

$$E_y = \epsilon_0 E_0 \sin(\omega t - \beta z)$$

$$\begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & E_y & 0 \end{vmatrix} = -\frac{\partial B}{\partial t}$$

Chapter 9 – Maxwell's Equations and Time-Varying Fields  
Chapter 10 – Transmission Lines

The purpose of this midterm exam is to assess your mastery of the fundamental techniques used to analyze transmission lines.

Answers should be short and to the point. Use sketches to explain your solution as required. Clarity, conciseness, and presentation all count. Solution = Intuition (strategy) + Execution (calculation). Make both explicit.

1.  $\mathbf{E} = E_0 \sin(\omega t - \beta z) \hat{y}$  in free space.  $E_0$  has units of volts per metre. Given Maxwell's equations in point form, find and give the name of the quantity, and the units of, and the expression for:

- a. D [5] ELECTRIC FLUX DENSITY (C/m<sup>2</sup>)

$$\mathbf{D} = \epsilon_0 \mathbf{E} = \epsilon_0 E_0 \sin(\omega t - \beta z) \hat{y} \quad \checkmark$$

- b. B [5] MAGNETIC FLUX DENSITY (WB/m<sup>2</sup> or T)

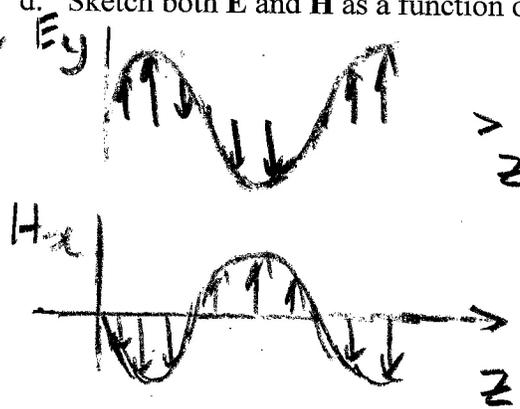
$$\mathbf{B} = -\frac{\beta E_0}{\omega} \sin(\omega t - \beta z) \hat{x}$$

- c. H [5] MAGNETIC FIELD STRENGTH (A/m)

$$\mathbf{H} = \frac{\mathbf{B}}{\mu_0} = -\frac{\beta E_0}{\omega \mu_0} \sin(\omega t - \beta z) \hat{x}$$

- d. Sketch both  $\mathbf{E}$  and  $\mathbf{H}$  as a function of  $z$  at the instant  $t = 0$ . [10]

FOR THE WAVE TO PROPAGATE IN THE +z DIRECTION,  
 $E_y \times -H_x = S_z$



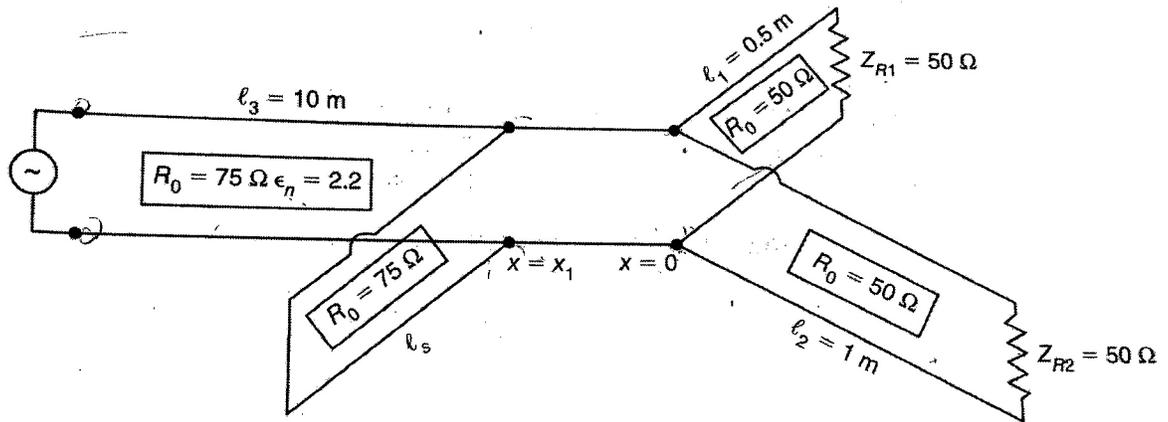
$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\mathbf{B} = -\int \frac{\partial \mathbf{B}}{\partial t} dt$$

BECAUSE THE FIELDS ARE TIME HARMONIC,  $C = 0$ .



