

ELEC 342

Electromechanical Energy Conversion and Transmission

2025-26 Winter Term 2

Lecture 10

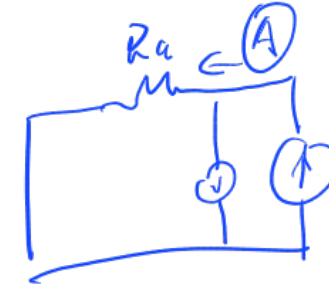
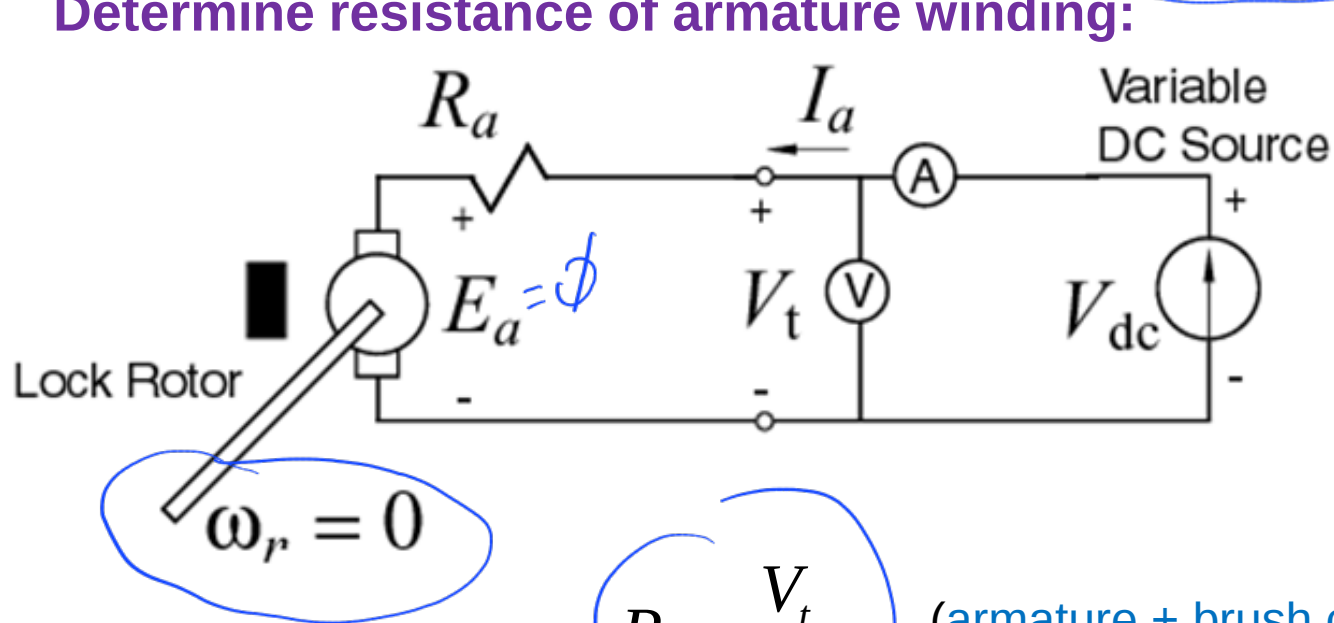
February 5, 2026

Zhi Jin (Justin) Zhang

Parameters of PM DC Machine

- **Blocked-Rotor Test** (DC Measurements)

Slowly ramp up DC voltage and measure DC current up to nominal value
Determine resistance of armature winding:



$$R_a = \frac{V_t}{I_a}$$

(armature + brush combined resistance at no speed!)

Use similar measurement for field winding to estimate its resistance for field-wound DC machines



$$R_f = \frac{V_f}{I_f}$$

Parameters of PM DC Machine

- No Load Test** (Friction vs. Speed)

rotate ~ manual speed, no load

Assume you know R_a

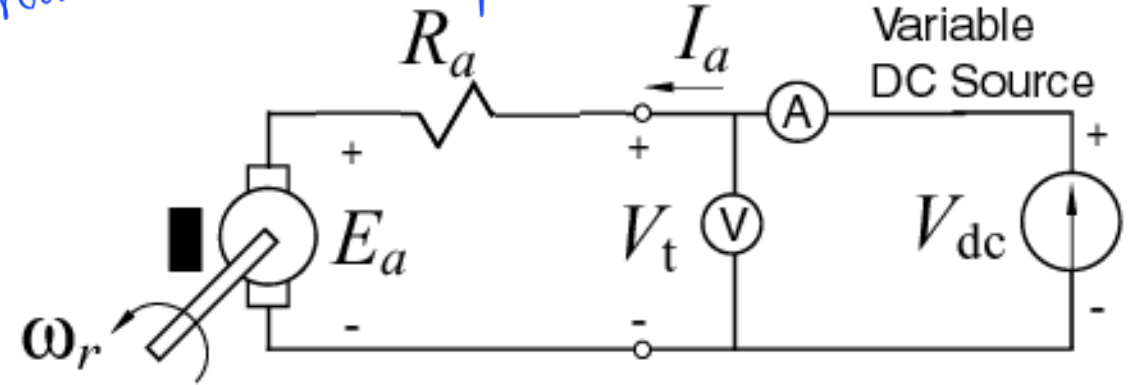
Measure I_a, V_t, ω_r

$$E_a = k_v \omega_r$$

$$V_t = R_a I_a + E_a = k_v \omega_r + R_a I_a$$

Torque / voltage
machine constant

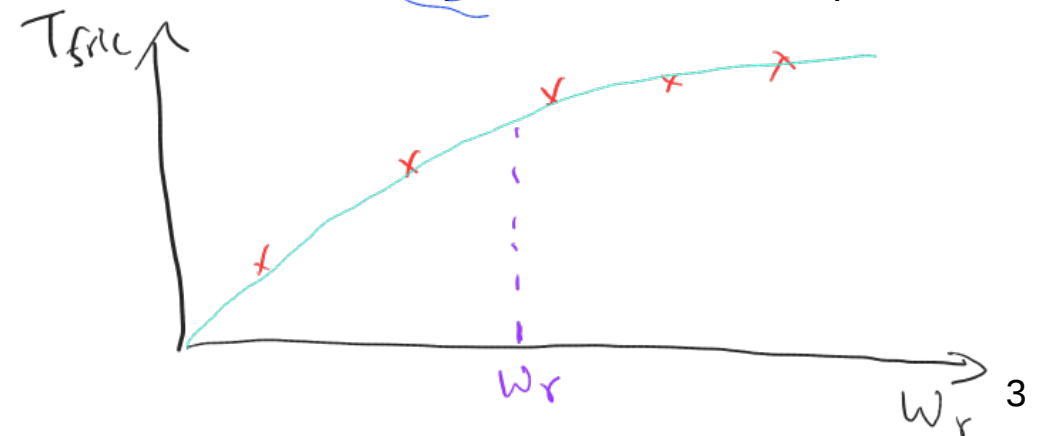
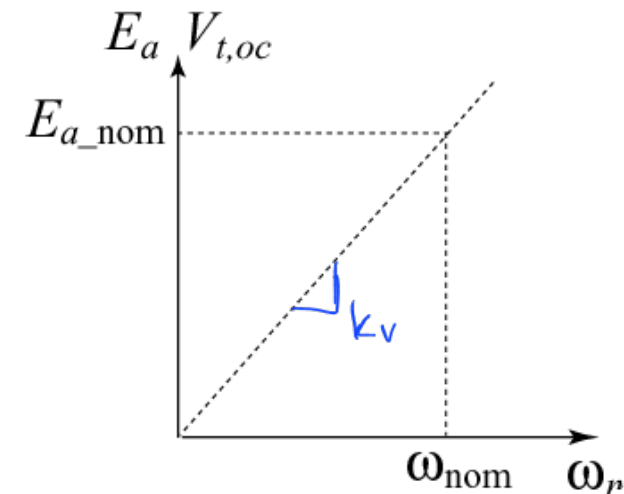
$$k_t = k_v \Rightarrow \frac{V_t - R_a I_a}{\omega_r}$$



Obtain Friction Torque-Speed Characteristic

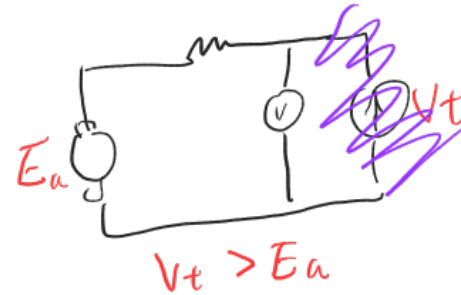
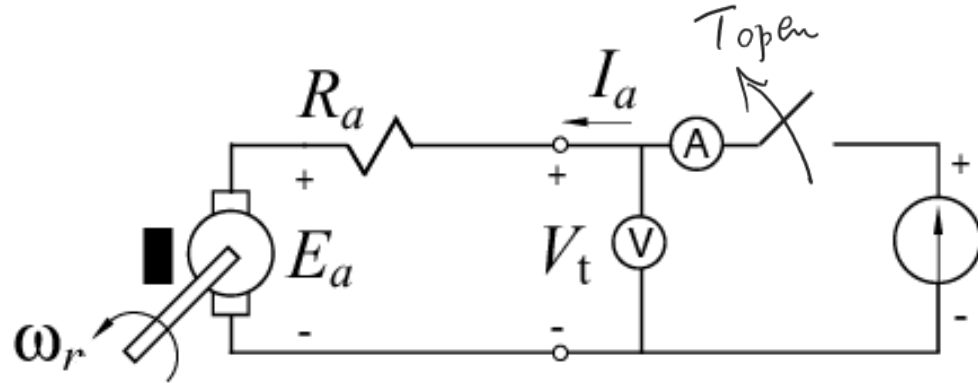
$$T_e = k_t I_a$$

$$T_e = T_{fric}(\omega_r) = \omega_r K_{fric}$$



Parameters of DC Machine

- **Stopping Transient** (for Determining Inertia)



