

ELEC 342

Electromechanical Energy Conversion and Transmission

2025-26 Winter Term 2

Lecture 9

February 3, 2026

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Course Logistics

- Assignment 3 due on Feb. 11
- Quiz 2 will take place on Feb. 13 *⇒ Modules 2 + 3*
- Midterm will take place either Feb. 24 or Feb. 26 (there is a poll on Piazza)

Fundamentals: Force & Torque

Consider a conductor frame (single-coil)

Lorentz
Force

$$F = lBi_a$$

Torque

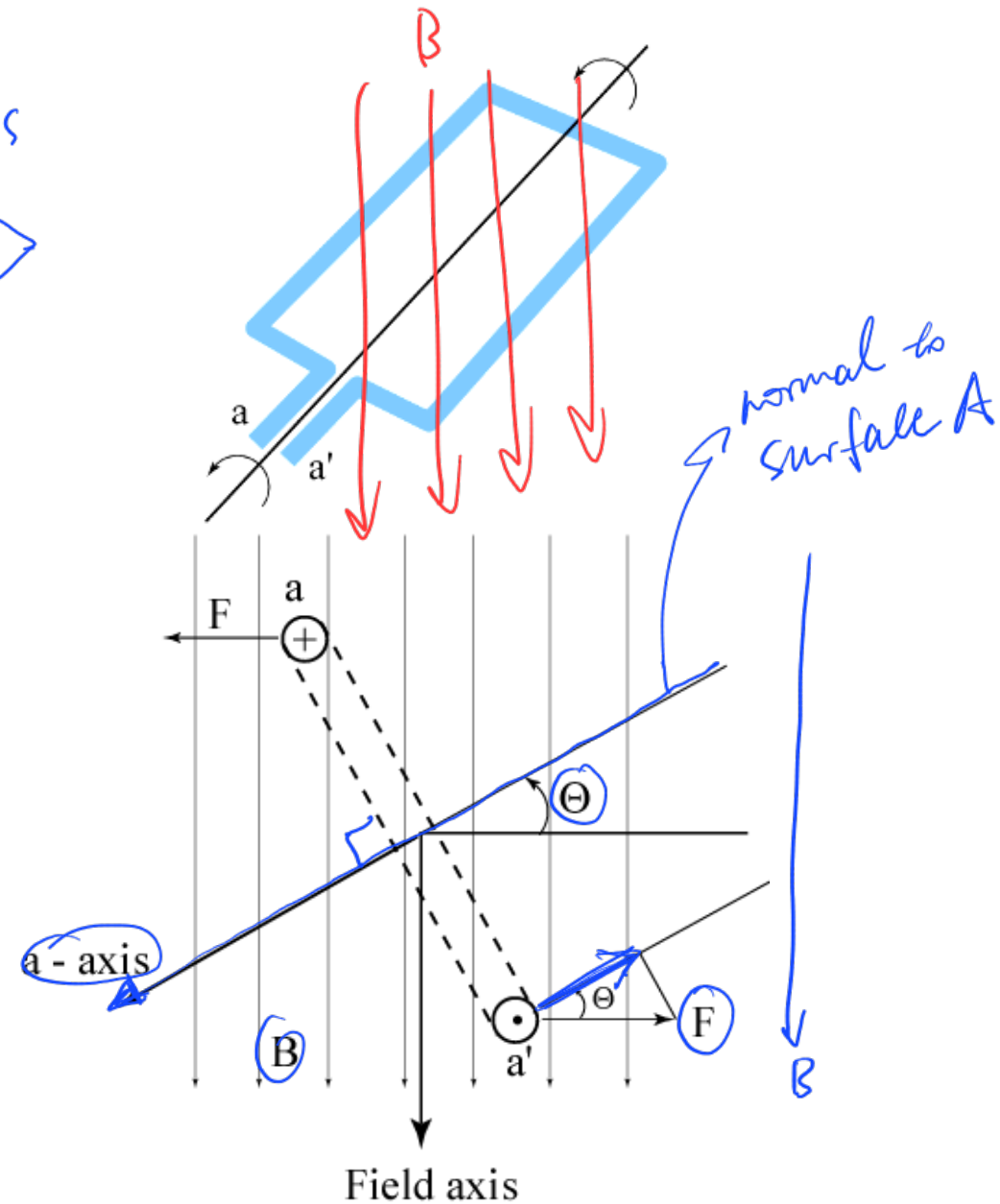
$$T_e = 2R\underline{F} \cos(\theta)$$

$$T_e = 2RlBi_a \cos(\theta)$$

$$T_e = ABi_a \cos(\theta) = \Phi_p i_a \cos(\theta)$$

NOTE: Maximum torque is when $a - axis \perp B$

and $\longrightarrow T_e \sim \Phi_p i_a$



Fundamentals: Induced Voltage

$$\Phi = \int \mathbf{B} \cdot d\mathbf{A} \leadsto \mathbf{B} \perp \mathbf{A}$$

Consider a conductor frame (single-coil)