3. A 0.15 GHz signal is applied to a 10-m-long 75-Ω coaxial line terminated in a composite load consisting of the parallel connection of two 50-Ω lines of lengths 0.5 m and 1 m, each terminated in a 50-Ω resistance. All lines are lossless with  $\epsilon_r = 2.2$ . See the figure below.



- a. Find the phase velocity and wavelength on the main feedline. [5]

$$v_p = \frac{c}{\sqrt{2.2}} = 2.02 \times 10^8 \text{ m/s} \quad \lambda = \frac{v_p}{f} = 1.35 \text{ m}$$

- b. Find the effective load impedance at  $x = 0$ . [5]

$$Z_L = 25 \Omega \quad \beta L = 0.3 = \frac{Z_L}{Z_0}$$

- c. Use a Smith Chart to determine the length  $l_s$  of a shunt short-circuit stub that will produce minimum VSWR on the feed line. The stub should be as close as possible to the load. [5]

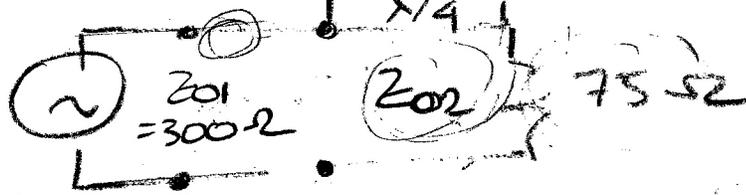
$$x_1 = 0.3325 - 0.25 \lambda = 0.0835 \lambda = 0.1127 \text{ m}$$

- d. Use a Smith Chart to determine the connection point  $x_1$  of a shunt short-circuit stub that will produce minimum VSWR on the feed line. The stub should be as short as possible. [5]

$$l_s = (0.25 + 0.1345 \lambda) = 0.3845 \lambda = 0.519 \text{ cm}$$

- e. What are the two main disadvantages of a single-stub matching network? [5]

- ONLY WORKS AT A SINGLE FREQUENCY
- MAY BE DIFFICULT TO ATTACH A STUB TO THE TRANSMISSION LINE AT AN ARBITRARY DISTANCE, PARTICULARLY IF THE TRANSMISSION LINE IS A COAXIAL CABLE



4. A quarter-wave section of transmission line is used to match a  $75\text{-}\Omega$  load to a  $300\text{-}\Omega$  transmission line. Use a Smith Chart to determine:

a. The characteristic impedance of the quarter-wave section. [5]

$$Z_0 = \sqrt{Z_L Z_{in}} = \sqrt{75 \times 300} = 150 \Omega$$

EXPLANATION:  $\frac{Z_L}{Z_0}$  must equal  $\frac{Z_0}{Z_{in}} = \frac{1}{\frac{Z_{in}}{Z_0}}$

b. The VSWR on the quarter-wave section. [5]

$$S = \frac{1 + |\Gamma|}{1 - |\Gamma|} = \frac{1.333}{0.666} = 2 = \frac{V_{max}}{V_{min}} = \text{VSWR}$$

$$|\Gamma| = 0.333$$

c. The voltage reflection coefficient on the quarter-wave section [5]

$$\Gamma(z) = \Gamma_0 e^{j2\beta z} = -0.333 e^{j(2 \cdot \frac{2\pi}{\lambda} \cdot z)} = -0.333 e^{j\frac{4\pi z}{\lambda}}$$

d. The reflection coefficient at the load. [5]

$$\Gamma_0 = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{75 - 300}{75 + 300} = \frac{-225}{375} = -\frac{1}{3} = -0.333$$

e. What are the principal advantages and disadvantages of this matching technique? [5]

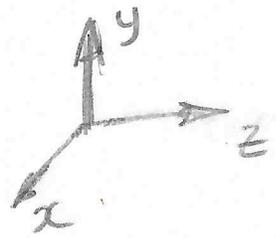
### ADVANTAGES

- COMPACT
- A SOLUTION ALWAYS EXISTS

### DISADVANTAGES

- ONLY WORKS AT THE DESIGN FREQ.
- PERFORMANCE DEGRADATES AWAY FROM THE DESIGN FREQ.
- MAY NEED A CUSTOM BUILT MATCHING SECTION

$$\beta = \frac{2\pi}{\lambda}$$



$$E_y = \epsilon_0 E_0 \sin(\omega t - \beta z)$$

$$\begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & E_y & 0 \end{vmatrix} = -\frac{\partial B}{\partial t}$$

The purpose of this midterm exam is to assess your mastery of the fundamental techniques used to analyze transmission lines.