Assume you know $T_{fric}(\omega_r)$

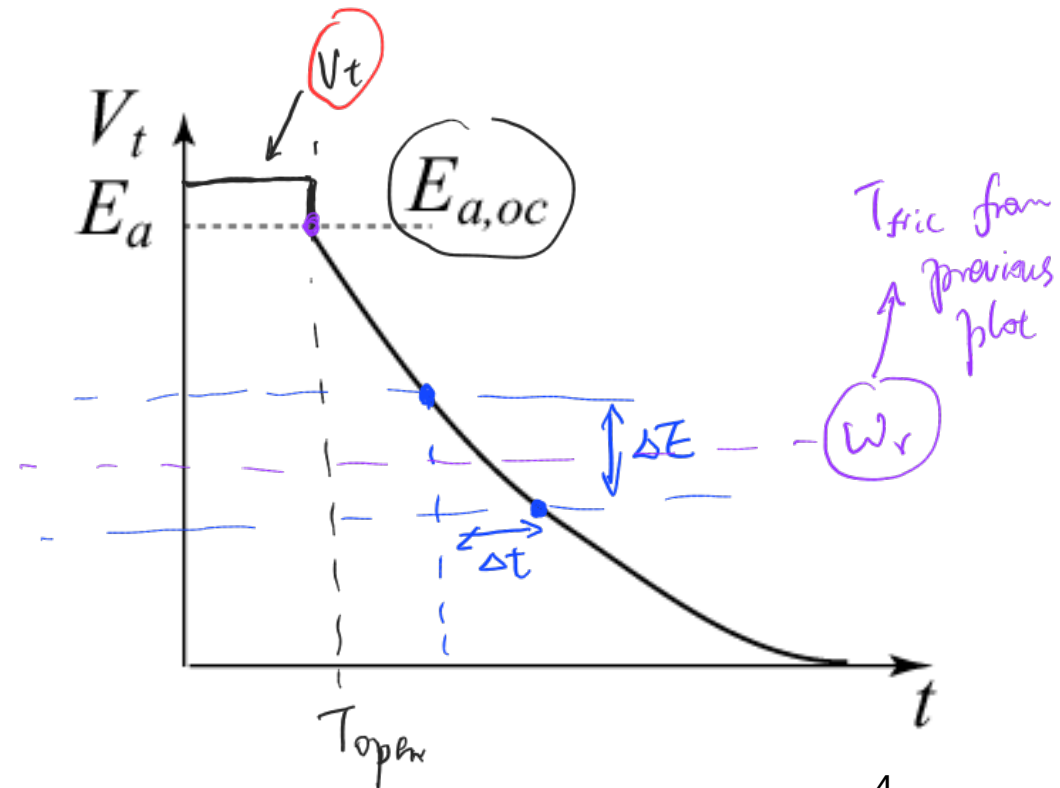
Measure & Record I_a, V_t, ω_r

$$T_e = T_m + T_{fric}(\omega_r) + J \frac{d\omega_r}{dt}$$

$$E_a = K_a \Phi_p \omega_r = K_v \omega_r$$

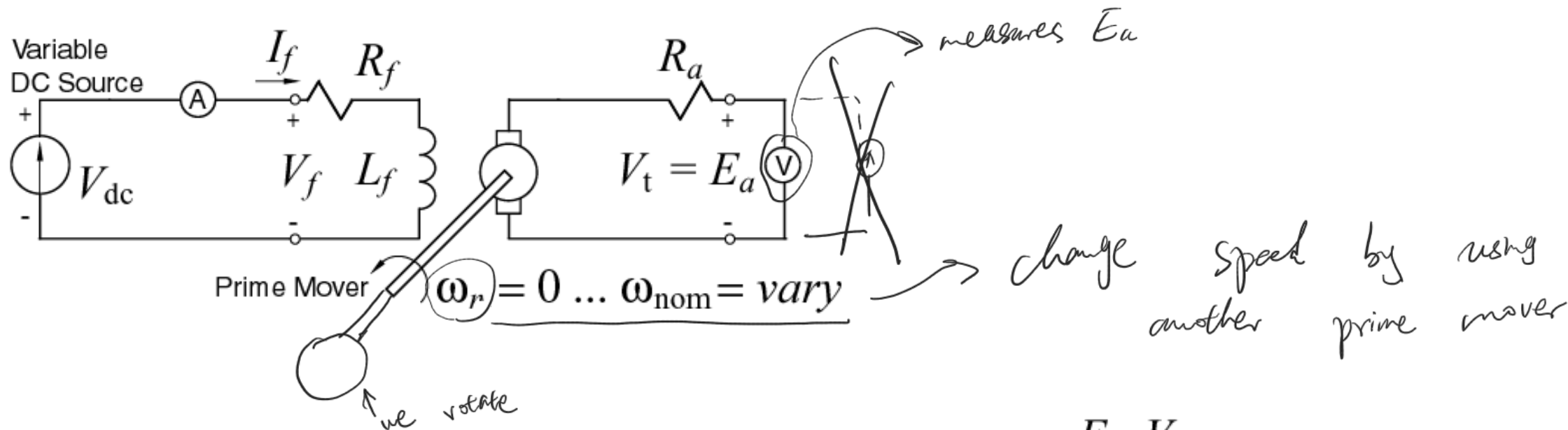
$$\Rightarrow T_{fric}(\omega_r) = -J \frac{\Delta\omega_r}{\Delta t} = -J \frac{\Delta E_a}{K_v \Delta t}$$

$$J = \frac{T_{fric}(\omega_r) \cdot K_v \cdot \Delta t}{\Delta E}$$

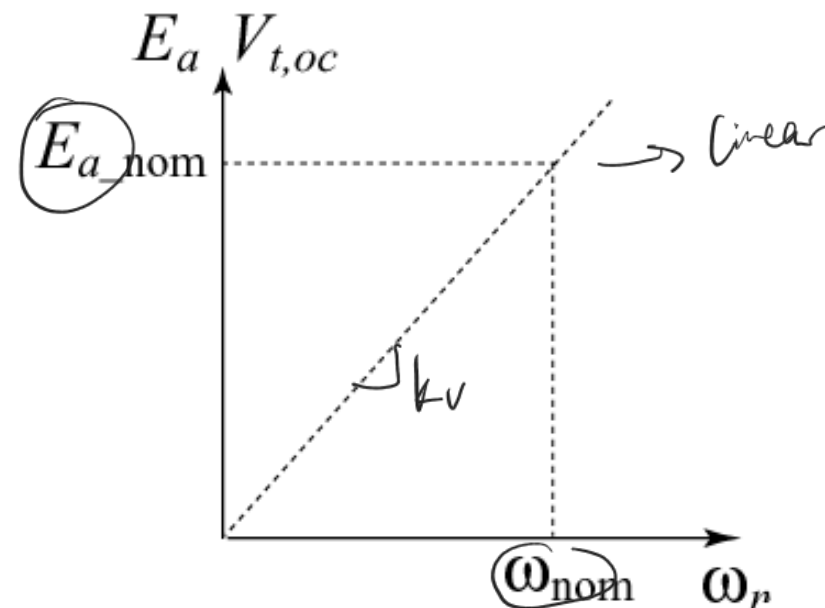


Parameters of DC Machine

- Open-Circuit Test** (Generated Voltage vs. Speed)