$$\Phi = BA \sin(\theta) = B2Rl \sin(\theta)$$

Let us rotate the frame with speed ω

$$\theta = \omega t + \theta_0$$

$$\Phi = BA \sin(\theta) = \Phi_p \sin(\theta)$$

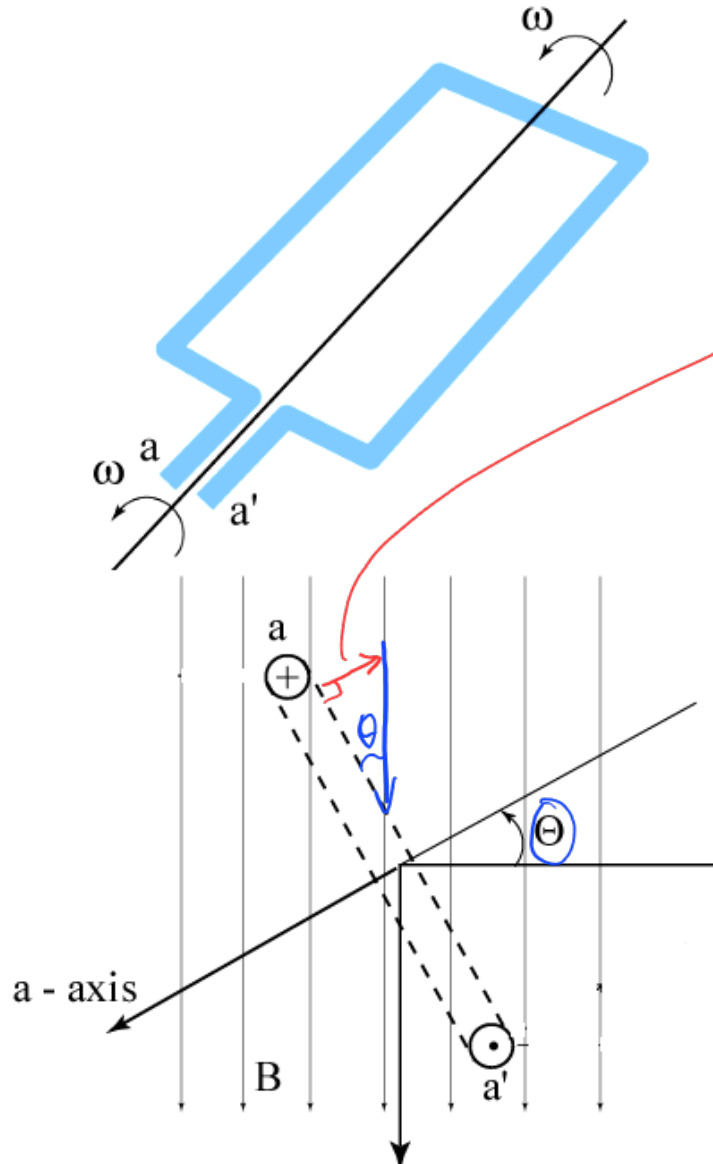
Faraday's Law $e = \frac{d\Phi}{dt}$

For coil with one turn

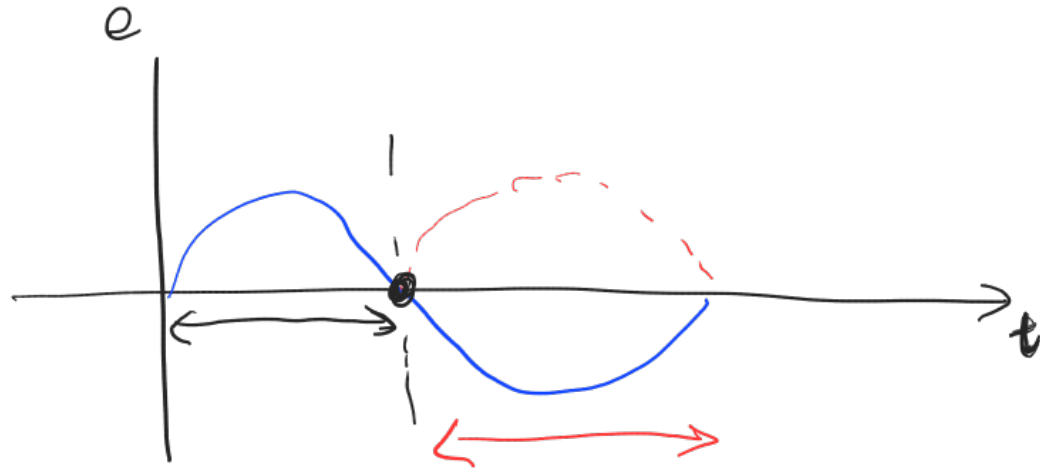
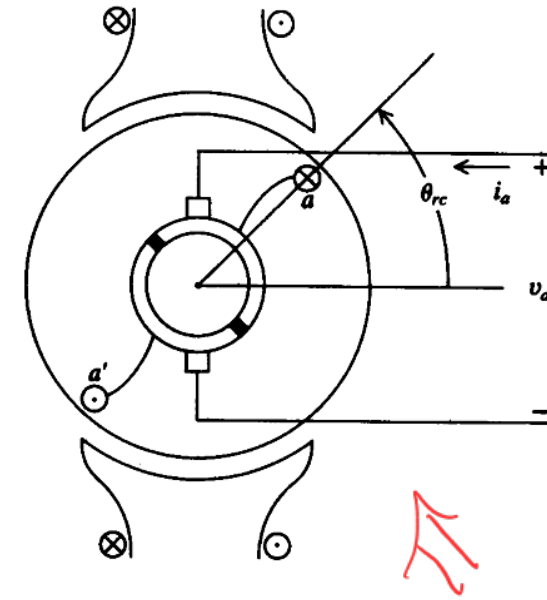
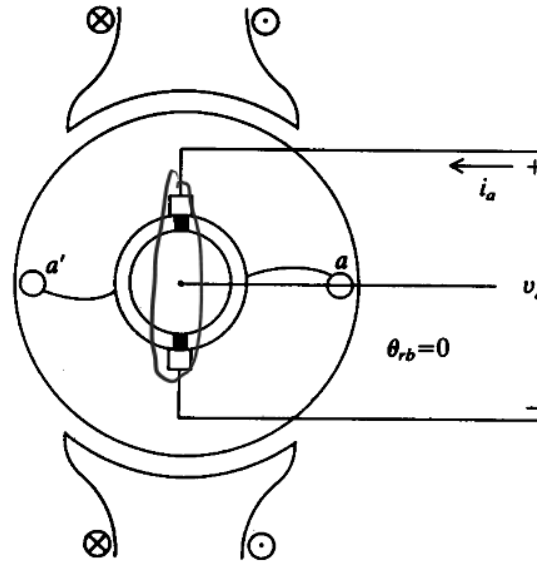
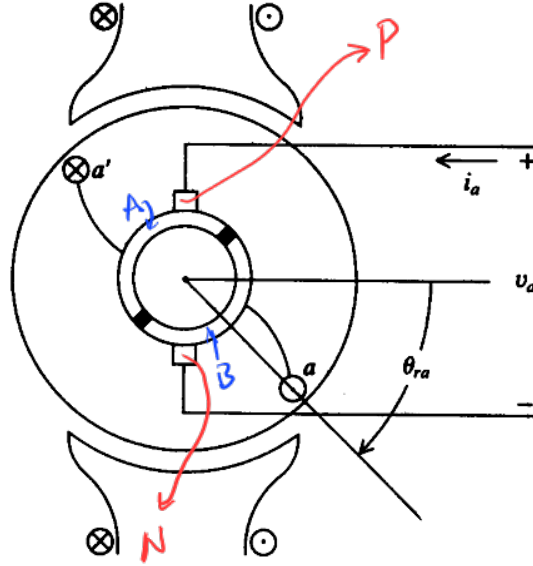
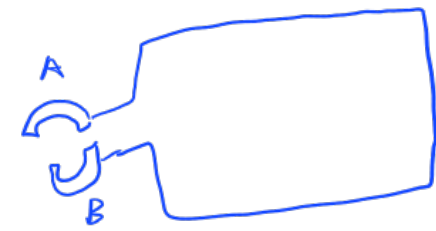
$$e = \frac{d\Phi}{dt} = \omega \Phi_p \cos(\theta) \quad \Rightarrow \quad e \sim \omega \Phi_p$$

For coil with N turns

$$e = N \frac{d\Phi}{dt} = \omega N \Phi_p \cos(\theta)$$



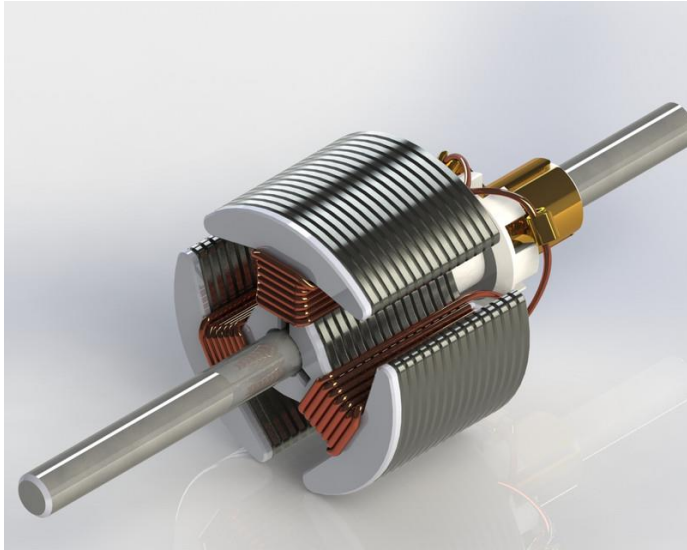
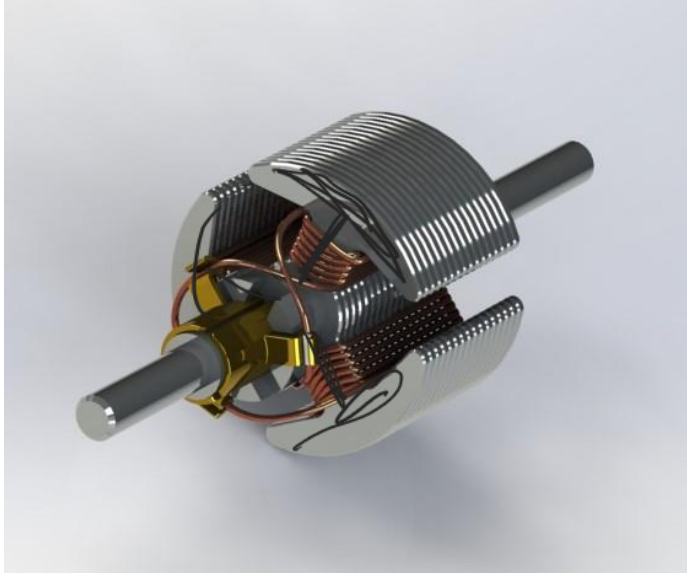
Commutation of Elementary DC Machine



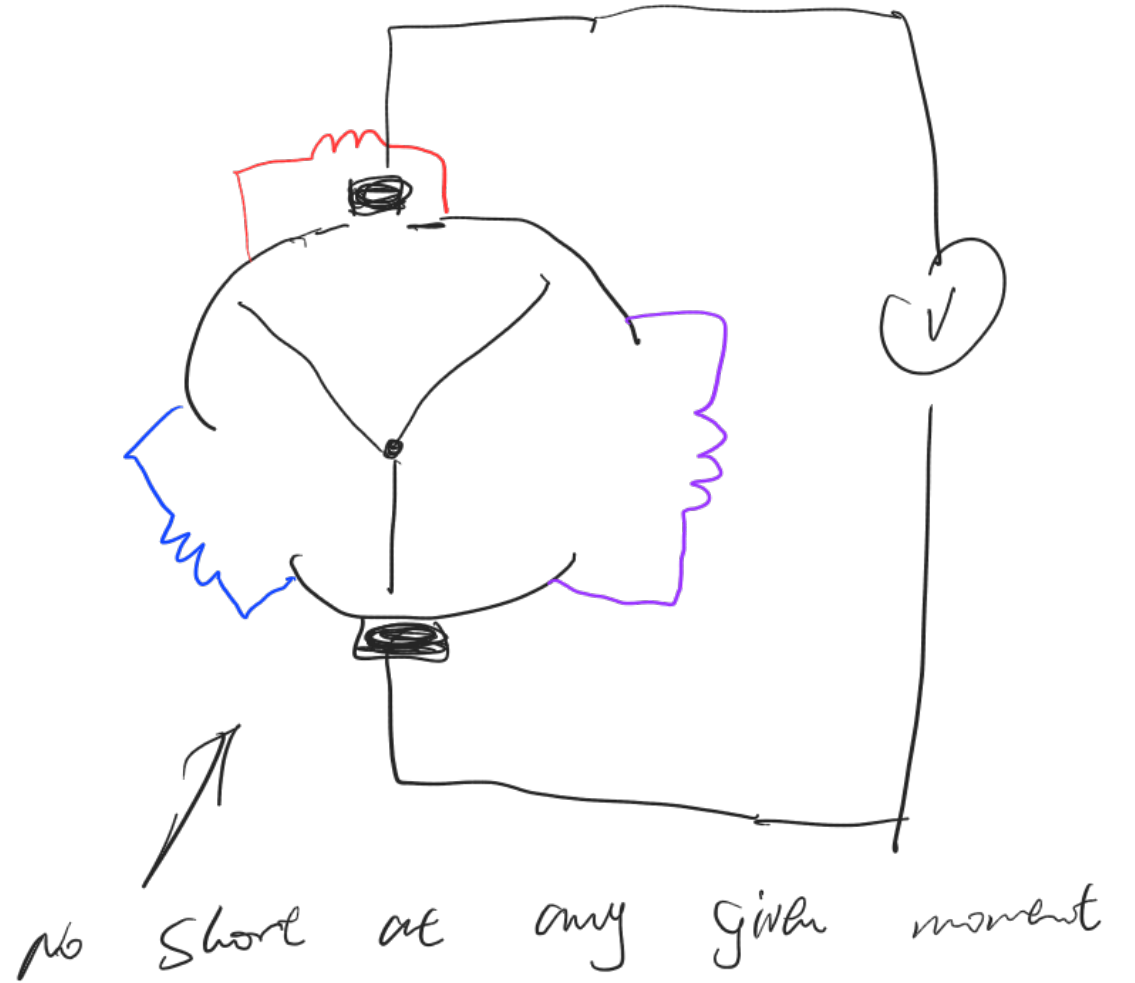
Add more frames to
reduce ripple

More Realistic DC Machine

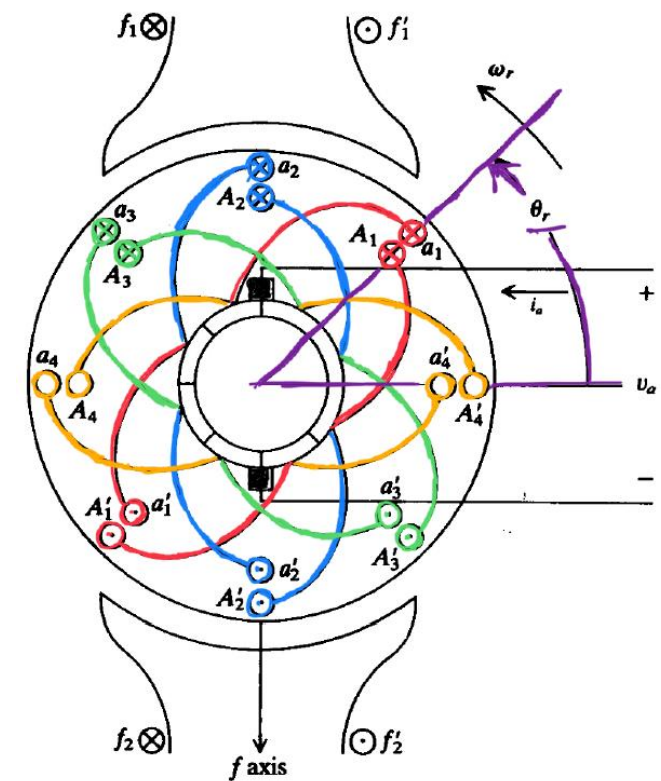
3 windings on rotor (also called armature)