Answers should be short and to the point. Use sketches to explain your solution as required. Clarity, conciseness, and presentation all count. Solution = Intuition (strategy) + Execution (calculation). Make both explicit.

1.  $\mathbf{E} = E_0 \sin(\omega t - \beta z) \hat{y}$  in free space.  $E_0$  has units of volts per metre. Given Maxwell's equations in point form, find and give the name of the quantity, and the units of, and the expression for:

- a. **D** [5] ELECTRIC FLUX DENSITY (C/m<sup>2</sup>)

$$\mathbf{D} = \epsilon_0 \mathbf{E} = \epsilon_0 E_0 \sin(\omega t - \beta z) \hat{y} \quad \checkmark$$

- b. **B** [5] MAGNETIC FLUX DENSITY (WB/m<sup>2</sup> or T)

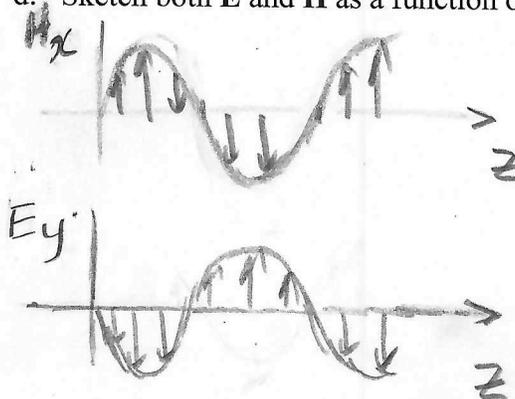
$$\mathbf{B} = -\frac{\beta E_0}{\omega} \sin(\omega t - \beta z) \hat{x}$$

- c. **H** [5] MAGNETIC FIELD STRENGTH (A/m)

$$\mathbf{H} = \frac{\mathbf{B}}{\mu_0} = -\frac{\beta E_0}{\omega \mu_0} \sin(\omega t - \beta z) \hat{x}$$

- d. Sketch both  $\mathbf{E}$  and  $\mathbf{H}$  as a function of  $z$  at the instant  $t = 0$ . [10]

FOR THE WAVE TO PROPAGATE IN THE +z DIRECTION,  
 $E_y \times -H_x = S_z$



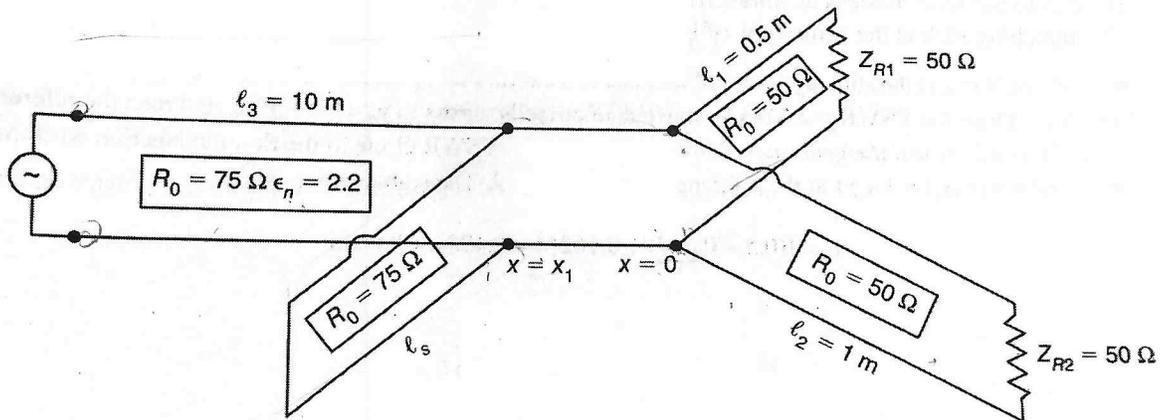
$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\mathbf{B} = -\int \frac{\partial \mathbf{B}}{\partial t} dt$$

BECAUSE THE FIELDS ARE TIME HARMONIC,  $C = 0$ .



