

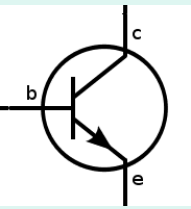


ELEC 301 - Switched- capacitor filters

L33 - Dec 1, 2025

Instructor: Edmond Cretu





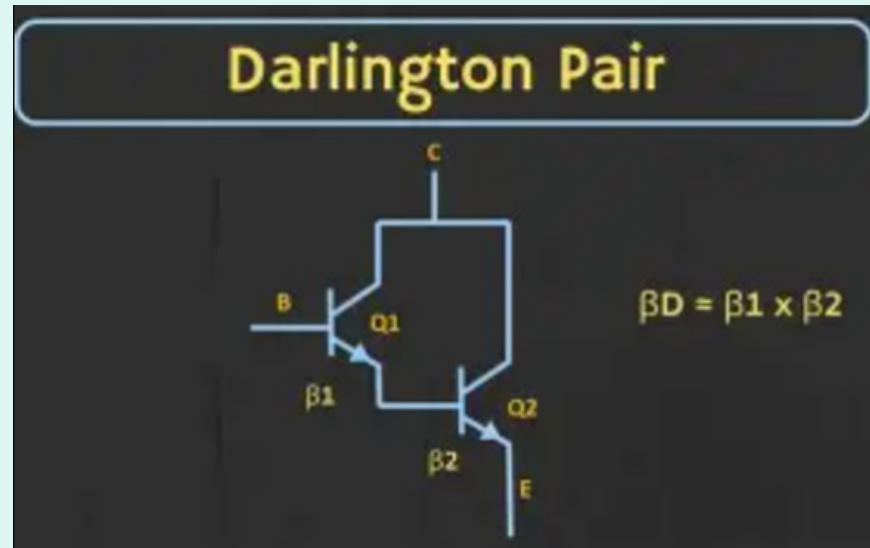
Last time

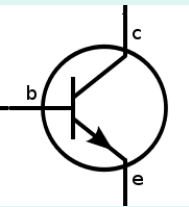
- Oscillators - design perspective, phase and gain conditions. frequency stability
- RLC oscillators
- Wien-bridge oscillators
- Amplitude control loop for oscillators



History bits

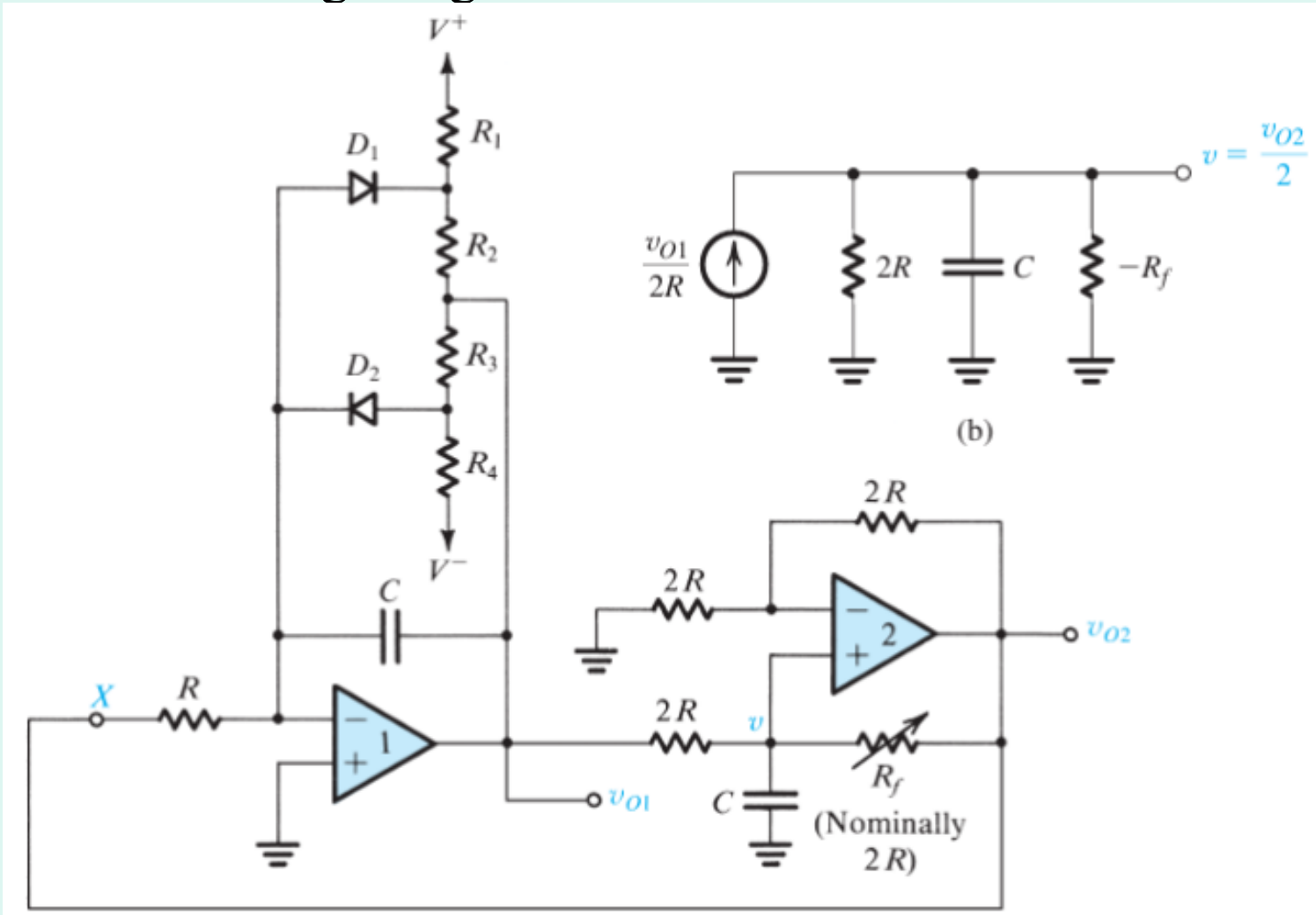
- Wilhelm Cauer (1900-1945) - used Chebyshev polynomials in an approach that unified the design of filters transfer functions + significant contributions to LC filter synthesis
- Sidney Darlington (1906-1997)- developed a complete design theory for LC filters, but better known for the transistor Darlington pair circuit