Winding Connection

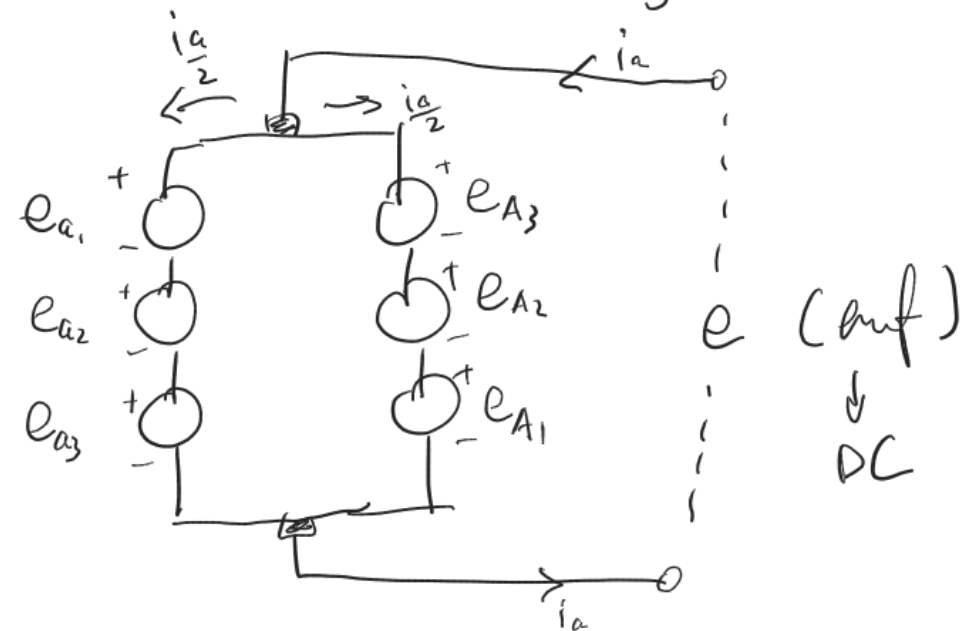
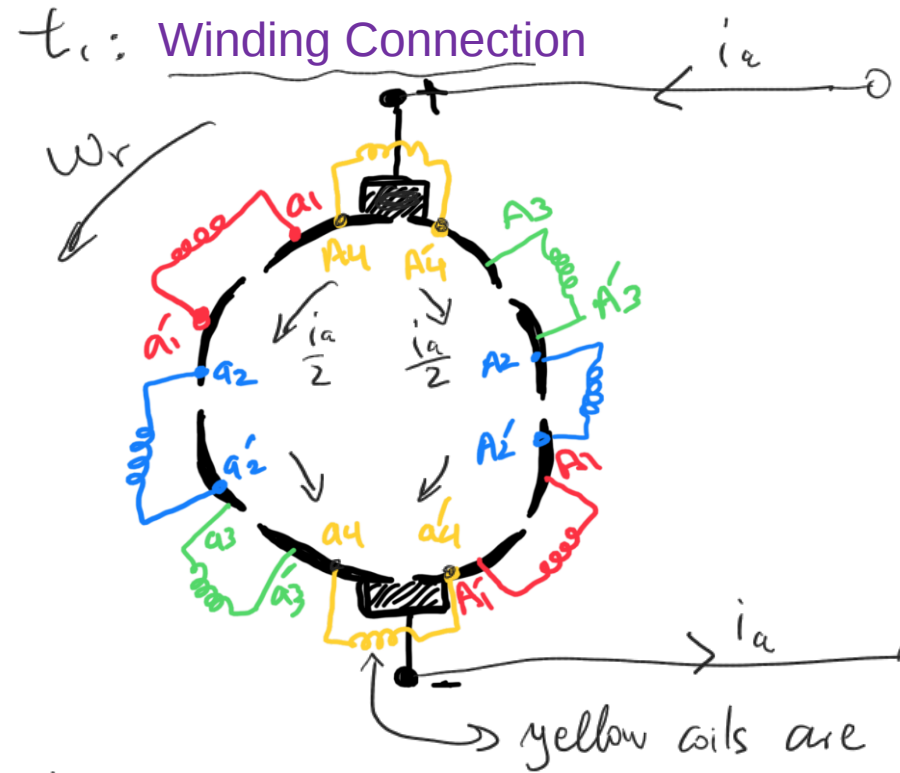
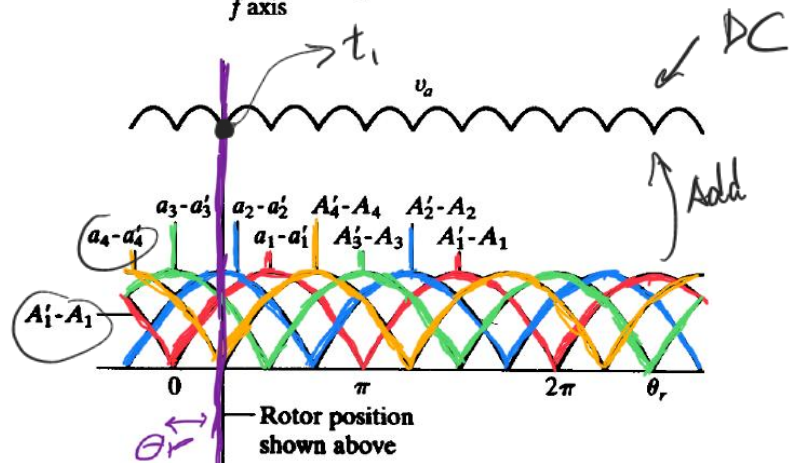


More Realistic DC Machine

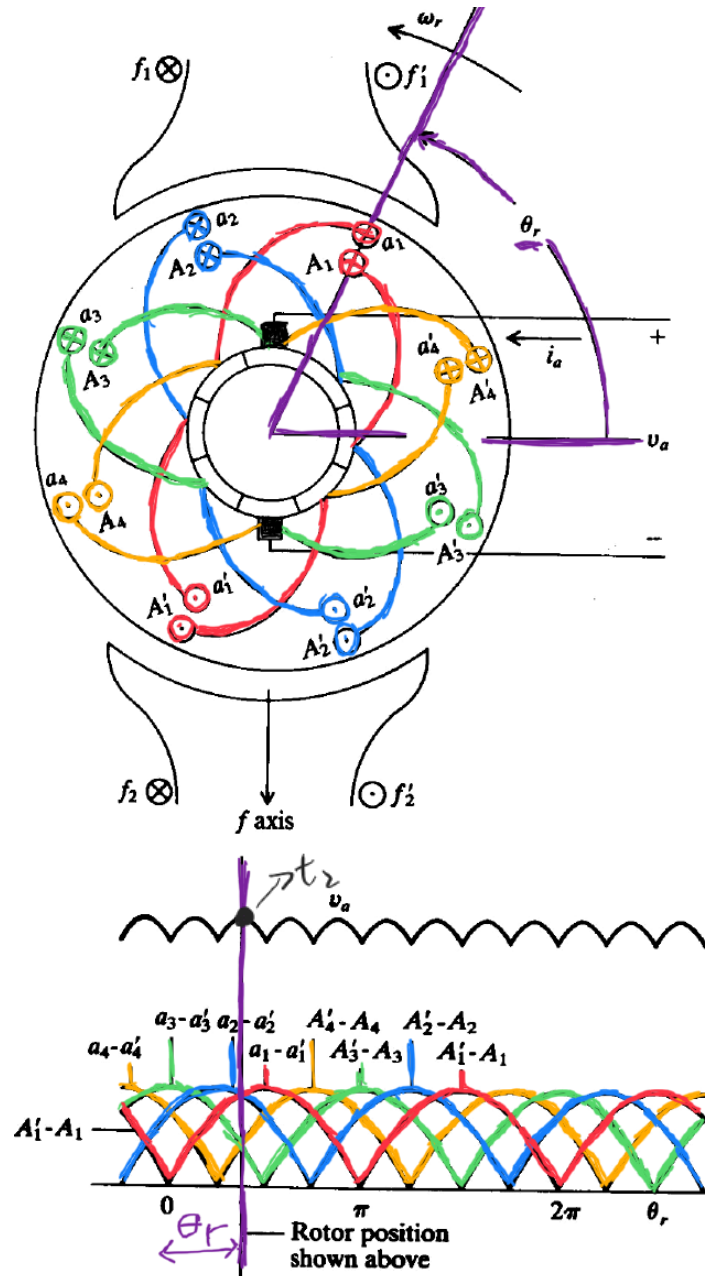


f windings:

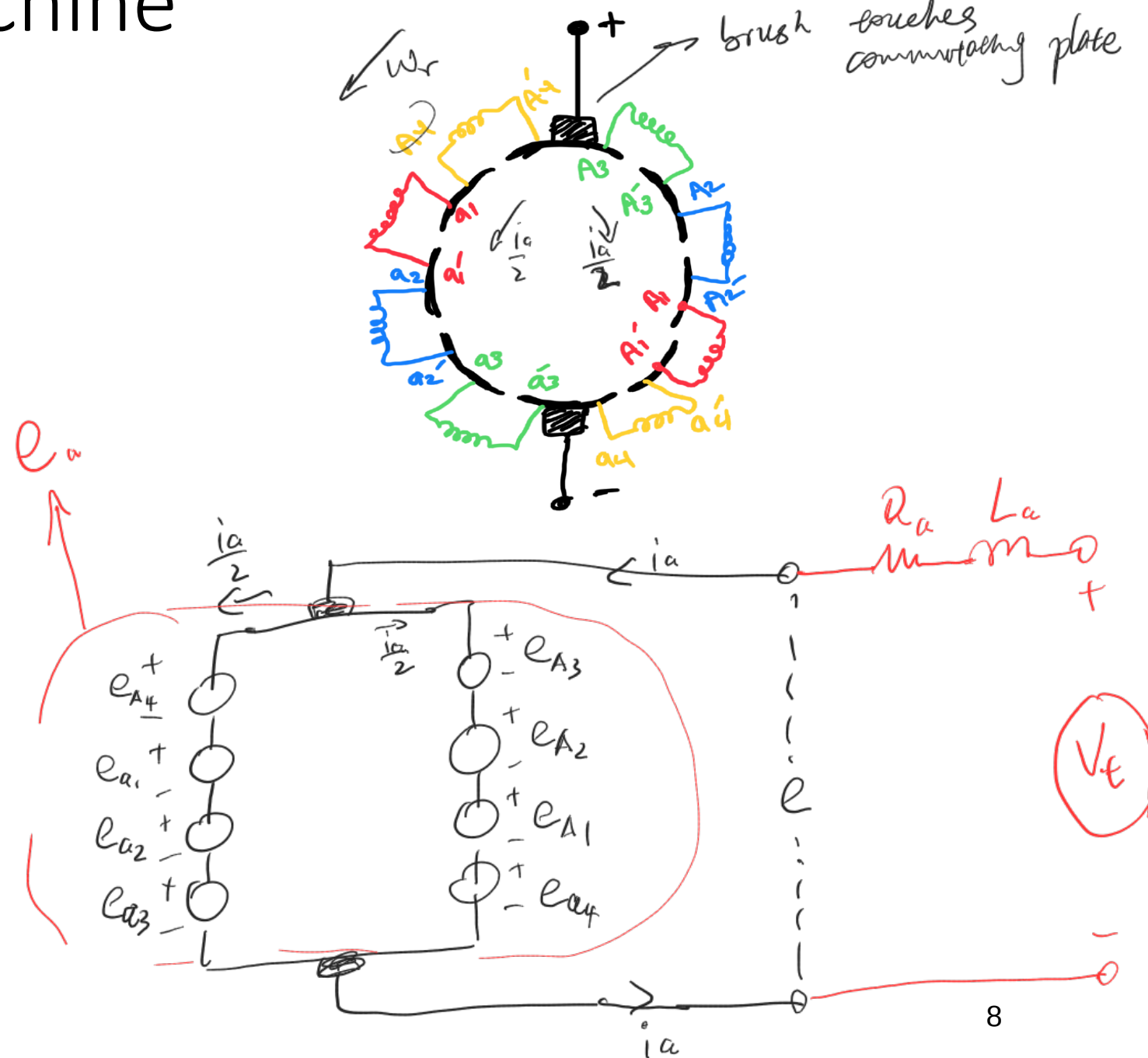
- $A_1 - A_1'$
- $A_2 - A_2'$
- + $A_3 - A_3'$
- $A_4 - A_4'$
- $a_1 - a_1'$
- $a_2 - a_2'$
- $a_3 - a_3'$
- $a_4 - a_4'$



More Realistic DC Machine

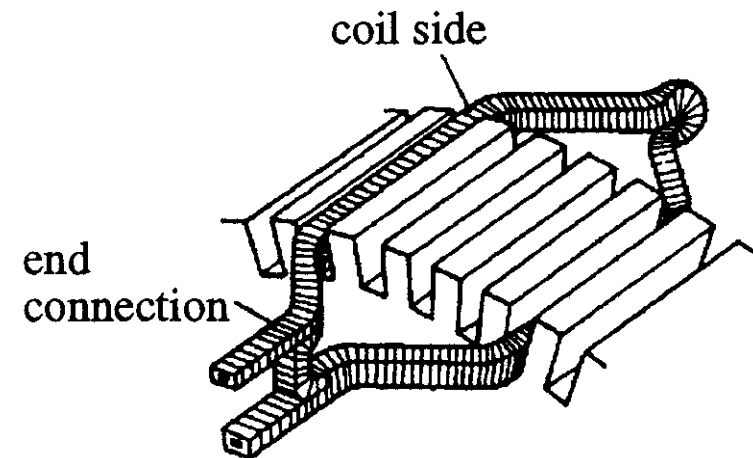
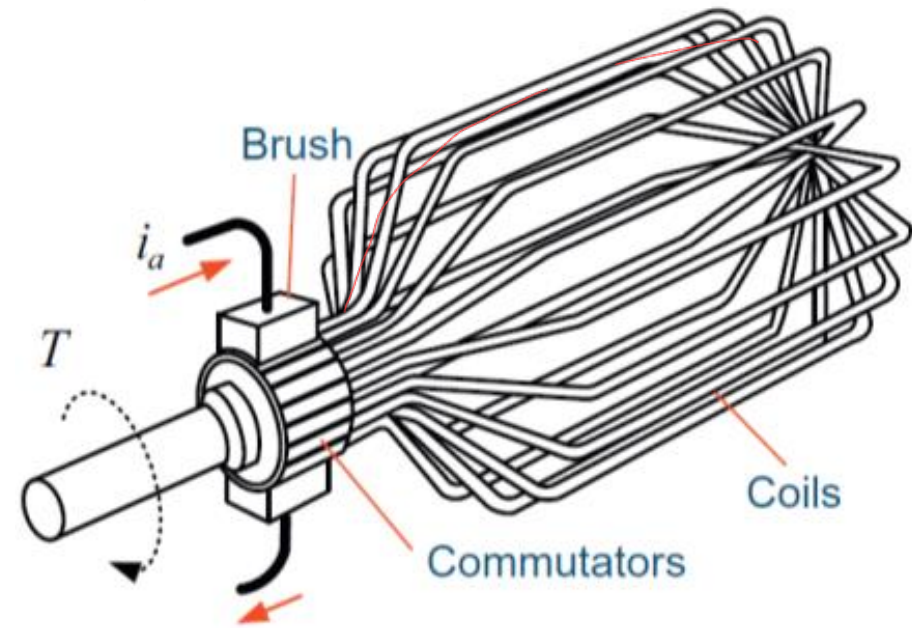
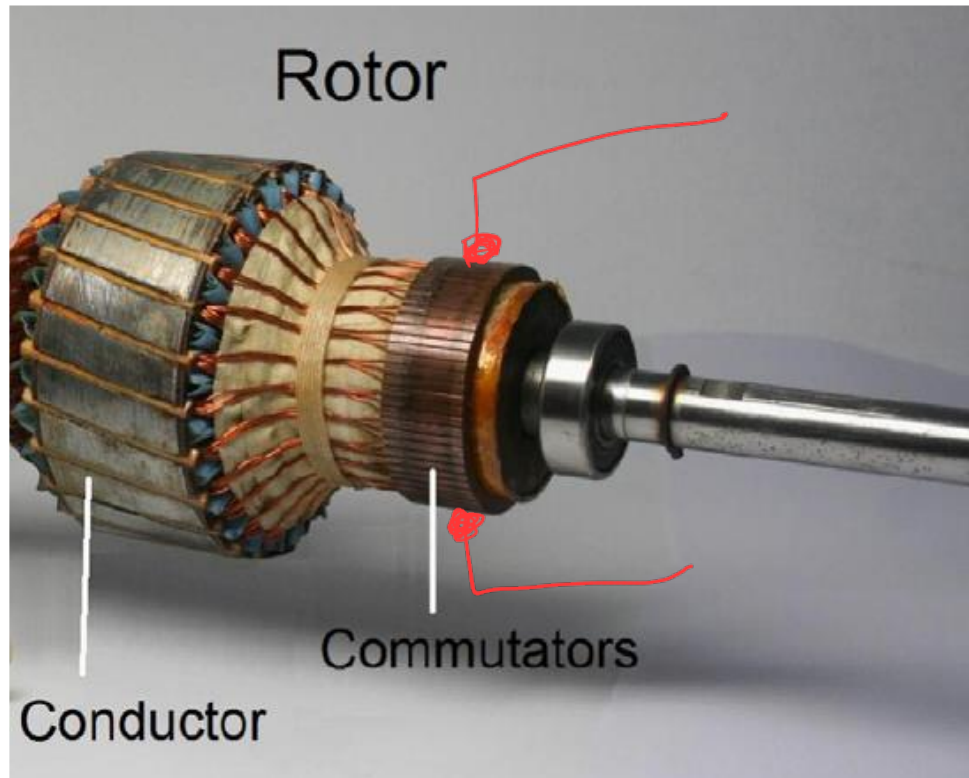


t_2 : Winding Connection



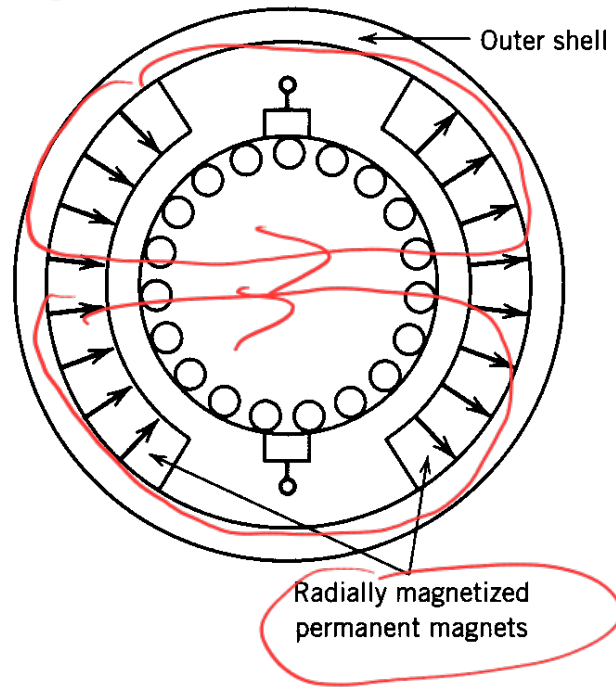
More Realistic DC Machine (rotor)

Conductor frame with several coils:

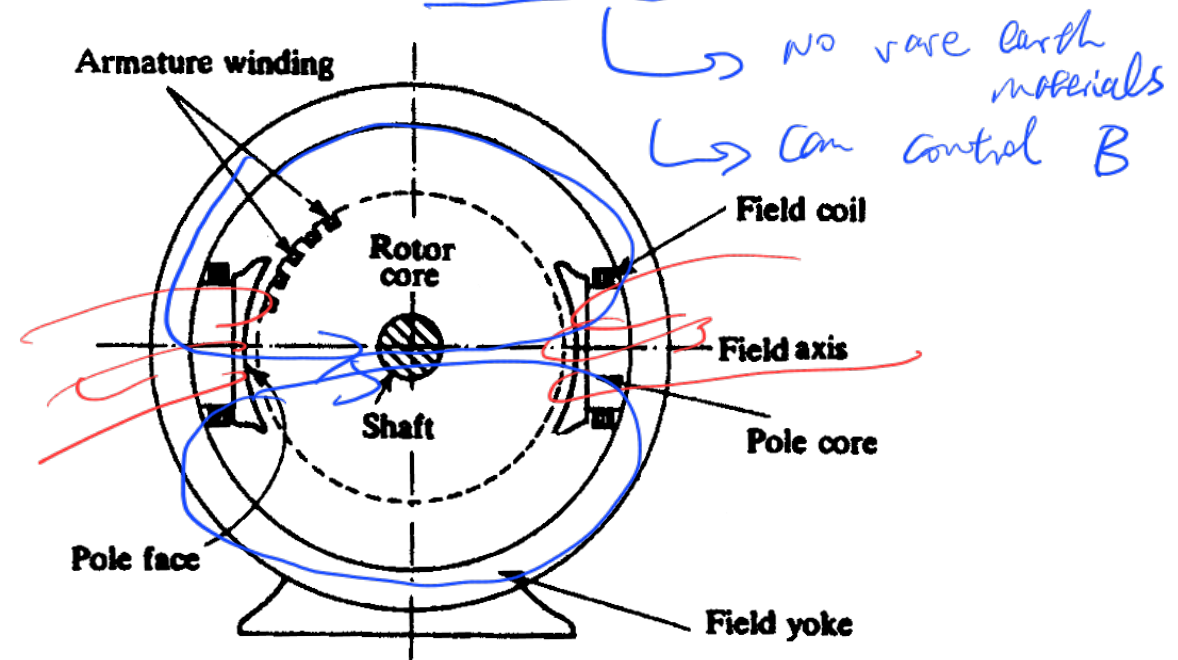


DC Machine Construction

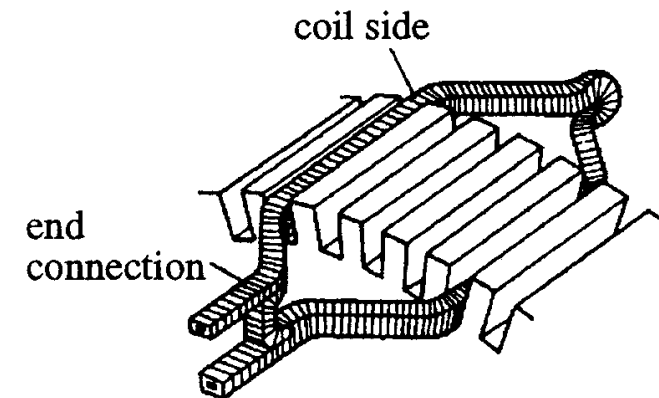
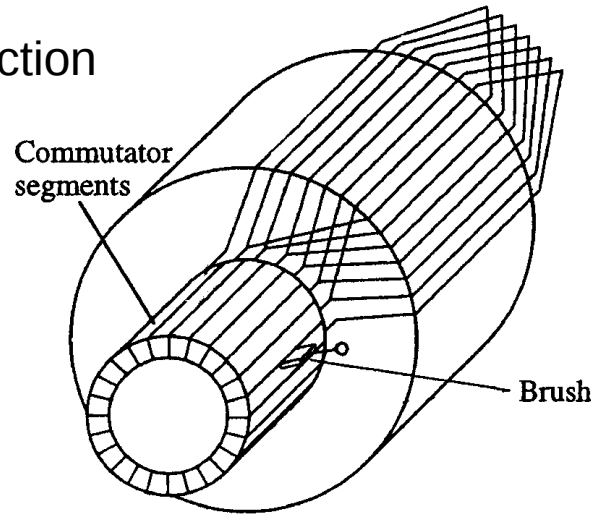
Permanent Magnet (PM) DC machine *Stator*



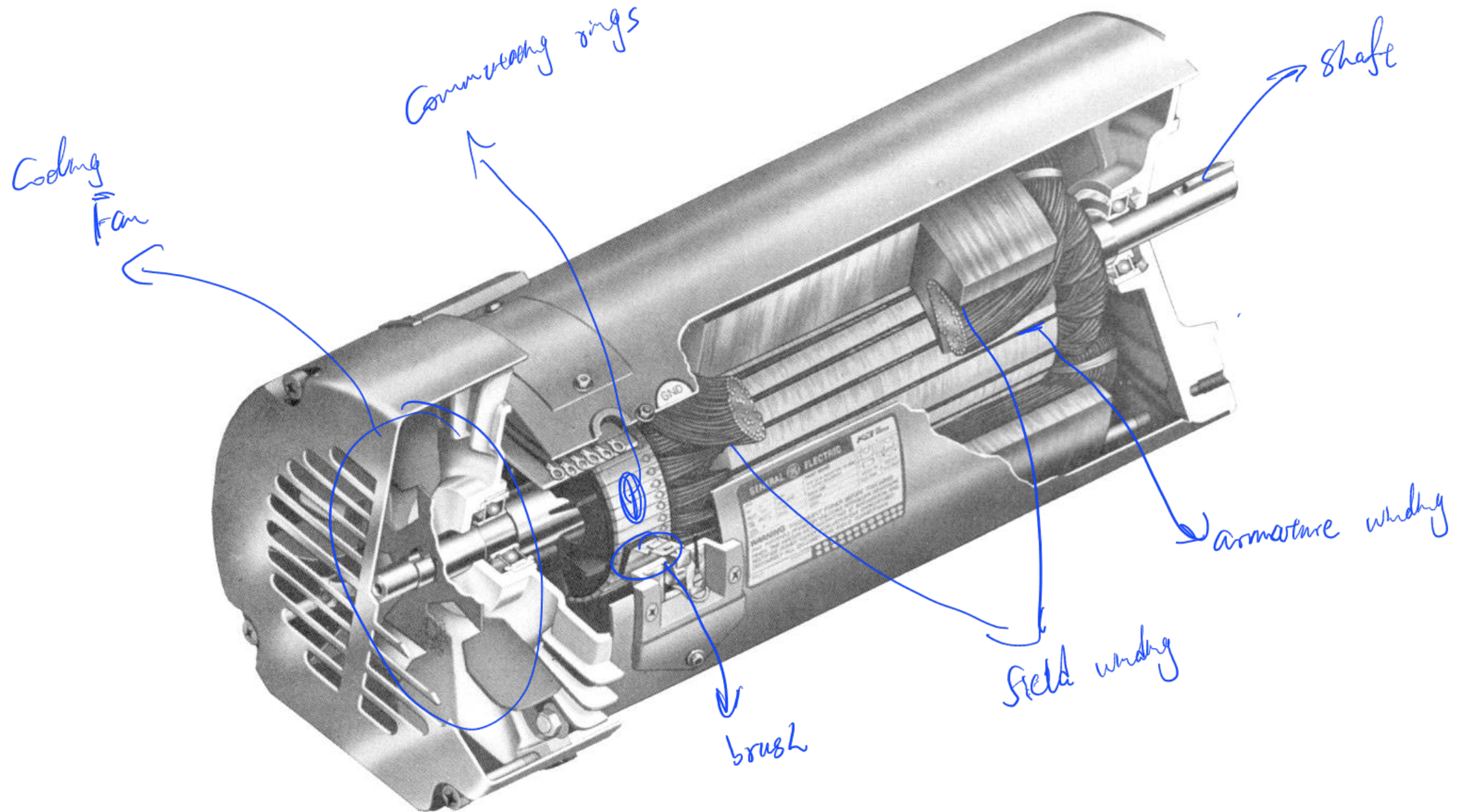
DC machine with field winding *Stator*



Rotor (Armature) construction

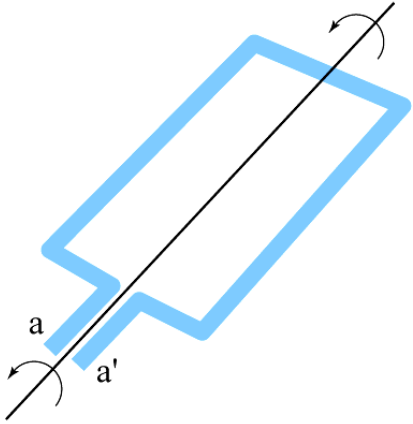


Cutaway View of a Two-Pole DC Machine



Induced Voltage & Torque

Recall a simple coil-frame – one turn



- Type of winding, rectification/averaging by the commutator action, etc.

