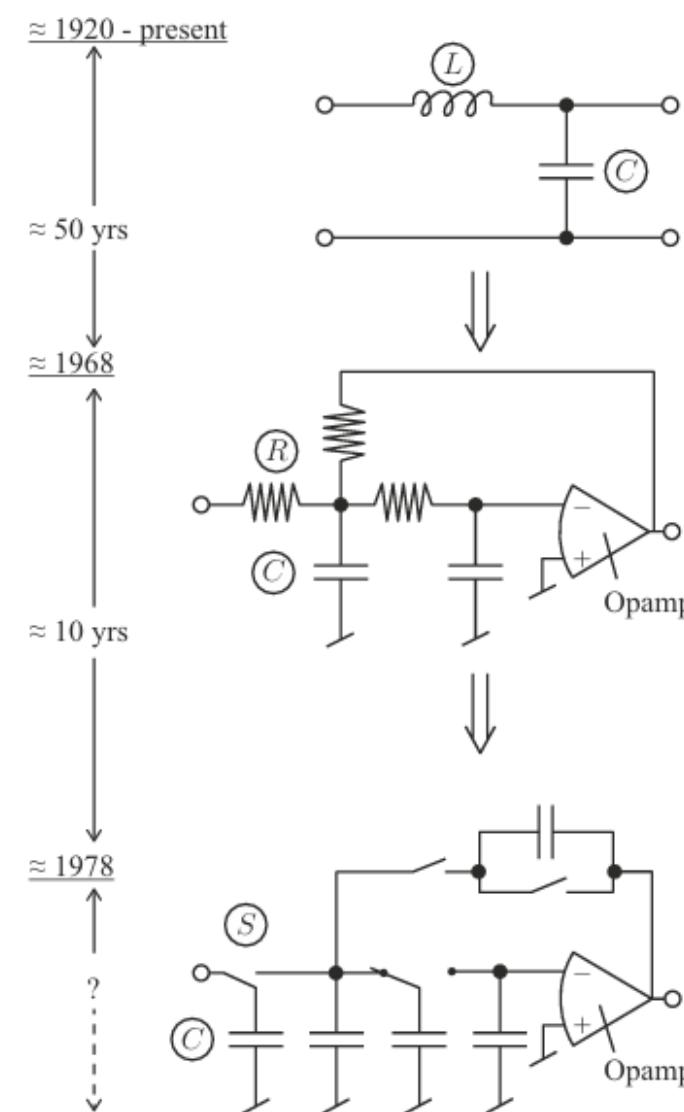
# Switched-capacitor circuits

- Goal: reduce IC area by avoiding large resistance
- Concept: mimic a large value resistance at a lower frequency by fast switching a capacitor at high frequency
- Discrete-time circuits, not continuous time filters
- Applications: audio filters (low-frequency filters) in CMOS technology (CMOS switches, op amps and small capacitors)





# Evolution of analog filters



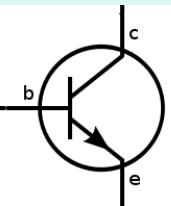
LC Filter  
Discrete  
Components

Active RC Filter  
Hybrid Integrated  
Circuit (Thin and  
Thick Film)