Quadrature oscillator

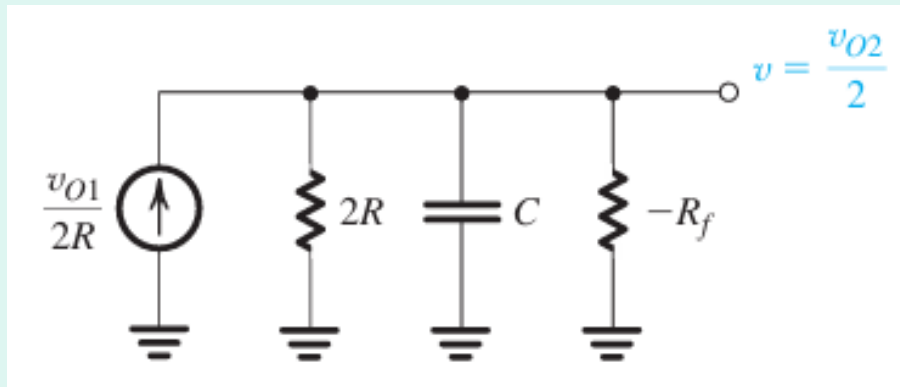
- Two op-amps - two series integrators: inverting integrator + non-inverting integrator





Quadrature oscillator analysis

- equivalent model (linear region, no limiter)



$$\frac{V_{o2}}{2} = \frac{V_{o1}}{2R} \frac{1}{sC} \Rightarrow V_{o2} = -\frac{V_x}{sRC} \frac{1}{sRC}$$

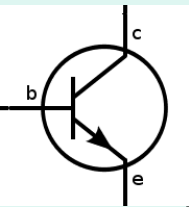
The loop gain:

$$L(s) = \frac{V_{o2}}{V_x} = -\frac{1}{s^2 (RC)^2}$$

The oscillation frequency:

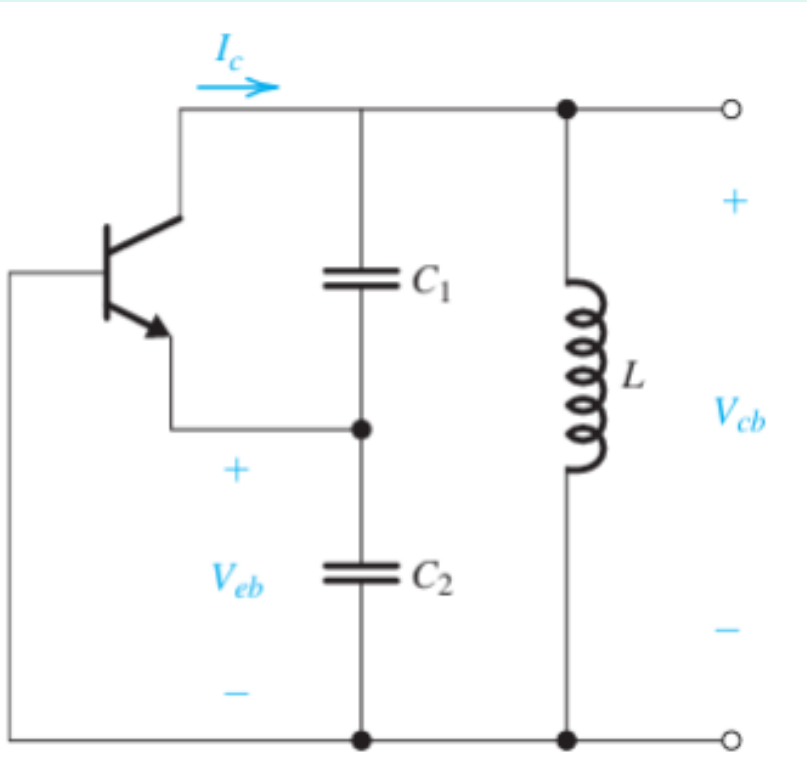
$$\omega_0 = \frac{1}{RC}$$

Remark: V_{o1} , V_{o2} have 90° phase shifts - used in many applications (e.g. Hilbert transform, quadrature modulation/demodulation)



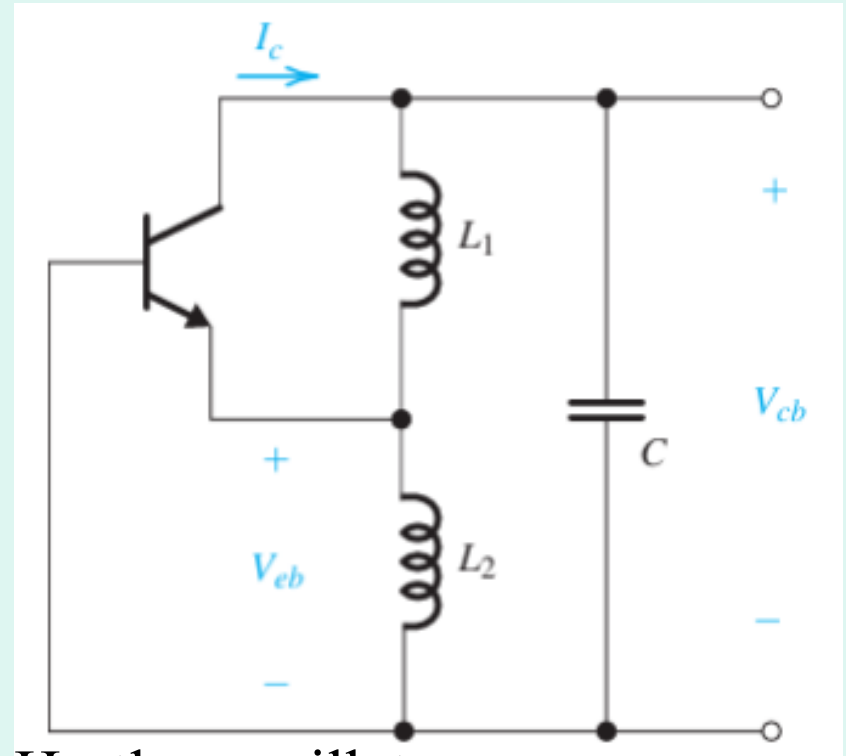
LC oscillators

- Difficult to tune over wide ranges
- see ch. 18.13 in Sedra&Smith



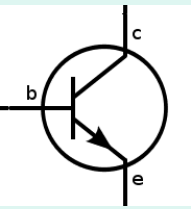
Colpitts oscillator

$$\omega_{0,Colpitts} = \frac{1}{\sqrt{L \frac{C_1 C_2}{C_1 + C_2}}}$$



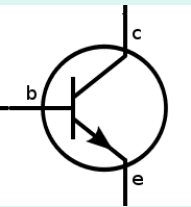
Hartley oscillator

$$\omega_{0,Hartley} = \frac{1}{\sqrt{(L_1 + L_2)C}}$$



Switched-capacitor circuits

- Goal: reduce IC area by avoiding large resistance
- Concept: mimic a large value resistance at a lower frequency by fast switching a capacitor at high frequency
- Discrete-time circuits, not continuous time filters
- Applications: audio filters (low-frequency filters) in CMOS technology (CMOS switches, op amps and small capacitors)