3. A 0.15 GHz signal is applied to a 10-m-long 75- $\Omega$  coaxial line terminated in a composite load consisting of the parallel connection of two 50- $\Omega$  lines of lengths 0.5 m and 1 m, each terminated in a 50- $\Omega$  resistance. All lines are lossless with  $\epsilon_r = 2.2$ . See the figure below.



- a. Find the phase velocity and wavelength on the main feedline. [5]

$$v_p = \frac{c}{\sqrt{2.2}} = 2.02 \times 10^8 \text{ m/s} \quad \lambda = \frac{v_p}{f} = 1.35 \text{ m}$$

- b. Find the effective load impedance at  $x = 0$ . [5]

$$Z_L = 25 \Omega \quad \beta L = 0.3 = \frac{Z_L}{Z_0}$$

- c. Use a Smith Chart to determine the length  $\ell_s$  of a shunt short-circuit stub that will produce minimum VSWR on the feed line. The stub should be as close as possible to the load. [5]

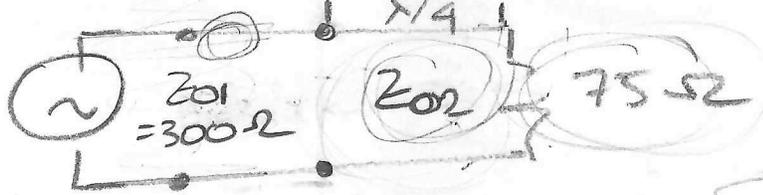
$$x_1 = 0.3325 - 0.25 \lambda = 0.0835 \lambda = 0.1127 \text{ m}$$

- d. Use a Smith Chart to determine the connection point  $x_1$  of a shunt short-circuit stub that will produce minimum VSWR on the feed line. The stub should be as short as possible. [5]

$$\ell_s = (0.25 + 0.1345 \lambda) = 0.3845 \lambda = 0.519 \text{ cm}$$

- e. What are the two main disadvantages of a single-stub matching network? [5]

- ONLY WORKS AT A SINGLE FREQUENCY
- MAY BE DIFFICULT TO ATTACH A STUB TO THE TRANSMISSION LINE AT AN ARBITRARY DISTANCE, PARTICULARLY IF THE TRANSMISSION LINE IS A COAXIAL CABLE



4. A quarter-wave section of transmission line is used to match a  $75\text{-}\Omega$  load to a  $300\text{-}\Omega$  transmission line. Use a Smith Chart to determine:

a. The characteristic impedance of the quarter-wave section. [5]

$$Z_0 = \sqrt{Z_L Z_{in}} = \sqrt{75 \times 300} = 150\ \Omega$$

EXPLANATION:  $\frac{Z_L}{Z_0}$  must equal  $\frac{Z_0}{Z_{in}} = \frac{1}{\frac{Z_{in}}{Z_0}}$

b. The VSWR on the quarter-wave section. [5]

$$S = \frac{1 + |\Gamma|}{1 - |\Gamma|} = \frac{1.333}{0.666} = 2 = \frac{V_{max}}{V_{min}} = \text{VSWR}$$

$$|\Gamma| = 0.333$$

c. The voltage reflection coefficient on the quarter-wave section [5]

$$\Gamma(z) = \Gamma_0 e^{j2\beta z} = -0.333 e^{j(2 \cdot \frac{2\pi}{\lambda} \cdot z)} = -0.333 e^{j\frac{4\pi z}{\lambda}}$$

d. The reflection coefficient at the load. [5]

$$\Gamma_0 = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{75 - 150}{75 + 150} = \frac{-75}{225} = -\frac{1}{3} = -0.333$$

e. What are the principal advantages and disadvantages of this matching technique? [5]

### ADVANTAGES

- COMPACT
- A SOLUTION ALWAYS EXISTS

$$\beta = \frac{2\pi}{\lambda}$$

### DISADVANTAGES

- ONLY WORKS AT THE DESIGN FREQ.
- PERFORMANCE DEGRADES AWAY FROM THE DESIGN FREQ.
- MAY NEED A CUSTOM BUILT MATCHING SECTION