$$e_{turn} \sim \omega \Phi_p \xRightarrow{BA} \boxed{E_a = K_a \omega_r \Phi_p}$$

$$T_{turn} \sim \Phi_p i_a \Rightarrow T_e = K_a \Phi_p I_a$$

K_a - is the machine armature constant – determined by construction / design

E_a - is the generated voltage or back emf

Power Balance

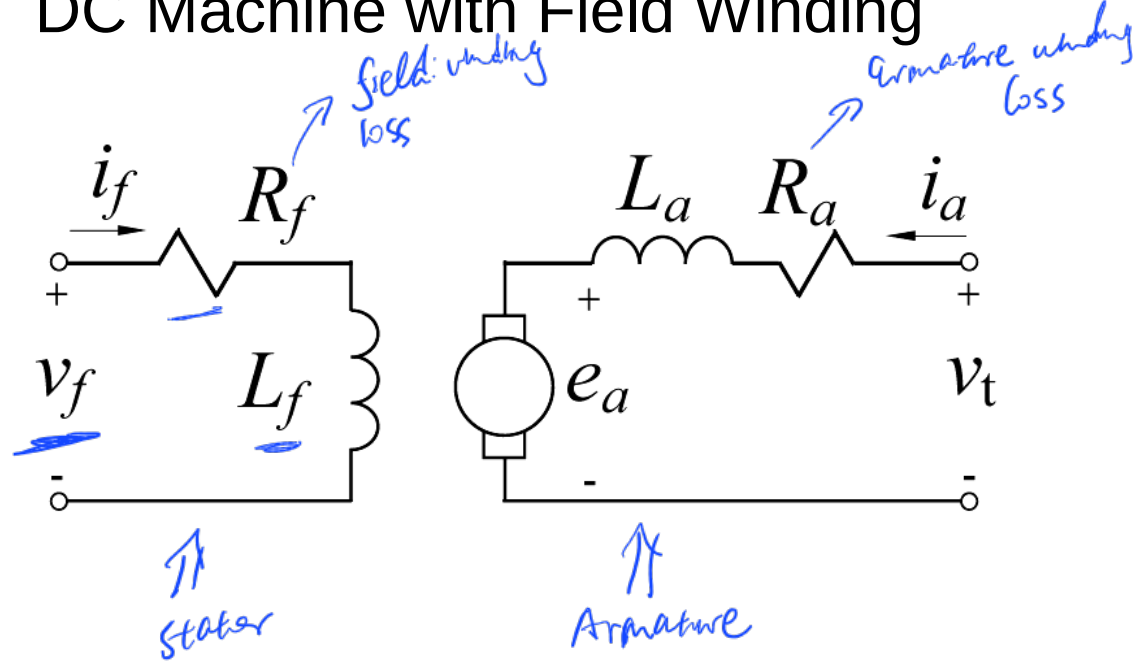
$$E_a I_a = P_e \text{ (electrical power)} \quad \omega_r T_e = P_e \text{ (electrical torque)}$$

$$P_e = E_a I_a = P_e = \omega_r T_e \text{ (lossless)}$$

$$\underbrace{K_a \omega_r \Phi_p I_a}_{E_a} = \omega_r \underbrace{K_a \Phi_p I_a}_{T_e} \Rightarrow T_e = K_a \Phi_p I_a$$

Commonly-Used Equivalent Circuit *Quiz questions*

DC Machine with Field Winding



v_f - is the field voltage

i_f - is the field current

R_f - field winding resistance

L_f - field winding inductance

v_t - applied terminal voltage

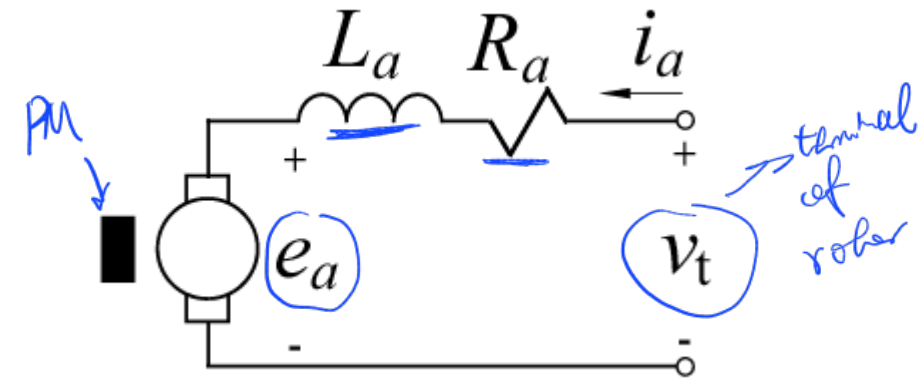
i_a - is the armature current

R_a - armature winding + brush resistance

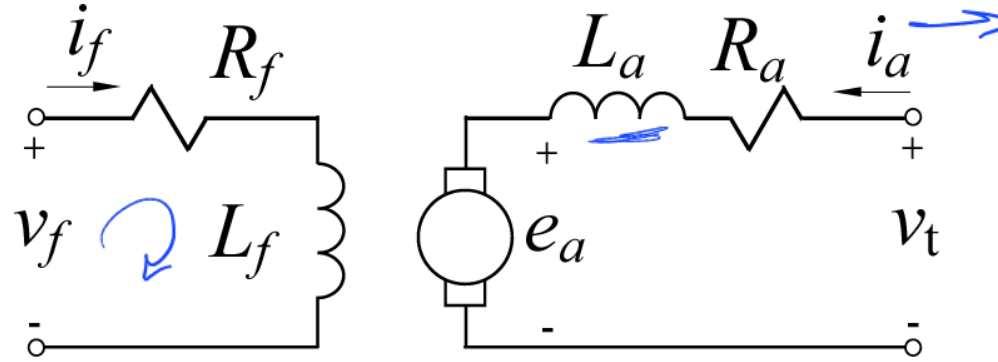
L_a - armature winding inductance

e_a - Induced back emf (voltage)

PM DC Machine



Governing Dynamics State Equations



Field Winding Equations

$$\underline{v_f} = \underline{R_f i_f} + \frac{d\lambda_f}{dt}$$

$$\underline{\lambda_f} = \underline{N_f \Phi_p} = \underline{L_f i_f}$$

Mechanical Motion

$$J \frac{d\omega_r}{dt} = \underline{T_e - T_m - T_{fric}}$$

$$\underline{J = J_{dc_machine} + J_{mech_load}}, \quad [kg \cdot m^2] \text{ - is the combined moment of inertia of the motor and load}$$

Armature Equations

$$\underline{v_t} = \underline{\pm R_a i_a} + L_a \frac{di_a}{dt} + e_a$$

$$\underline{e_a} = K_a \Phi_p \omega_r$$

$$\underline{T_e} = K_a \Phi_p i_a$$

Depending on
motoring or
generating,
polarity is different

motoring:
 $v_t > e_a$
generating:
 $v_t < e_a$

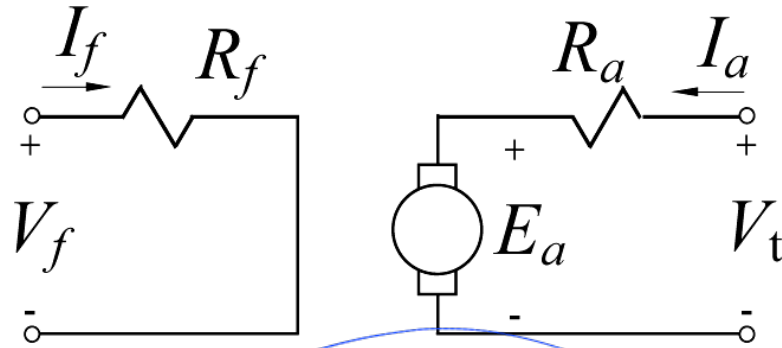
Steady-State Equivalent Circuit $\Rightarrow \infty L, \frac{dw}{dt} = \emptyset$

Field-Wound Machine

Field Winding Equations

$$V_f = R_f I_f$$

$$\lambda_f = N_f \Phi_p = L_f I_f$$

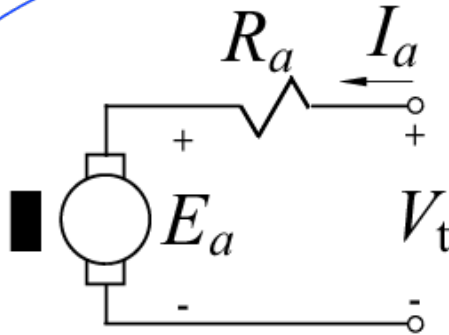


Armature Equations

$$V_t = \pm R_a I_a + E_a$$

$$E_a = K_a \Phi_p \omega_r$$

PM Machine



Torque / Mechanical Side $T_e = K_a \Phi_p I_a$

$$T_e = T_m + T_{mech_loss} = T_m + K_{fric} \omega_r$$

Friction loss
(for large machines
often can be neglected)

Torque & Voltage Constant for PM Machines

Recall field winding flux: $\Phi_p = \frac{\lambda_f}{N_f} = \frac{L_f}{N_f} i_f$

Back emf: $e_a = K_a \Phi_p \omega_r = K_a \frac{L_f}{N_f} i_f \omega_r$

Electromagnetic torque: $T_e = K_a \Phi_p i_a = K_a \frac{L_f}{N_f} i_f i_a$

Define $L_{af} = K_a \frac{L_f}{N_f}$ - is the mutual inductance between field and rotating armature coils

field ↔ armature

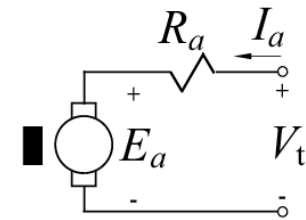
We can use alternative expression for back EMF and Torque for **Field-Wound Machine**

$e_a = L_{af} I_f \omega_r = \tau_{af} \omega_r$

$T_e = L_{af} I_f I_a = \tau_{af} I_a$

$L I = \lambda$
constant in PM

For PM Machine



$e_a = K_v \omega_r$

$T_e = K_t i_a$

Torque / voltage machine constant

$K_t = K_v$

often you find these #s not equal in datasheet
Because different units

DC Machine: Example 1

Consider a small PM DC Motor with the following parameters:

$V_{t_rated} = 6 \text{ V}$, $I_{no_load} = 0.15 \text{ A}$, $R_a = 7 \Omega$, and torque constant $K_t = 0.014 \text{ [Vs/rad]}$.