Evolution of analog filters

≈ 1920 - present

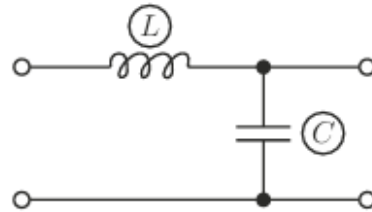
≈ 50 yrs

≈ 1968

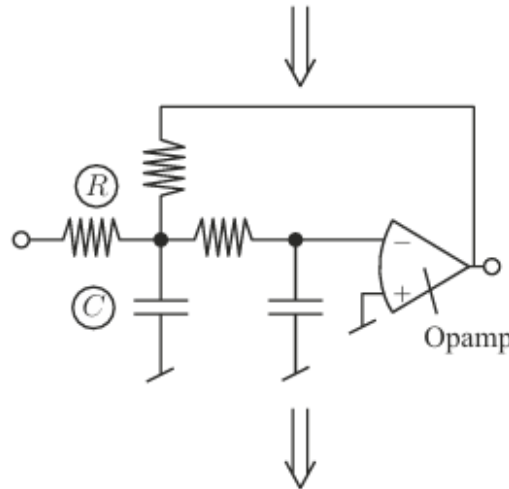
≈ 10 yrs

≈ 1978

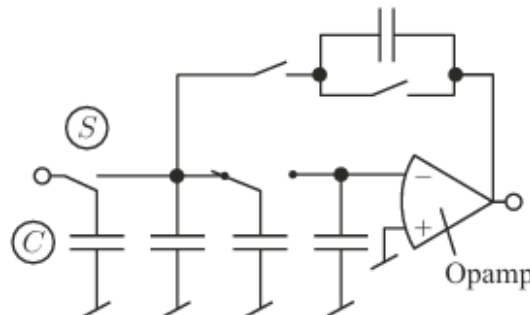
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LC Filter
Discrete
Components

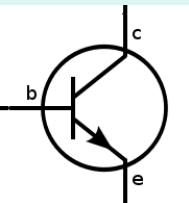


Active RC Filter
Hybrid Integrated
Circuit (Thin and
Thick Film)