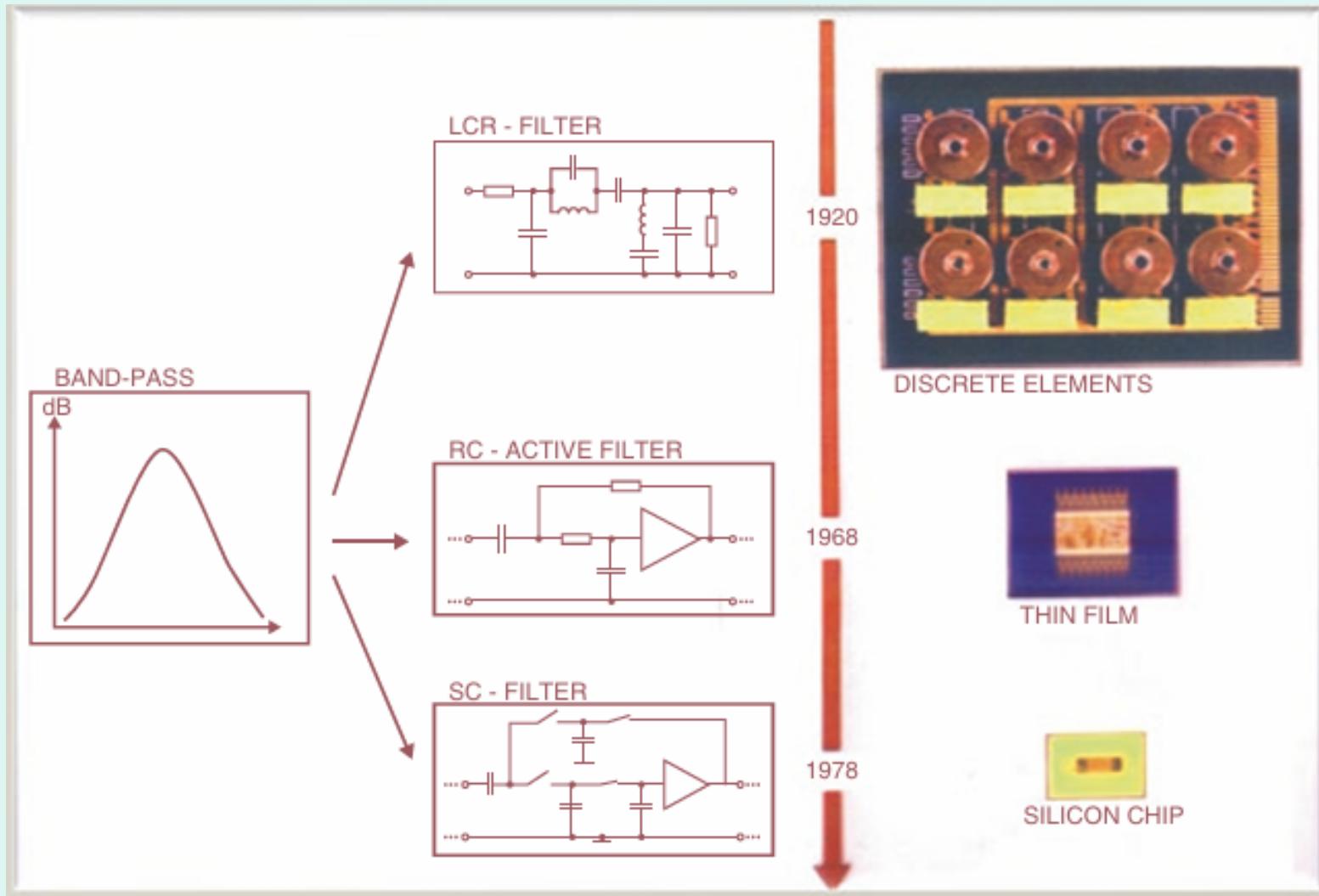
Switched-Capacitor  
(SC) Filter  
“Filter on a chip!”

Source: Moschytz[2019] Analog circuit theory and filter design



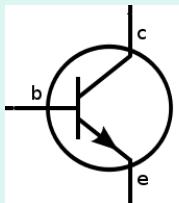


# Evolution of frequency-selective filters



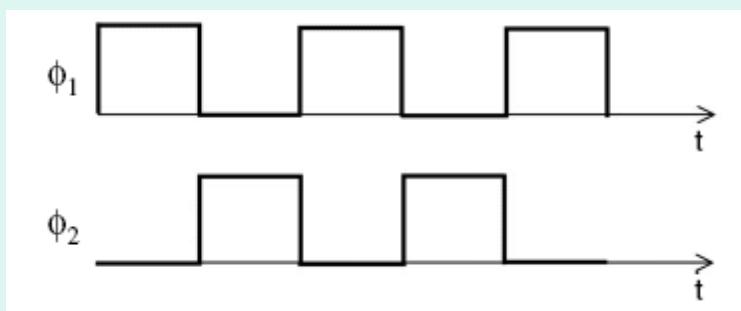
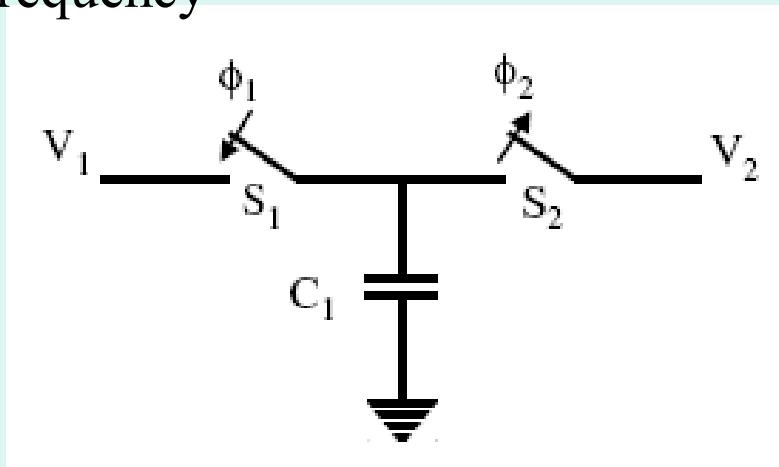
Source: Moschytz[2019]Analog circuit theory and filter design