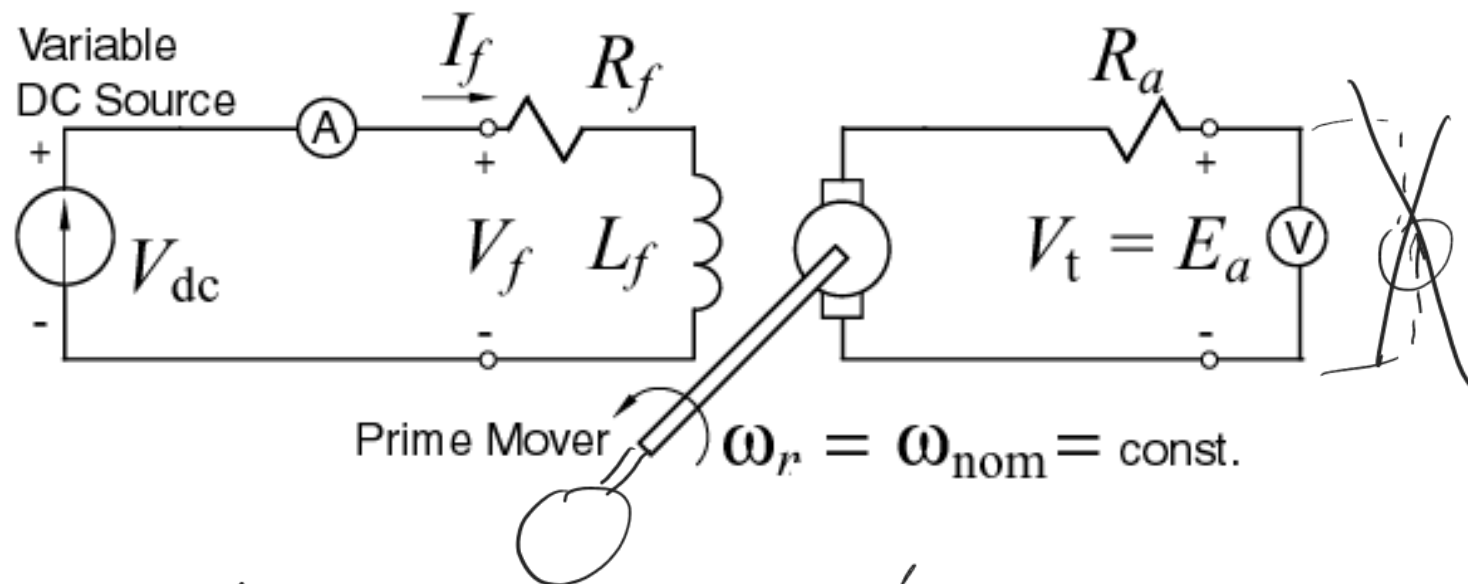


$$\begin{aligned}
 E_a &= K_a \Phi_p \omega_r = K_a \frac{L_f}{N_f} I_f \omega_r \\
 &= \underbrace{L_{af} I_f}_{\text{separately excited}} \omega_r \\
 &= \underbrace{K_v \omega_r}_{PM}
 \end{aligned}$$



Parameters of DC Machine

- **Open-Circuit Test** (Generated Voltage vs. Field Currents)



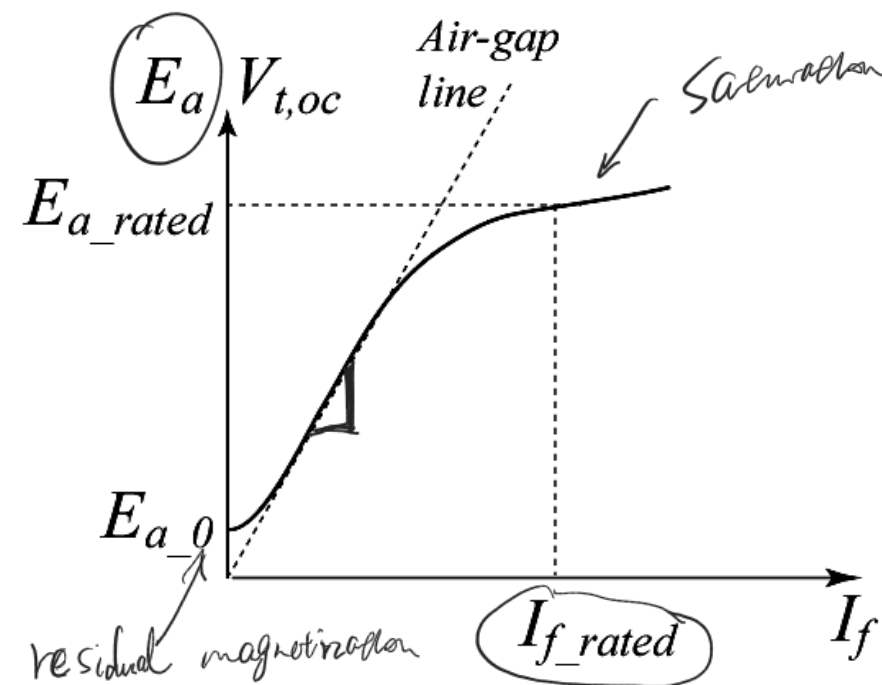
Handwritten notes and equations:

E_a is measured.

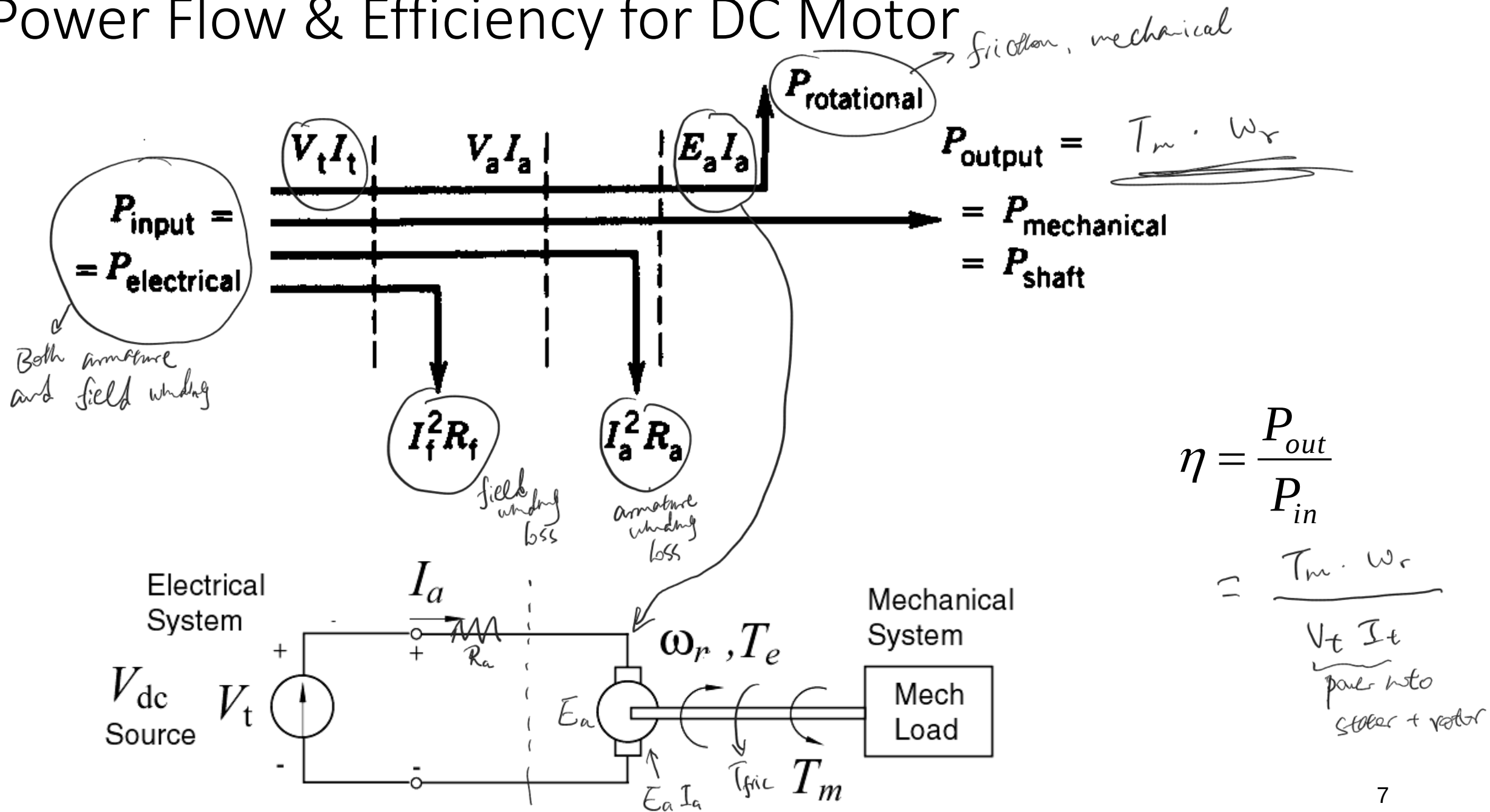
$$E_a = K_a \Phi_p \omega_r = K_a \frac{L_f}{N_f} I_f \omega_r$$

I_f is measured and ω_r is set.

$$= L_{af} I_f \omega_r \Rightarrow \boxed{L_{af} = \frac{E_a}{I_f \omega_r}}$$

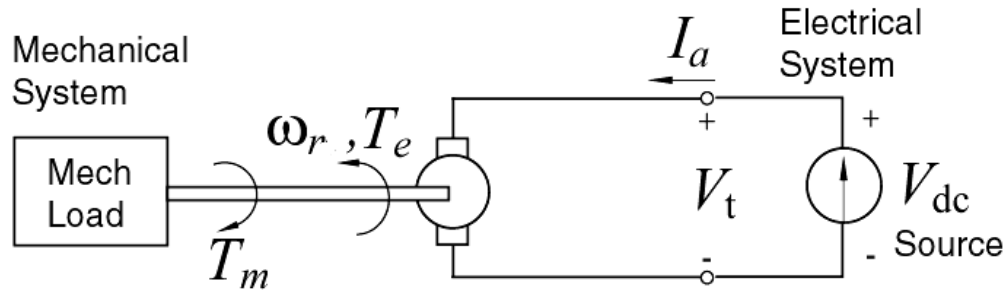


Power Flow & Efficiency for DC Motor



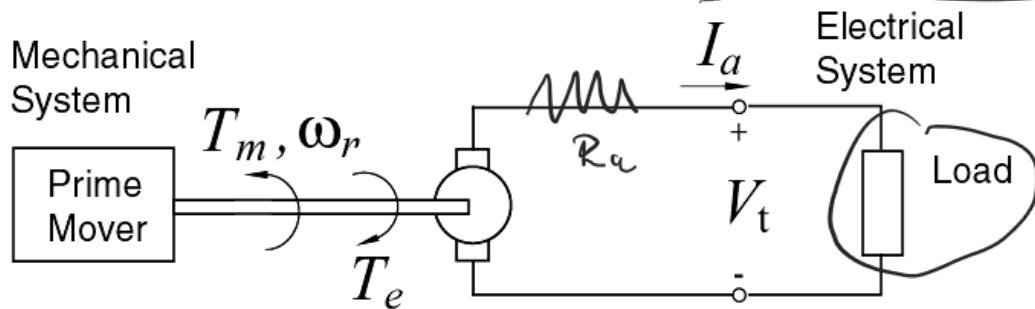
DC Machines Characteristics:

Speed Regulation (for Motors)



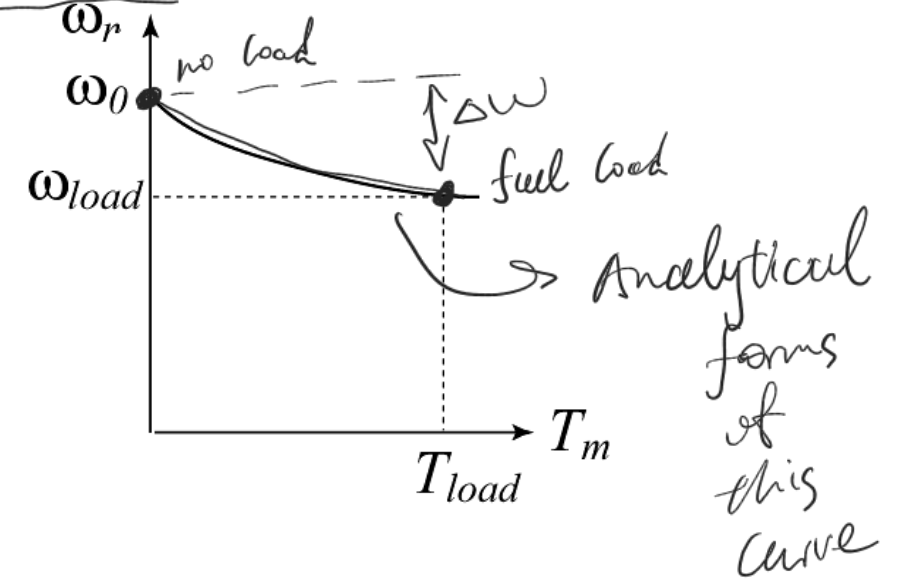
$$SR = \frac{\omega_{r,no_load} - \omega_{r,load}}{\omega_{r,load}} 100\% = \frac{n_{no_load} - n_{load}}{n_{load}} 100\%$$

Voltage Regulation (for Generators)

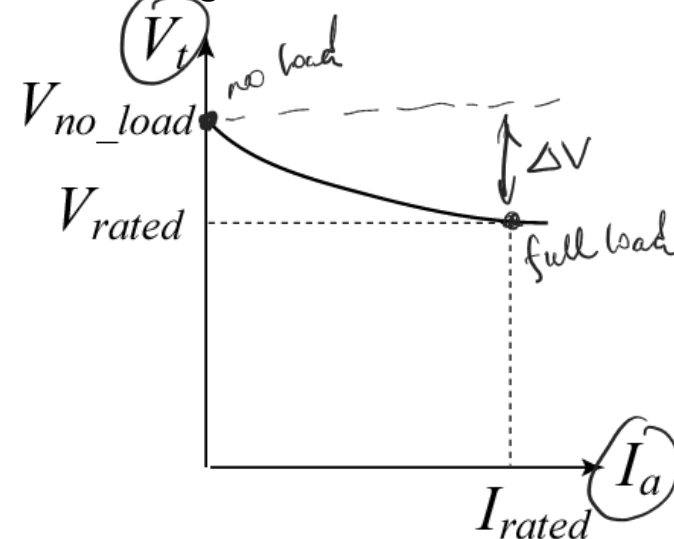


$$VR = \frac{V_{t,oc} - V_{t,load}}{V_{t,load}} 100\% = \frac{V_{no_load} - V_{nom}}{V_{nom}} 100\%$$

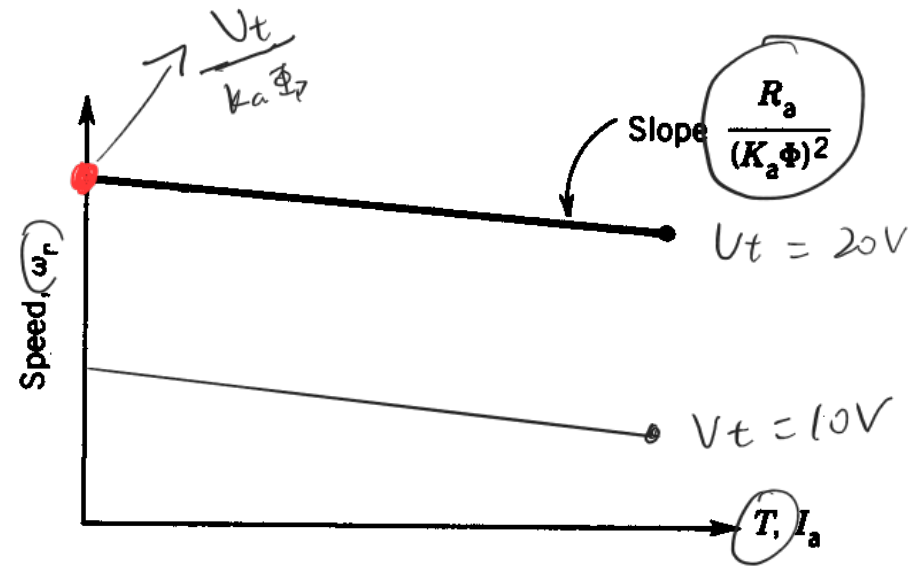
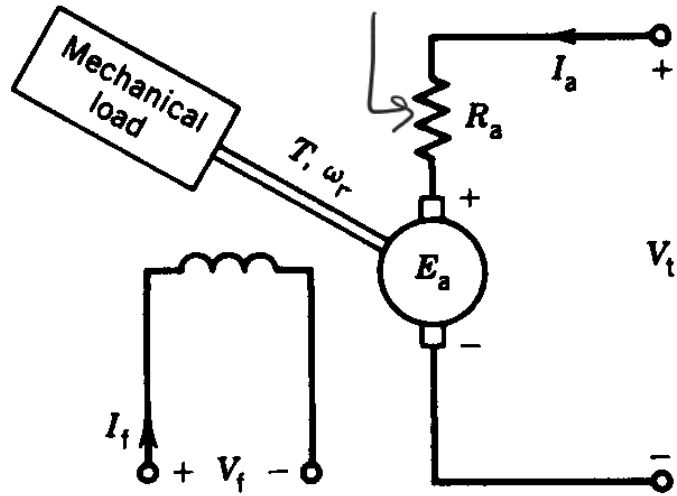
Speed-Torque Characteristic



Load-Voltage Characteristic



Separately-Excited DC Motor or PM DC motor



Speed-Torque Characteristic

$$\omega_r = \frac{V_t - I_a R_a}{K_a \Phi_p} = \frac{V_t - I_a R_a}{L_{af} I_f}$$

Sub. in T_e

$$\Rightarrow \omega_r = \frac{V_t}{K_a \Phi_p} - \frac{R_a}{(K_a \Phi_p)^2} T = \frac{V_t}{L_{af} I_f} - \frac{R_a}{(L_{af} I_f)^2} T$$

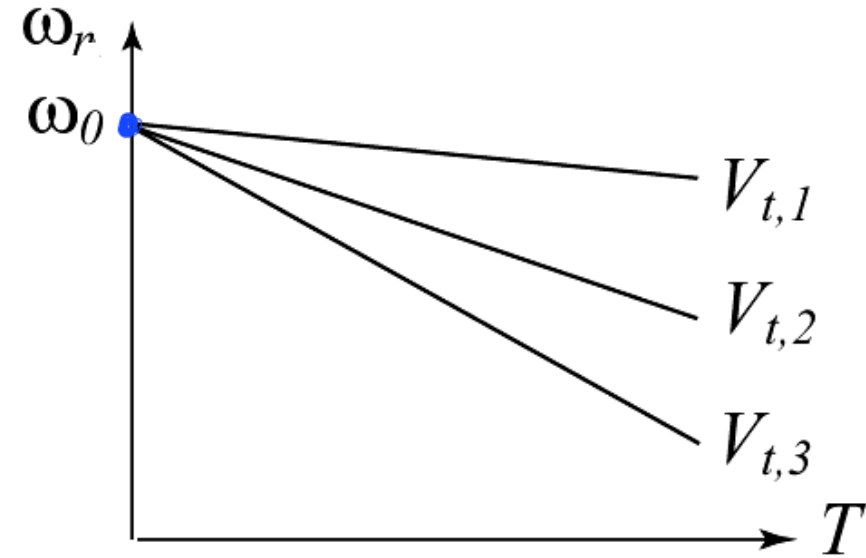
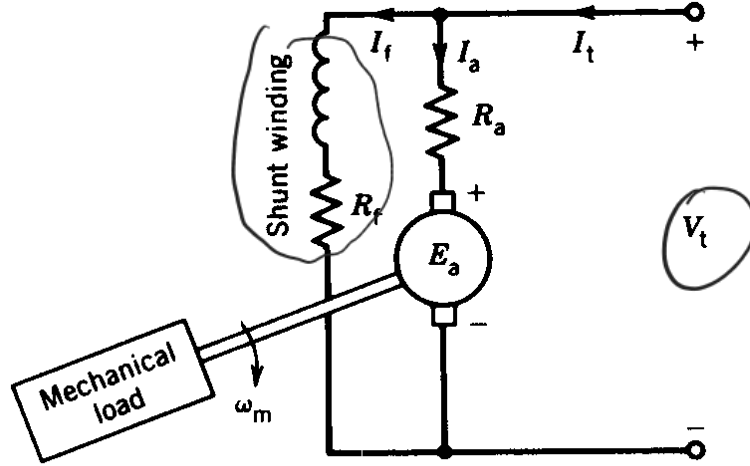
Slope not dependent on V_t

$$\omega_r = f(T)$$

$$\begin{aligned} V_t &= E_a + R_a I_a \Rightarrow E_a = V_t - R_a I_a \\ E_a &= K_a \Phi_p \omega_r = L_{af} I_f \omega_r \\ T &= K_a \Phi_p I_a = L_{af} I_f I_a \end{aligned}$$