Find no-load speed $n_{nl} \text{ [rpm]}$, back emf E_a , and friction torque T_{fric} at $V_t = 6 \text{ V}$

$$V_t = R_a I_a + E_a = R_a I_a + K_t \cdot \omega$$

$$\omega_{nl} = \frac{V_t - R_a I_a}{K_t} = \frac{6 - 7 \cdot 0.15}{0.014} = 353.57 \text{ rad/sec}$$

$$n_{nl} = \frac{30}{\pi} \omega_{nl} = 3,376.4 \text{ rpm}$$

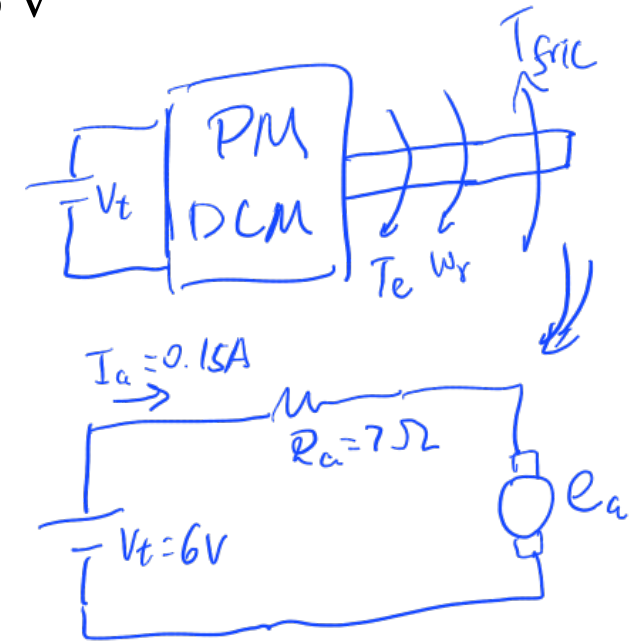
$$\text{Back emf } E_a = K_t \cdot \omega = 0.014 \cdot 353.57 = 4.95 \text{ V}$$

Electromagnetic torque

$$T_e = K_t \cdot I_a = 0.014 \cdot 0.15 = 0.0021 \text{ N}\cdot\text{m}$$

$$T_e = \frac{P_e}{\omega} = \frac{I_a \cdot E_a}{\omega} = \frac{0.15 \cdot 4.95}{353.57} = 0.0021 \text{ N}\cdot\text{m}$$

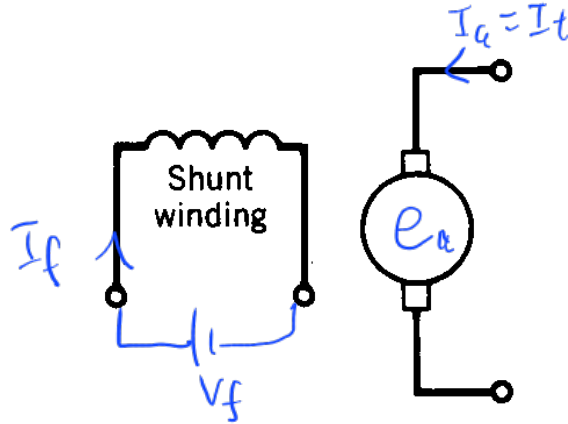
$$T_{fric} = T_e = 0.0021 \text{ N}\cdot\text{m}$$



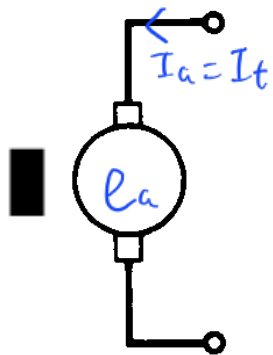
Need to be good
at this
on tests

Basic Types of DC Machines → 4 main types testable in this class

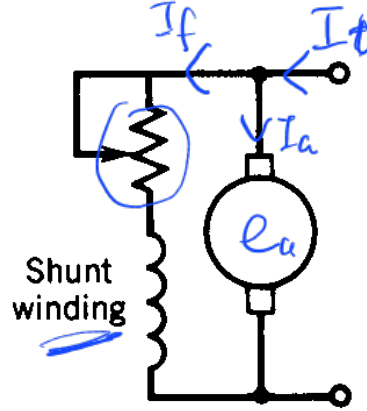
➤ Shunt or Series field windings are possible



Separately Excited
DC Machine

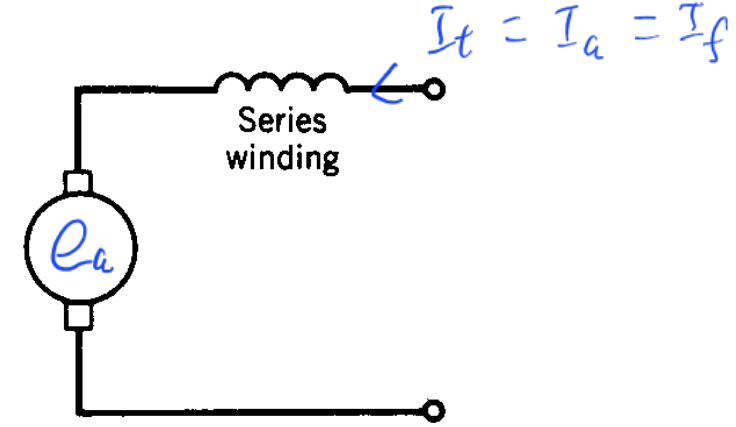


PM
DC Machine



Shunt
DC Machine

- Field winding is designed for up to rated armature voltage
- Field winding has large number of turns
- Field current is small compared to armature current



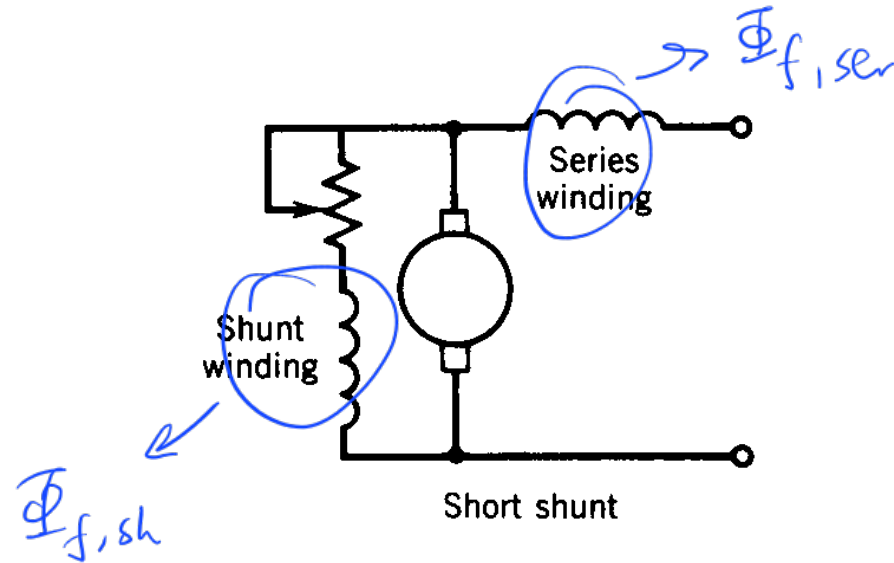
Series
DC Machine

- Field winding is designed for up to rated armature current
- Field winding has small number of turns
- Field current is the same as the armature current

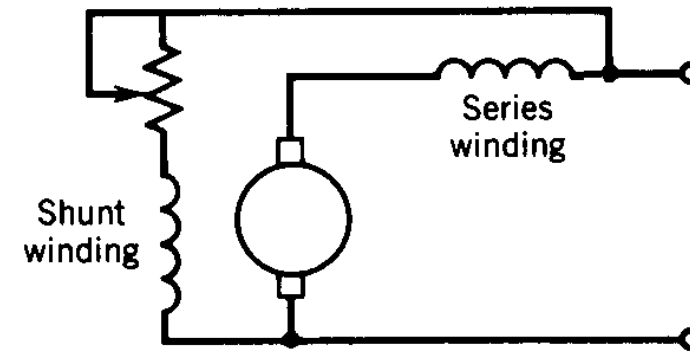
Basic Types of DC Machines *→ Not on test*

Compound DC Machines

- Both Shunt and Series field windings are present
- Various connections are possible
- Field windings are designed/connected to achieve a desirable torque/speed characteristics



Short-Shunt
Compound
DC Machine



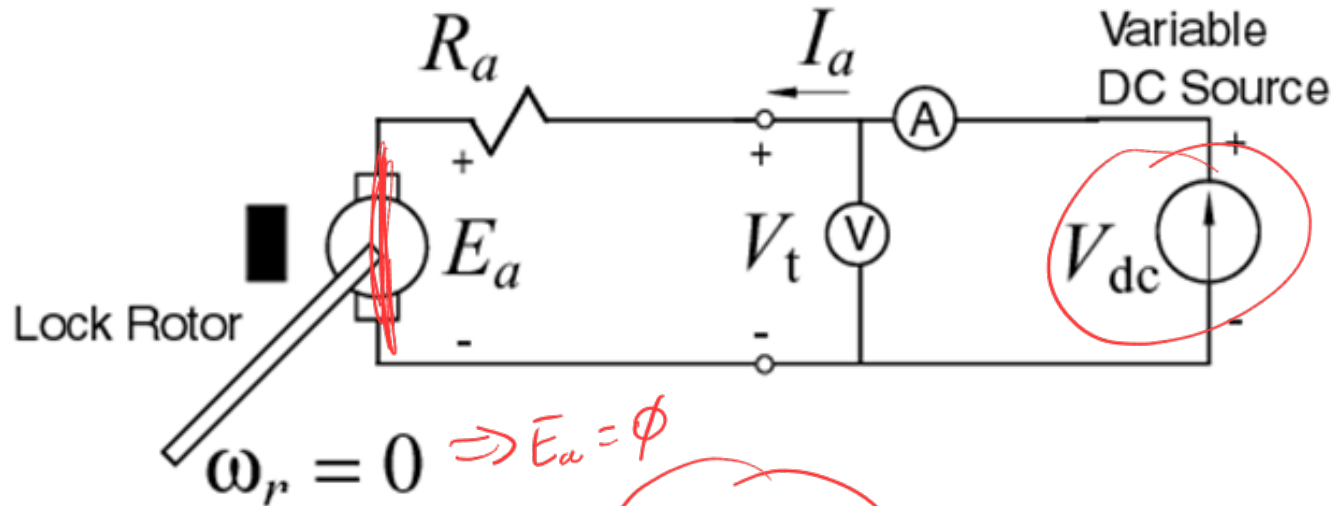
Long-Shunt
Compound
DC Machine

$$\Phi_f = \pm \Phi_{f,ser} \pm \Phi_{f,sh}$$

Parameters of PM DC Machine (Lab 3)

- **Blocked-Rotor Test** (DC Measurements)

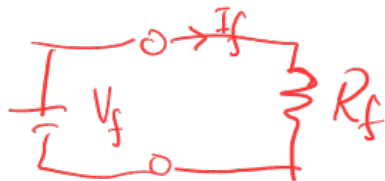
Slowly ramp up DC voltage and measure DC current up to nominal value
Determine resistance of armature winding:



$$R_a = \frac{V_t}{I_a}$$

(armature + brush combined resistance at no speed!)