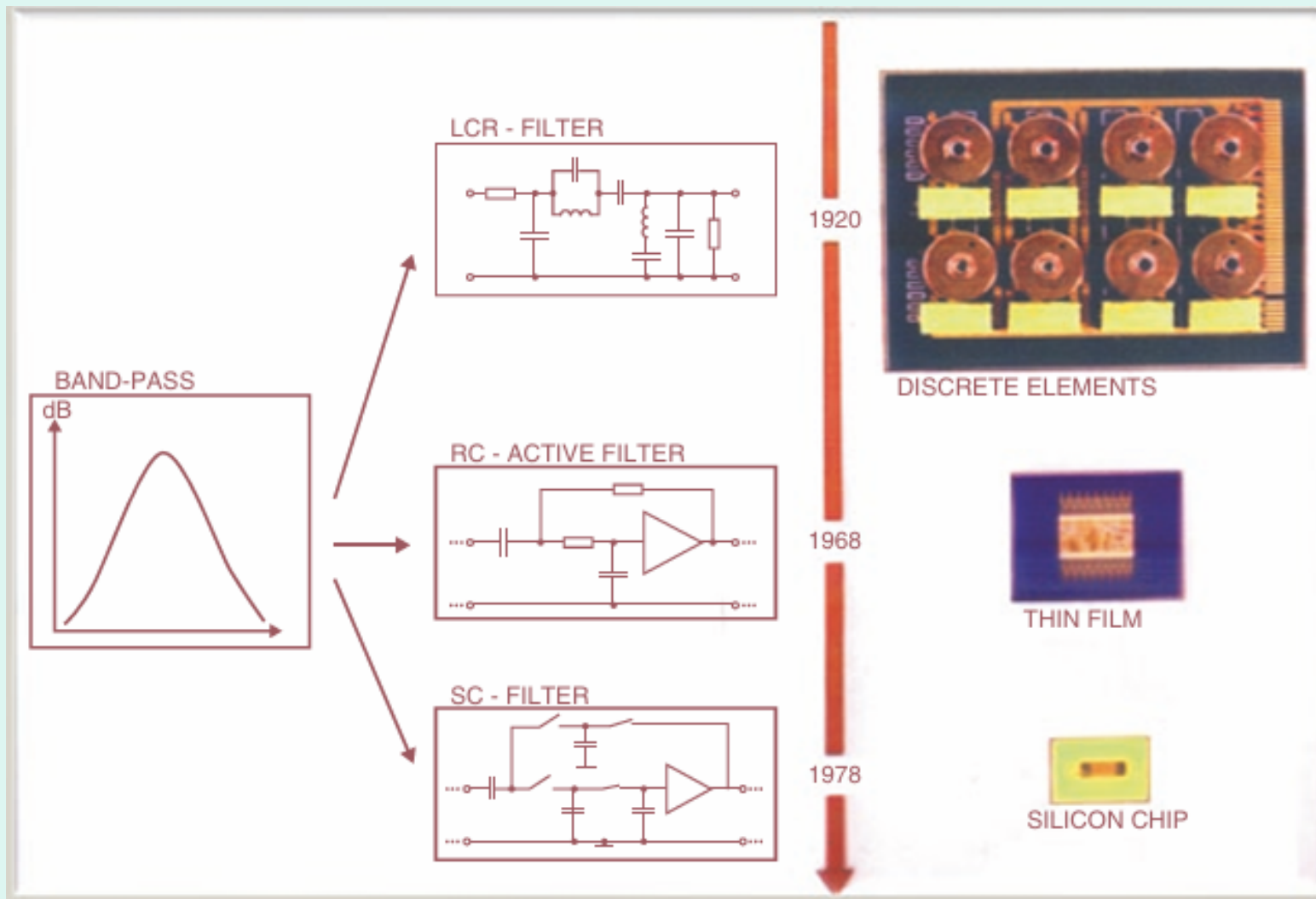


Switched-Capacitor
(SC) Filter
"Filter on a chip!"

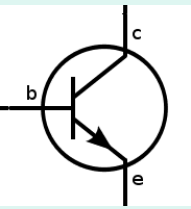
Source: Moschytz[2019]Analog circuit theory and filter design



Evolution of frequency-selective filters

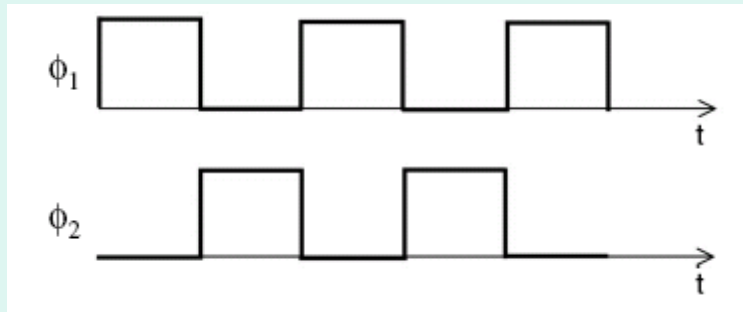
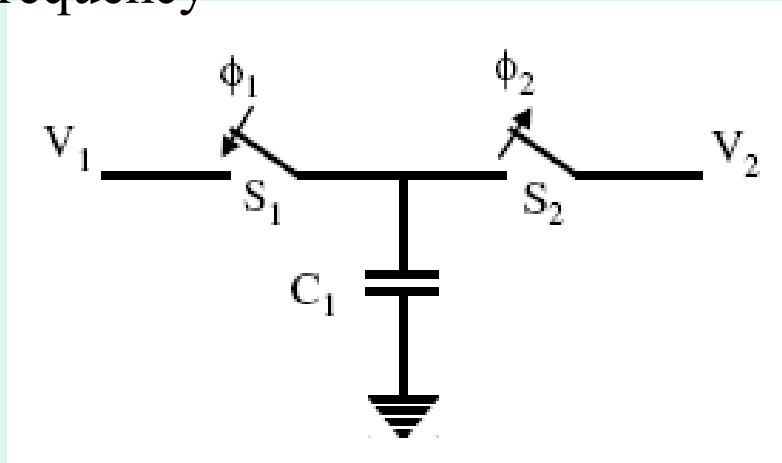