# Switched-capacitor resistor

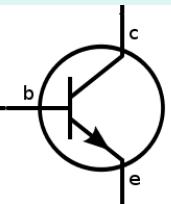
- Important: non-overlapping clock phases
- small  $C \Rightarrow$  large  $R_{eq,LF}$  + Equivalent resistance value changed by clock frequency



- Charge transfer from  $V_1$  to  $V_2$  as dictated by clock

$$i = \frac{\Delta Q}{\Delta t} = \frac{N \cdot C_1 (V_1 - V_2)}{\Delta t}$$

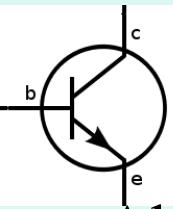
$$\Rightarrow R_{eq,LF} = \frac{V_1 - V_2}{i_{LF}} = \frac{1}{C_1 f_{clk}}$$



# Switched-capacitor (SC) circuits features

- Discrete-time interface - easier to interface with digital electronics
- Very suited to CMOS signal processing chain
- Transfer function depends on ratios of capacitors (not individual values)
- Filter frequency is tuned by changing the clock frequency of the SC circuit
- High-value resistors avoided
- Switches implemented with MOS transistors



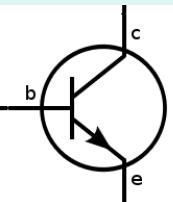


# SC resistor emulation circuits

- Alternative ways to mimic a LF resistor through charge transfer

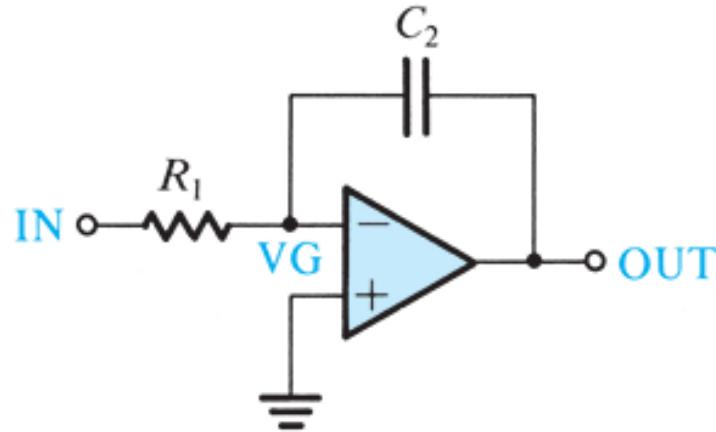
Circuit	Schematic	$R_{eq}$	$Q(\phi_1)$	$Q(\phi_2)$
Parallel		$\frac{T}{C}$	$V_{in}C$	$V_{out}C$
Series		$\frac{T}{C}$	0	$(V_{in} - V_{out})C$
Series-Parallel		$\frac{T}{C_1 + C_2}$	0	$(V_{in} - V_{out})C_1$
Bilinear		$\frac{1}{4} \frac{T}{C}$	$(V_{in} - V_{out})C$	$(V_{out} - V_{in})C$