Use similar measurement for field winding to estimate its resistance for field-wound DC machines



$$R_f = \frac{V_f}{I_f}$$

Parameters of PM DC Machine

• No Load Test (Friction vs. Speed)

Assume you know R_a *from blocked rotor test*

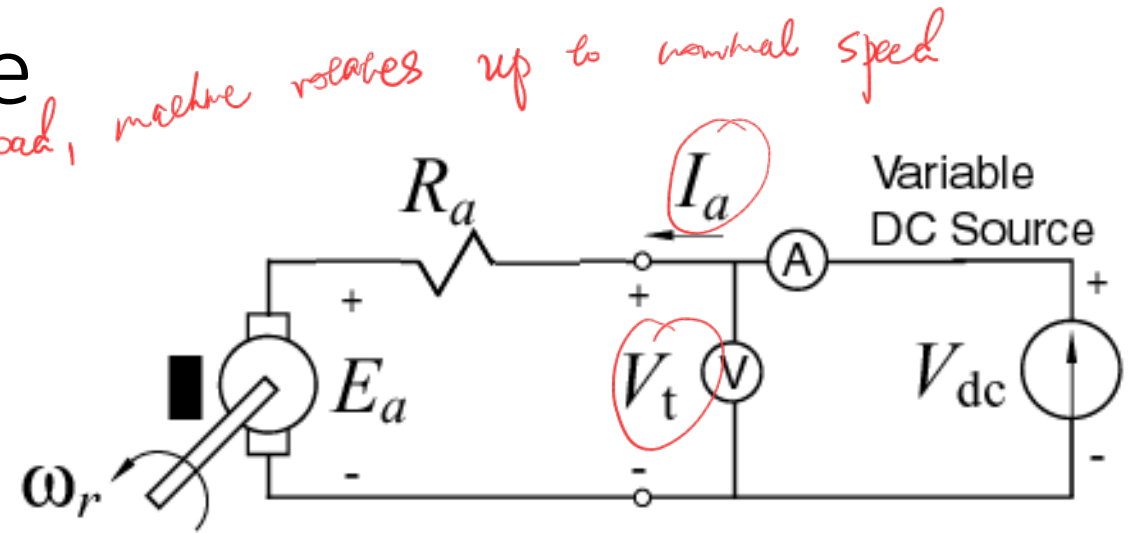
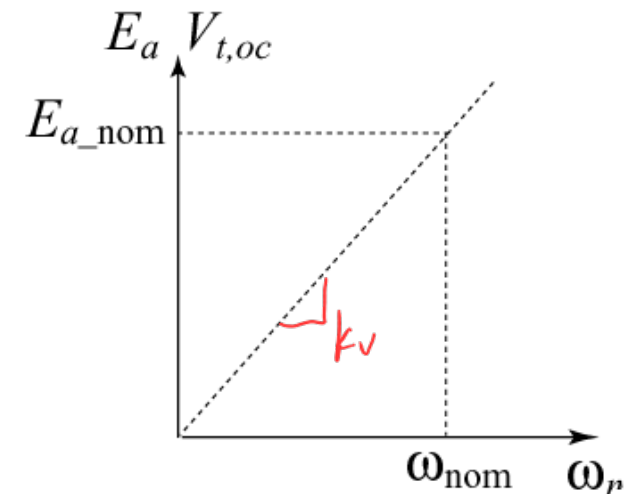
Measure $I_a, V_t, \omega_r \neq \emptyset$

$$E_a = k_v \omega_r$$

$$V_t = R_a I_a + E_a$$

Torque / voltage machine constant

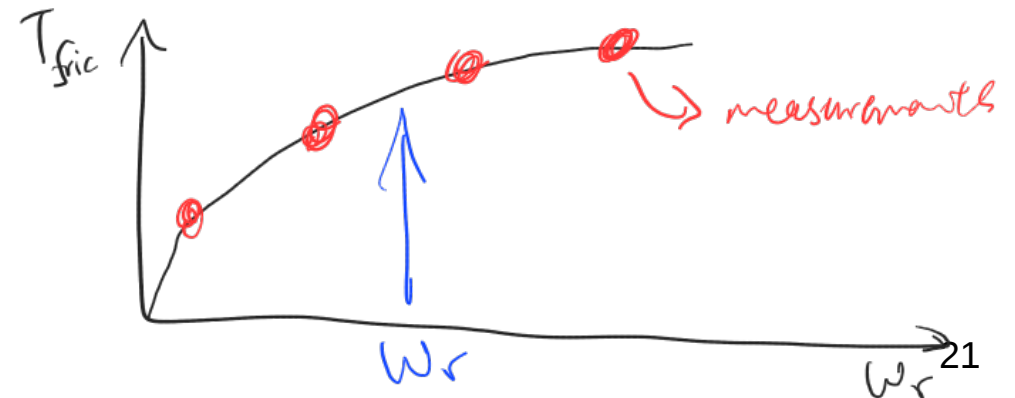
$$k_t = k_v = \frac{V_t - R_a I_a}{\omega_r}$$



Obtain Friction Torque-Speed Characteristic

$$T_e = k_t I_a$$

$$T_e = T_{fric}(\omega_r) = \omega_r K_{fric}$$

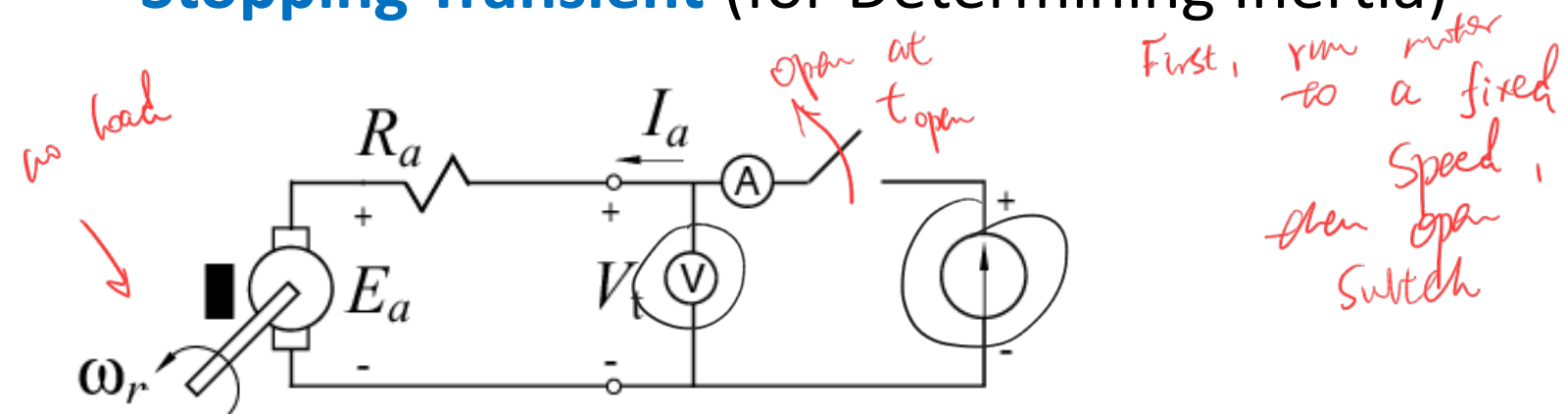


Parameters of DC Machine

• Stopping Transient (for Determining Inertia)

Assume you know $T_{fric}(\omega_r)$

Measure & Record I_a, V_t, ω_r



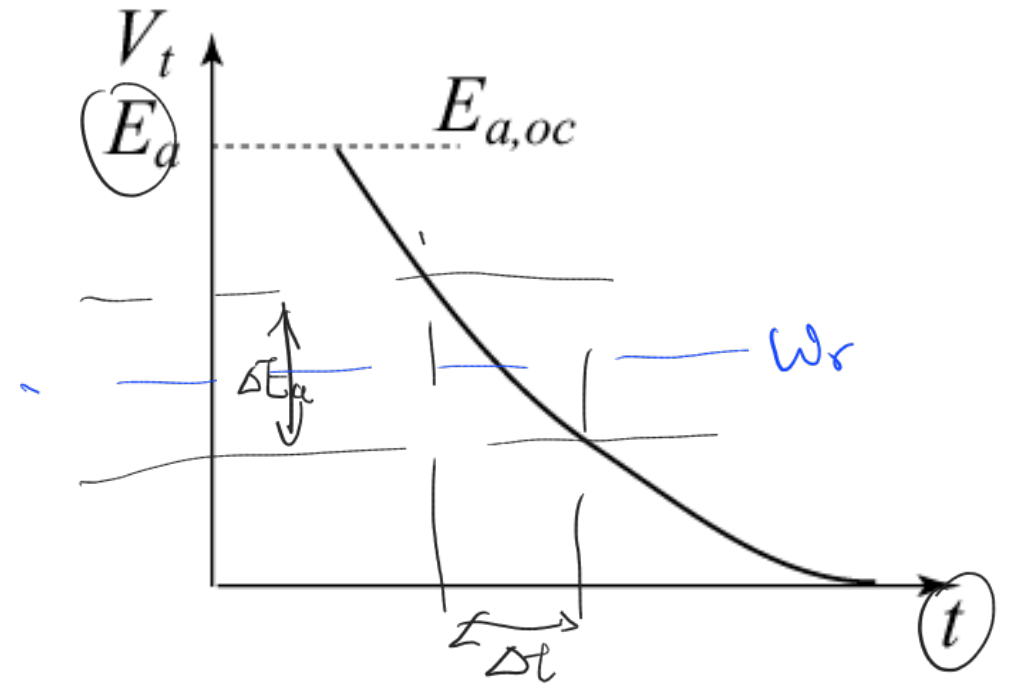
$$T_e = T_m + T_{fric}(\omega_r) + J \frac{d\omega_r}{dt}$$

$$E_a = K_a \Phi_p \omega_r = K_v \omega_r$$

$$T_{fric}(\omega_r) = -J \frac{\Delta \omega_r}{\Delta t} = -J \frac{\Delta E_a}{K_v \Delta t}$$

$$J = \frac{T_{fric}(\omega_r) \cdot K_v \cdot \Delta t}{\Delta E_a}$$

measured



Looking ahead...

- Continue **Module 4**