Source: Moschytz[2019]Analog circuit theory and filter design



Switched-capacitor resistor

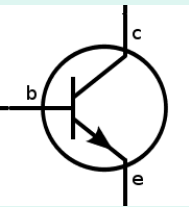
- Important: non-overlapping clock phases
- small $C \Rightarrow$ large $R_{eq,LF}$ + Equivalent resistance value changed by clock frequency



- Charge transfer from V_1 to V_2 as dictated by clock

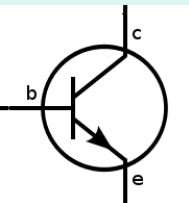
$$i = \frac{\Delta Q}{\Delta t} = \frac{N \cdot C_1 (V_1 - V_2)}{\Delta t}$$

$$\Rightarrow R_{eq,LF} = \frac{V_1 - V_2}{i_{LF}} = \frac{1}{C_1 f_{clk}}$$



Switched-capacitor (SC) circuits features

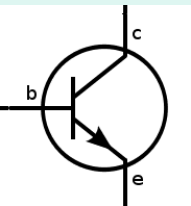
- Discrete-time interface - easier to interface with digital electronics
- Very suited to CMOS signal processing chain
- Transfer function depends on ratios of capacitors (not individual values)
- Filter frequency is tuned by changing the clock frequency of the SC circuit
- High-value resistors avoided
- Switches implemented with MOS transistors



SC resistor emulation circuits

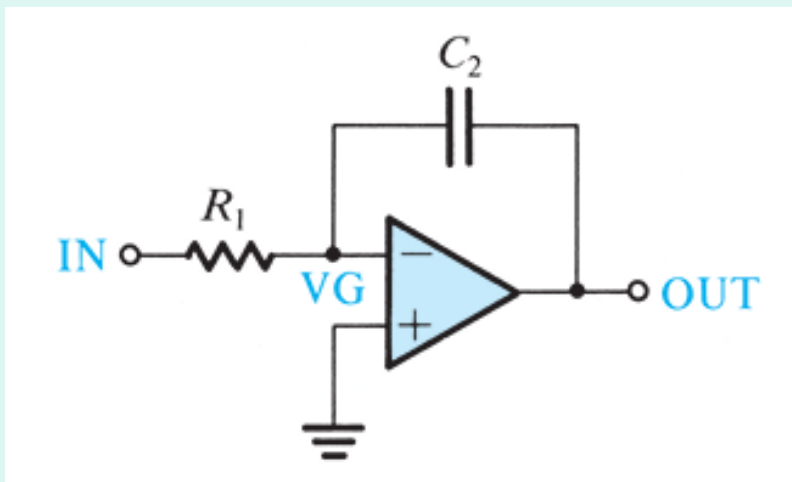
- Alternative ways to mimic a LF resistor through charge transfer

Circuit	Schematic	R_{eq}	$Q(\phi_1)$	$Q(\phi_2)$
Parallel		$\frac{T}{C}$	$V_{in}C$	$V_{out}C$
Series		$\frac{T}{C}$	0	$(V_{in} - V_{out})C$
Series-Parallel		$\frac{T}{C_1 + C_2}$	0	$(V_{in} - V_{out})C_1$ $V_{out}C_2$
Bilinear		$\frac{1}{4} \frac{T}{C}$	$(V_{in} - V_{out})C$	$(V_{out} - V_{in})C$