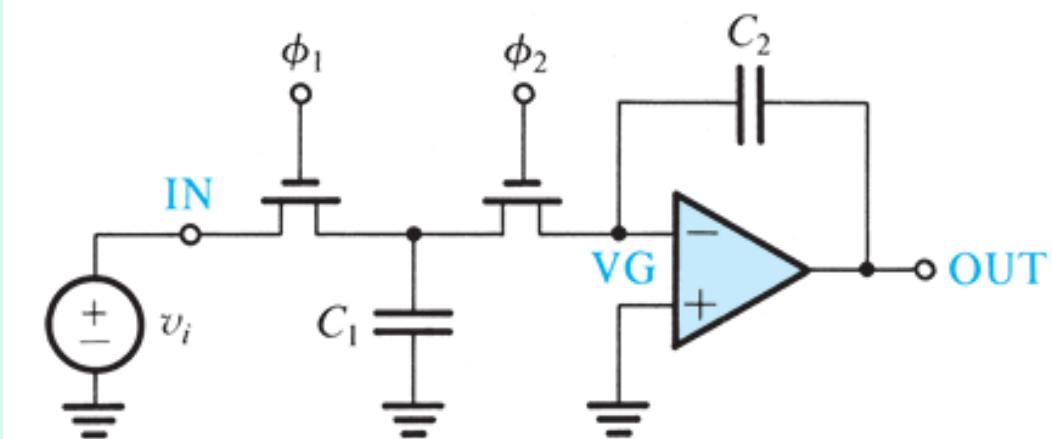


# Exm: integrator circuit

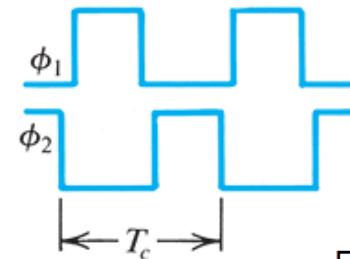
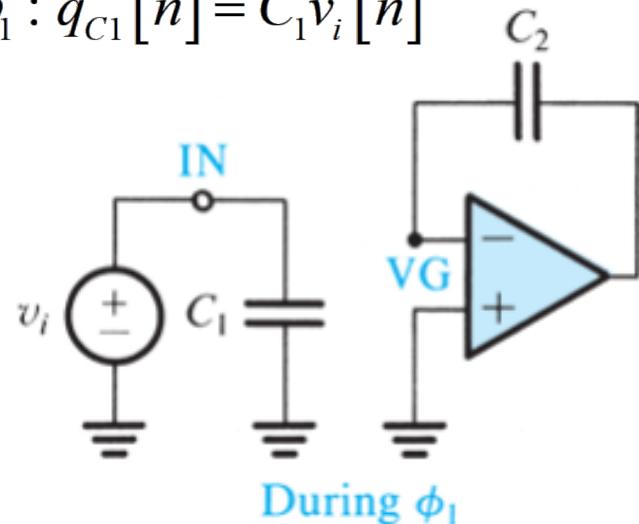
Continuous-time active integrator:



Switched-capacitor integrator ( $f_C \gg f_H$ ):

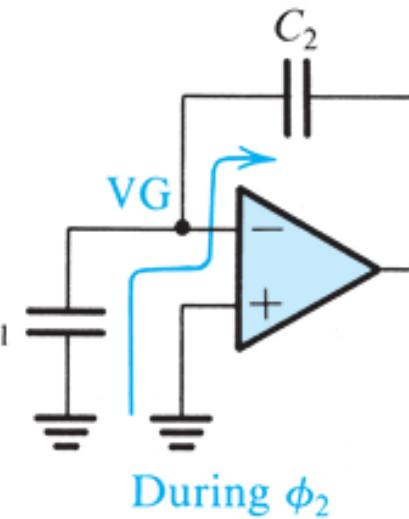


$$\varphi_1 : q_{C1}[n] = C_1 v_i[n]$$

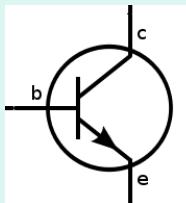


$$\varphi_2 : q_{C2}\left[n + \frac{1}{2}\right] = q_{C1}[n]$$

$$v_o\left[n + \frac{1}{2}\right] = v_o[n] - \frac{C_1}{C_2} v_i[n]$$



During  $\phi_2$



# Mapping back into CT

- The average current flowing between IN and the virtual ground (VG):

$$i_{av} = \frac{C_1 v_i}{T_c} = C_1 f_c v_i$$

If  $f_c \gg f_H$  (max frequency of the input analog voltage  $v_i$ ), then the equivalent LF resistance:

$$R_{eq} = \frac{1}{C_1 f_c}$$

Equivalent integrator time constant:

$$\tau = R_{eq} C_2 = \frac{C_2}{C_1} T_c$$

- Implementation aspects: the accuracy of capacitor ratios in IC technology  
 $C_2/C_1 \sim 0.1\%$  ( $C_1, C_2 \sim 0.05 \dots 100 \text{ pF}$ )
- with  $f_c \sim 100 \text{ kHz}$ ,  $C_2/C_1 \sim 10 \Rightarrow \tau \sim 10^{-4} \text{ s}$