Control V_t, R_a, I_f

Shunt DC Motor



$$\omega_r = \frac{V_t}{L_{af} I_f} - \frac{R_a}{(L_{af} I_f)^2} T$$

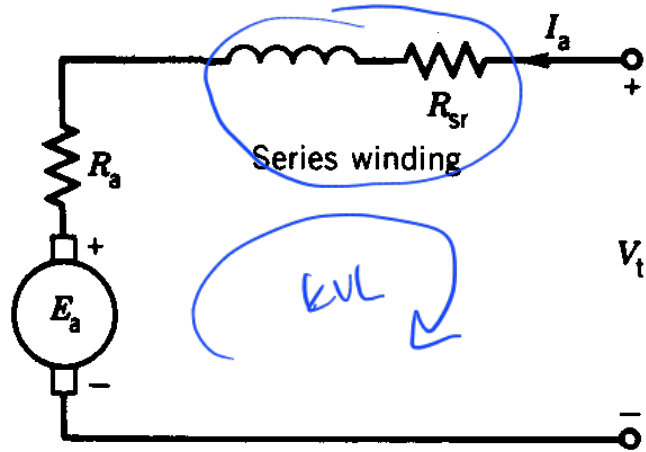
$$L_{af} I_f = \frac{L_{af} V_t}{R_f}$$

Speed-Torque Characteristic

$$\omega_r = \frac{R_f}{L_{af}} - \frac{R_a R_f^2}{(L_{af} V_t)^2} T$$

slope dependent

Series DC Motor

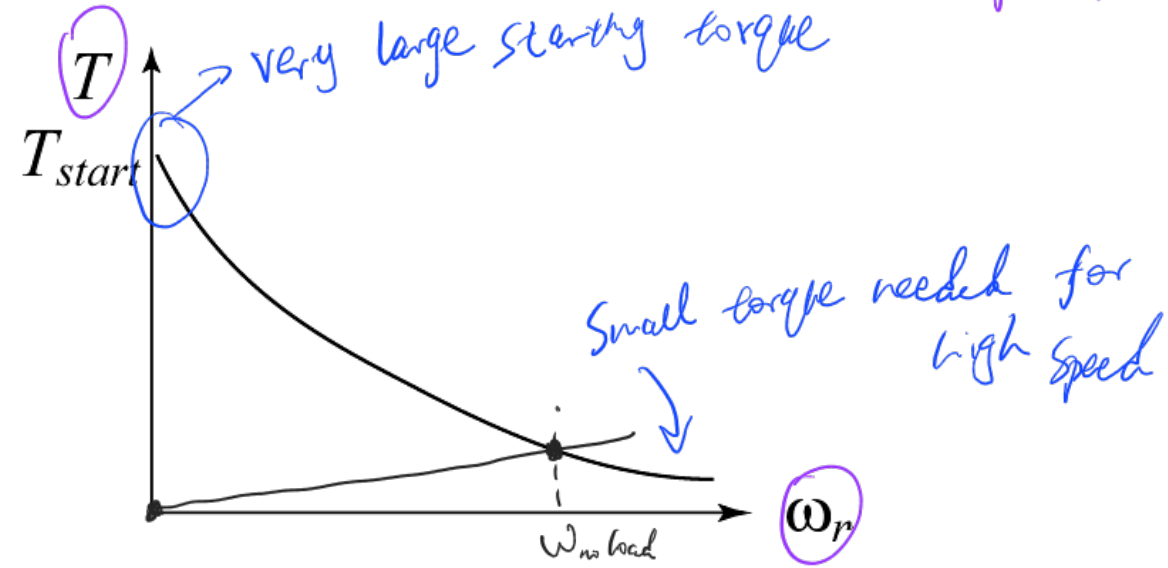


$$V_t = I_a (R_a + R_{sr}) + L_{af} I_a \omega_r$$

$$I_a = \frac{V_t}{R_a + R_{sr} + L_{af} \omega_r}$$

$$T_e = L_{af} I_a^2 = L_{af} I_f I_a$$

↑↑
equal

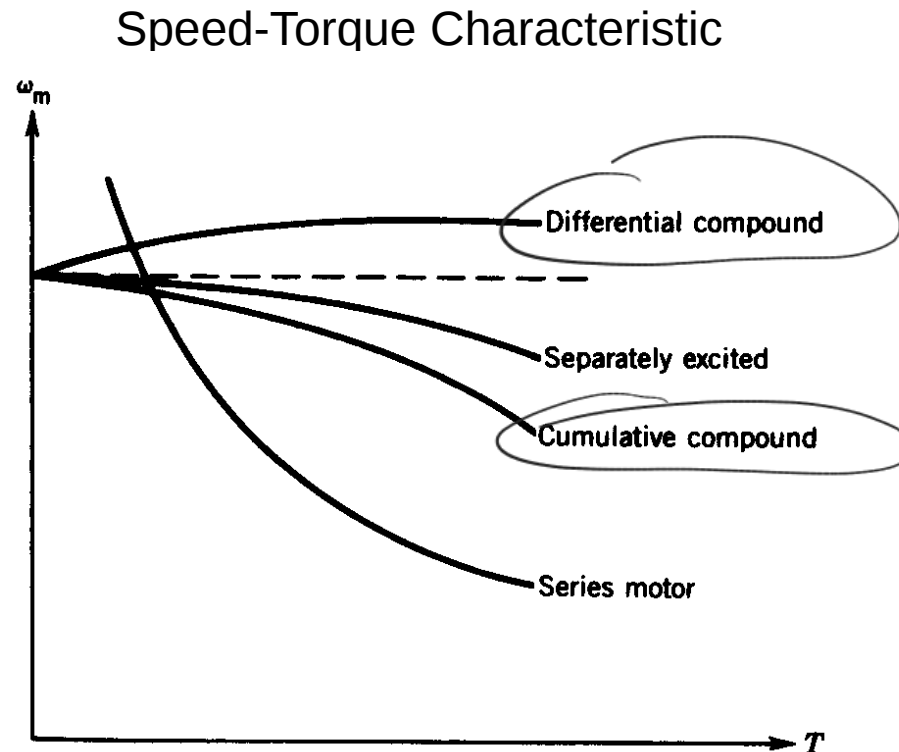
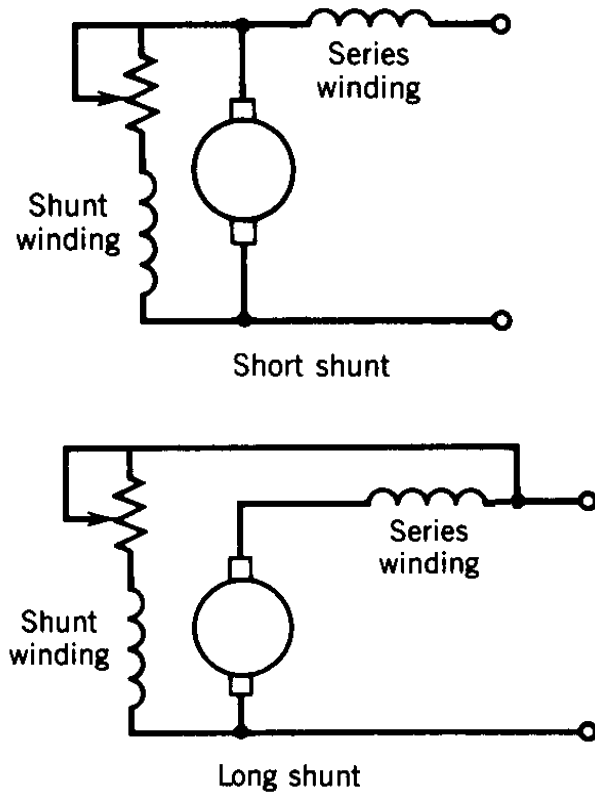


Torque-Speed Characteristic

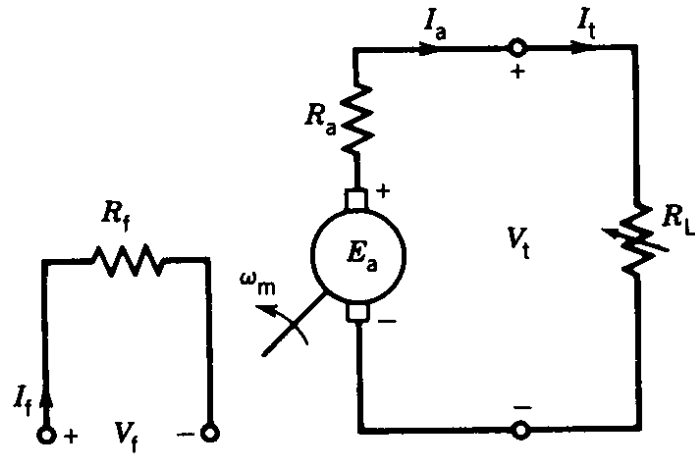
$$T = \frac{L_{af} V_t^2}{(R_a + R_{sr} + L_{af} \omega_r)^2}$$