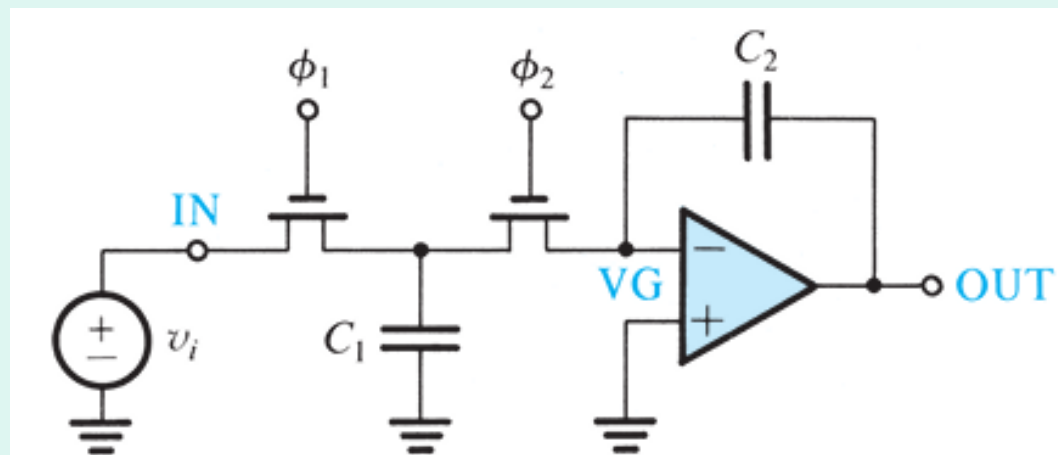


Exm: integrator circuit

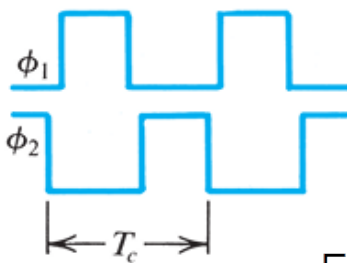
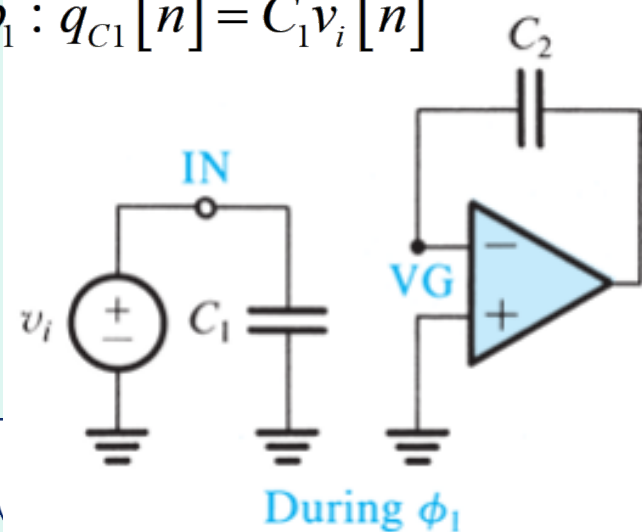
Continuous-time active integrator:



Switched-capacitor integrator ($f_C \gg f_H$):

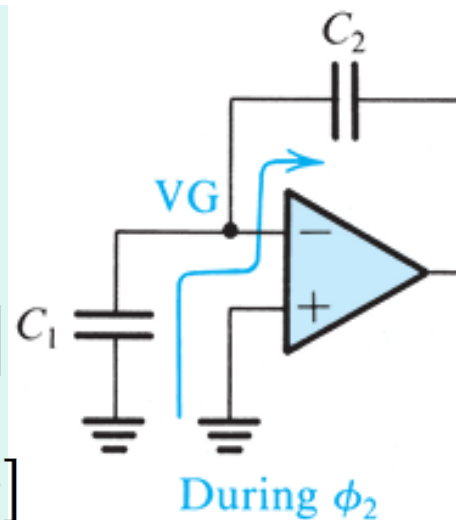


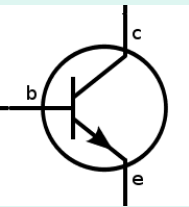
$$\phi_1 : q_{C1}[n] = C_1 v_i[n]$$



$$\phi_2 : q_{C2}\left[n + \frac{1}{2}\right] = q_{C1}[n]$$

$$v_o\left[n + \frac{1}{2}\right] = v_o[n] - \frac{C_1}{C_2} v_i[n]$$





Mapping back into CT

- The average current flowing between IN and the virtual ground (VG):

$$i_{av} = \frac{C_1 v_i}{T_c} = C_1 f_c v_i$$

If $f_c \gg f_H$ (max frequency of the input analog voltage v_i), then the equivalent LF resistance:

$$R_{eq} = \frac{1}{C_1 f_c}$$

Equivalent integrator time constant:

$$\tau = R_{eq} C_2 = \frac{C_2}{C_1} T_c$$

- Implementation aspects: the accuracy of capacitor ratios in IC technology
 $C_2/C_1 \sim 0.1\%$ ($C_1, C_2 \sim 0.05 \dots 100 \text{ pF}$)
- with $f_c \sim 100 \text{ kHz}$, $C_2/C_1 \sim 10 \Rightarrow \tau \sim 10^{-4} \text{ s}$