Compound DC Motor

- Both Shunt and Series field windings are present
- Various connections are possible
- Field windings are designed/adjusted and connected to achieve a desirable torque/speed characteristic



Separately-Excited DC Generator

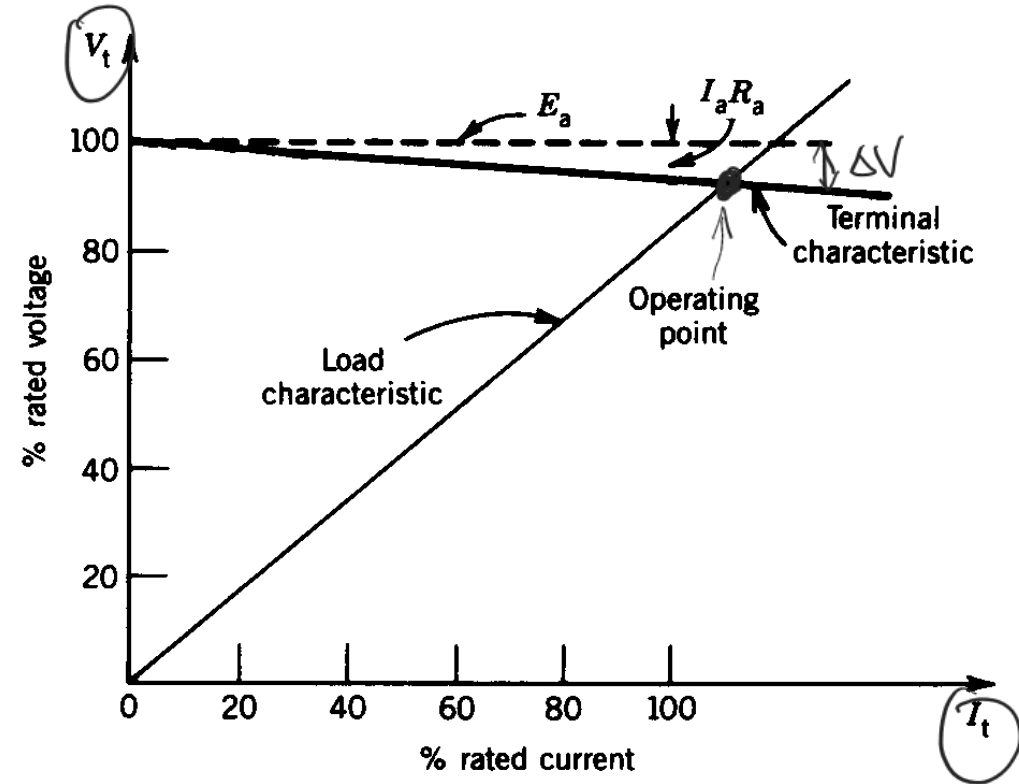


$$V_f = R_f I_f$$

$$E_a = V_t + I_a R_a$$

$$E_a = K_a \Phi_p \omega_r = L_{af} I_f \omega_r$$

$$V_t = I_t R_{load} = I_a R_{load}$$



Load-Voltage Characteristic

$$V_t = E_a - R_a I_a$$

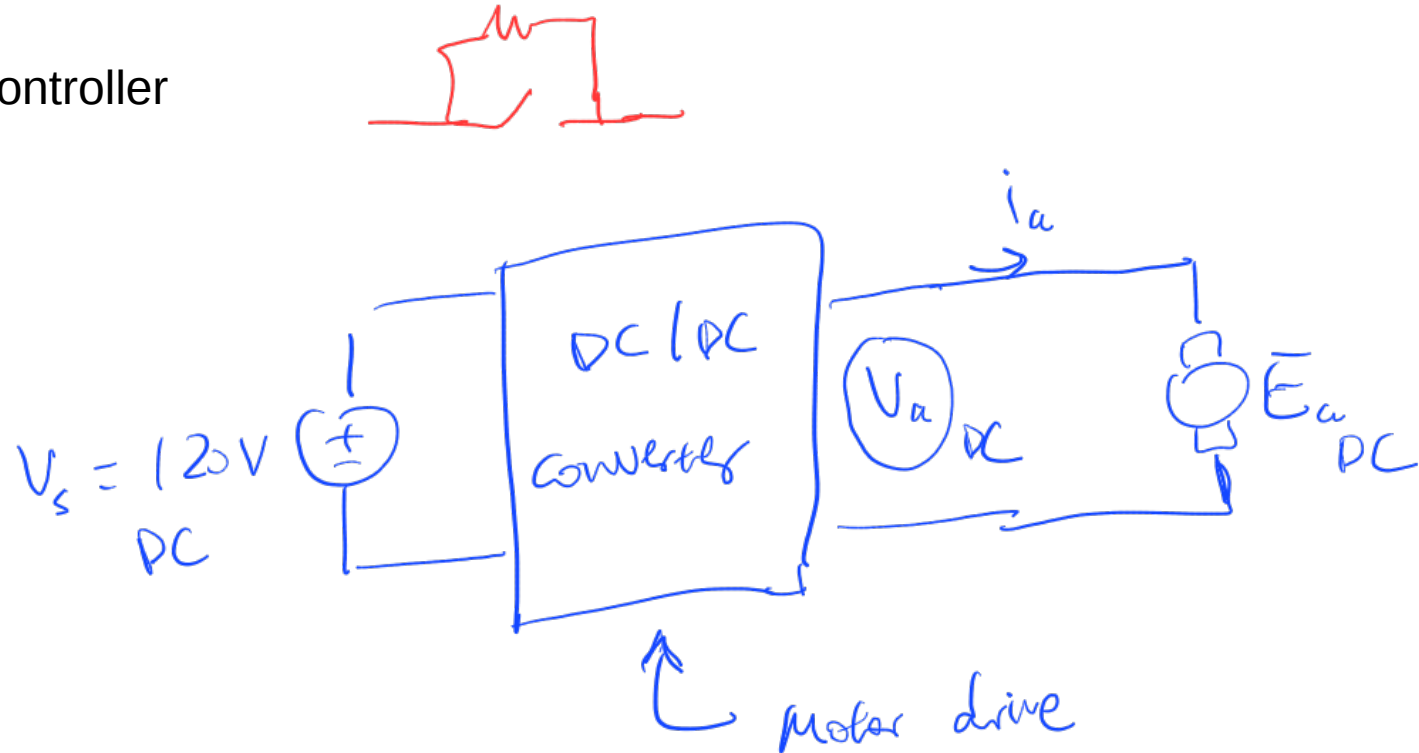
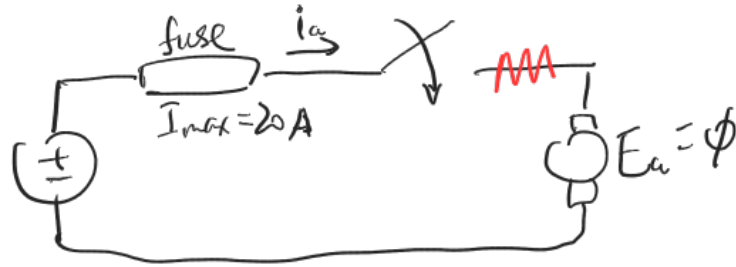
Starting DC machine: Issues and solutions

Consider a 1.2 kW, 120 V, Shunt DC Motor with $R_a = 2 \Omega$, and $I_{a_max} = 20 \text{ A}$

Rated current $I_{a, \text{rated}} = \frac{1200}{120} = 10 \text{ A}$ $\rightarrow E_a \neq 0$

Starting current $I_{a, \text{start}} = \frac{V_t - E_a}{R_a} = \frac{120 - 0}{2} = 60 \text{ A}$ $\rightarrow E_a = 0$ at start up
Too high ! $\Rightarrow$ It can burn the motor and cause damage!

1. Use additional starting resistor in series with armature
2. Use reduced voltage
3. Use Power Electronics Drive & Controller



DC Motor Drives and Dynamics

↳ Use power electronic converter to control DC machine behaviour through feedback control

Important Topics & Concepts

- Basic principles of controlling DC motors
- Four Quadrants of operation
- Power electronic converters
- Dynamic (State) equations of the separately-excited motor
- Dynamic (State) equations of the PM motor
- Possible model & implementations

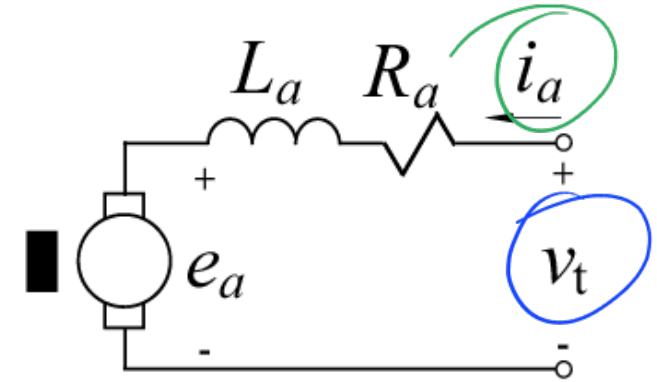
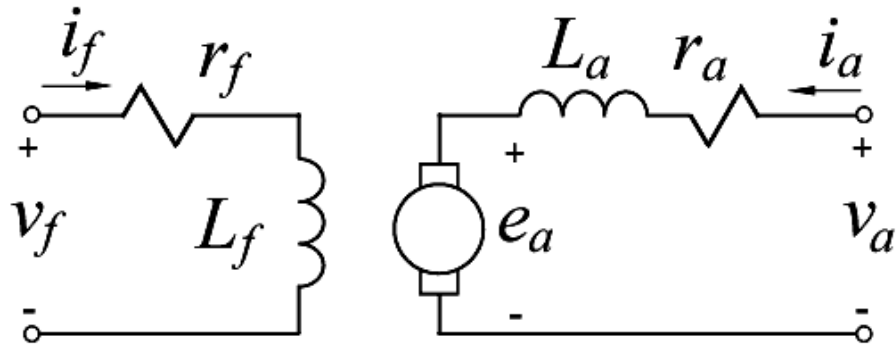
} Lab 3

} MATLAB / Simulink

- Read Chapter 10 of the textbook

Motivation: Speed/Torque Control of DC Motors

Recall Separately Excited DC Motor and PM DC Motor



$$\omega_r = \frac{V_t}{K_a \Phi_p} - \frac{R_a}{(K_a \Phi_p)^2} T = \frac{V_t}{L_{af} I_f} - \frac{R_a}{(L_{af} I_f)^2} T$$

$$T = K_a \Phi_p I_a = L_{af} I_f I_a$$

Control methods:

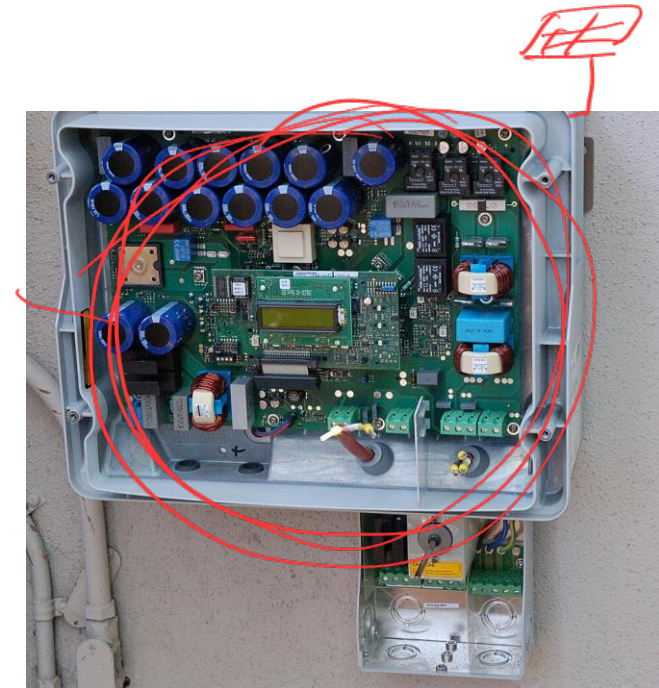
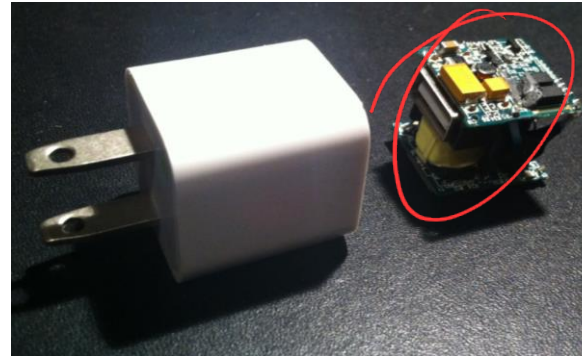
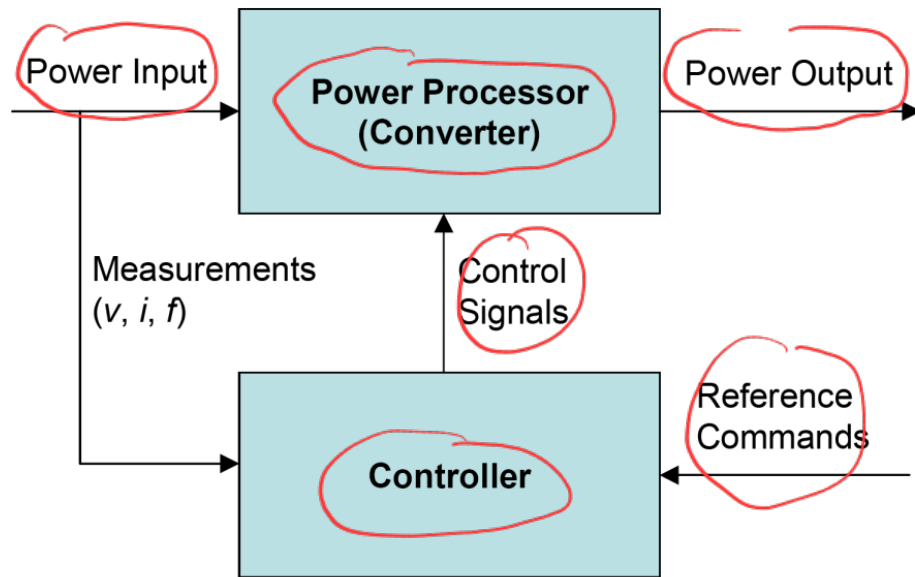
1. Varying armature resistance (not practical due to high losses)
2. Varying field (only for field winding)
3. Varying terminal voltage
4. Varying armature current

Power electronics

V, I, f

- Power electronics refers to the study of electronic circuits which efficiently process and transfer the electric power from the available form to a desired form using semiconductor switching devices $\rightarrow$ solid-state circuits

$I_{input} = I_{output}$



Conversion types

- input → output
- DC-DC converters (choppers)
 - For small & large DC motor drives

- AC-DC rectifiers
 - For large DC motor drives

- DC-AC inverters → solar, battery

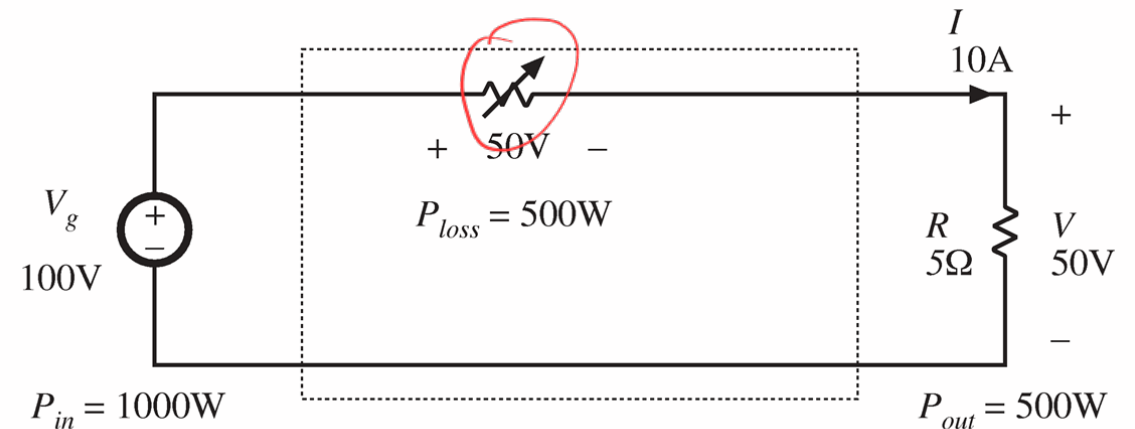
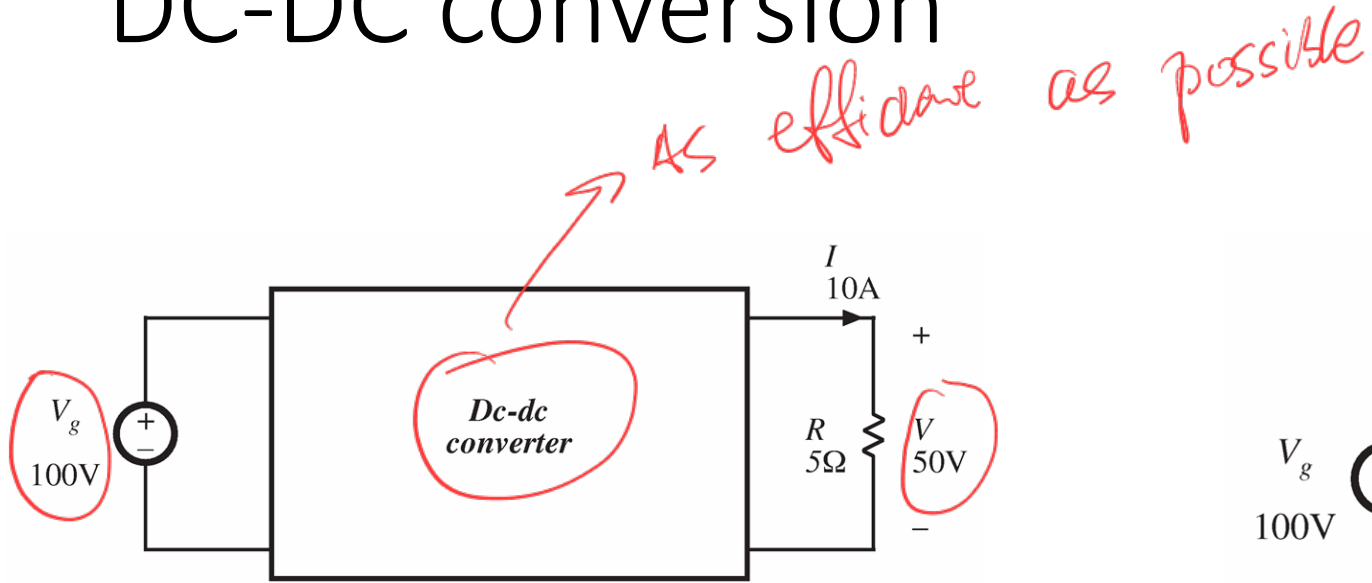
- AC-AC cycloconverters

→ ELEC 451

→ ELEC 571D

↳ P.E for grid level application

DC-DC conversion

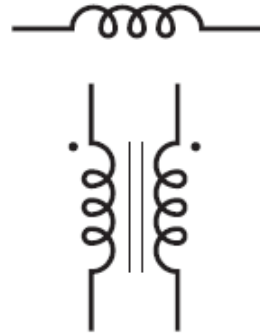


Power losses

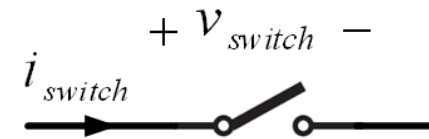
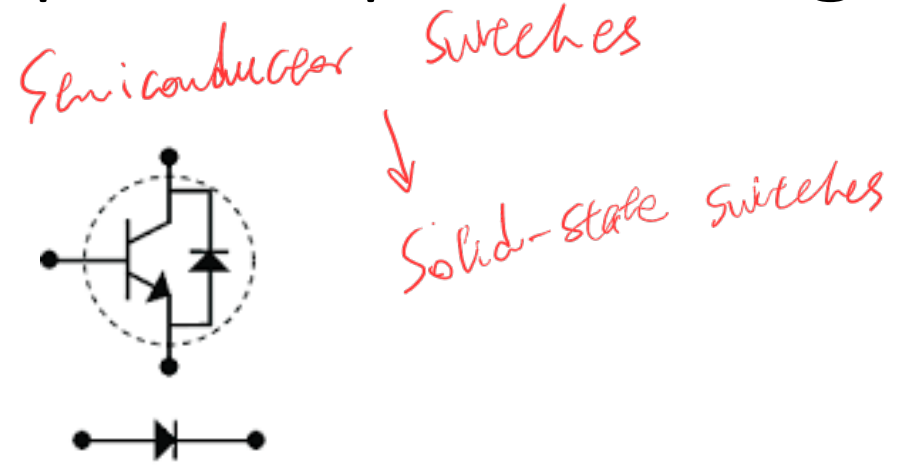
Components available for lossless power processing



Capacitor



magnetics



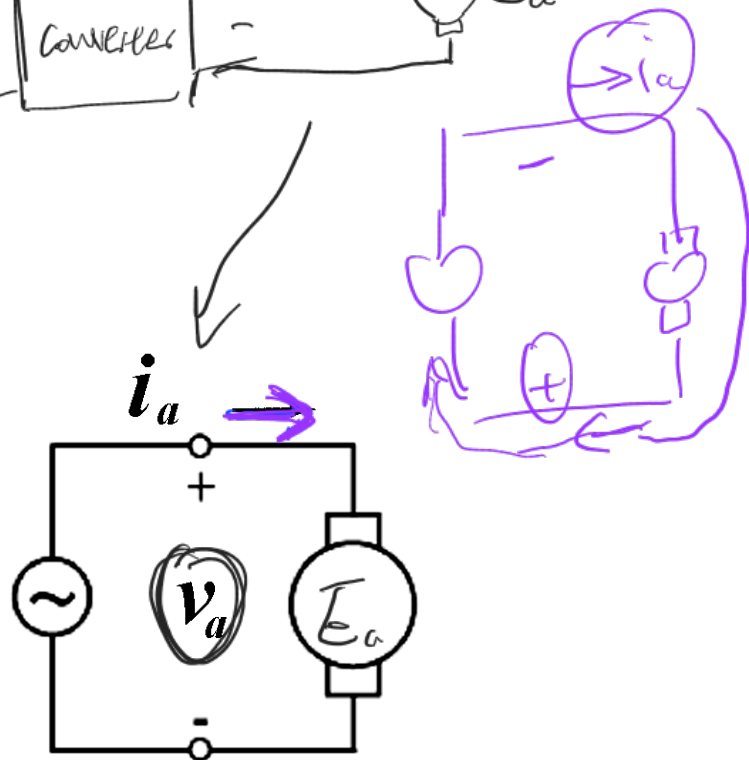
Switch can be realized using:

- Insulated Gate Bipolar Transistor (**IGBT**)
- Metal Oxide Semiconductor Field Effect Transistor (**MOSFET**)

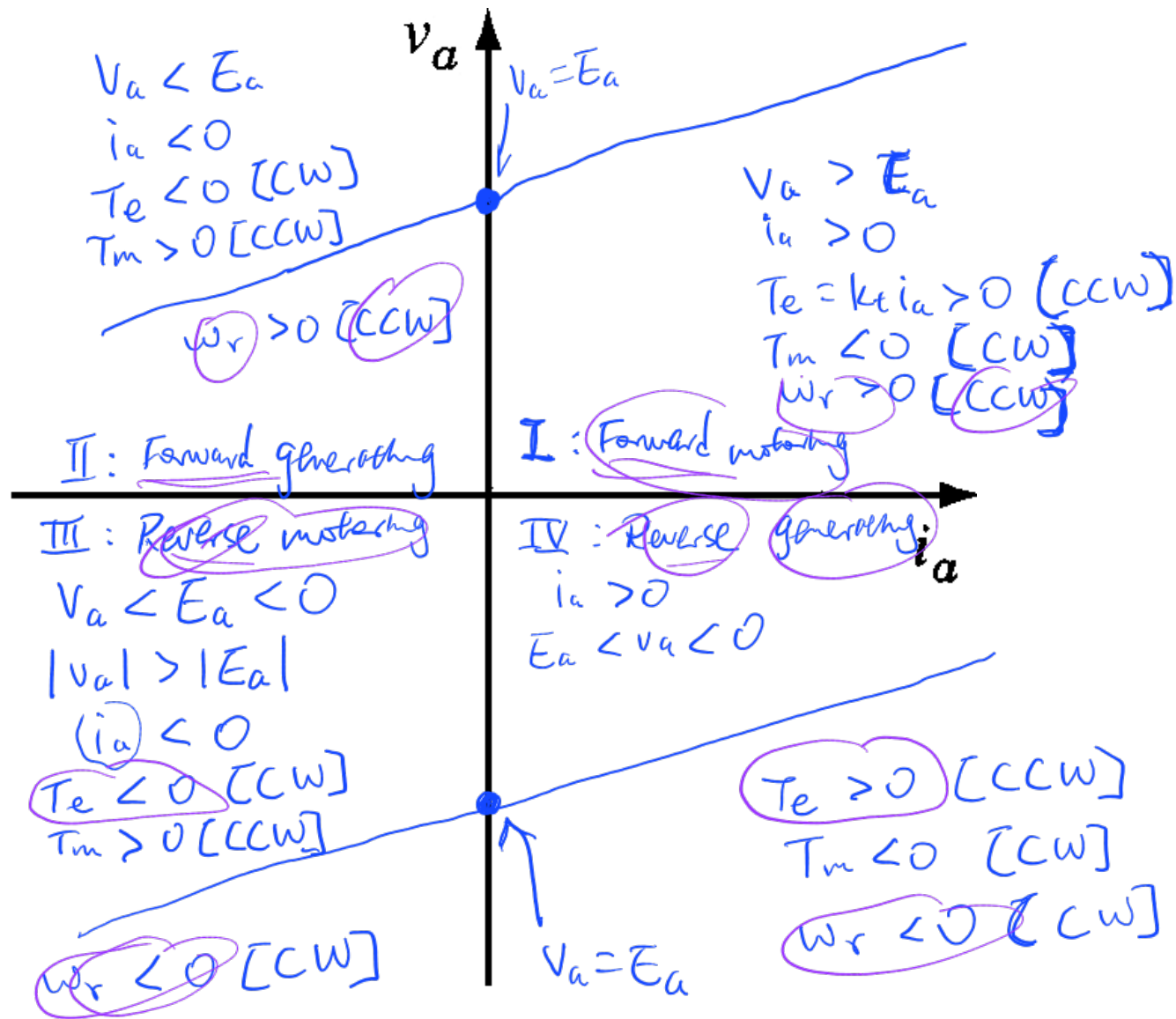
DC-DC Converters Quadrants

Define CCW as positive rotation, CW as negative rotation

Assume a DC voltage source wherein the averaged output voltage can be controlled



$$\bar{V}_a = \frac{1}{T} \int_0^T v_a(t) dt$$



DC-DC Converters Quadrants - Summary

	Quadrant I	Quadrant II	Quadrant III	Quadrant IV
Name	Forwarding motoring	Forward generating	Reverse motoring	Reverse generating
E_a, V_a	$V_a > E_a > 0$	$E_a > V_a > 0$	$V_a < E_a < 0$	$E_a < V_a < 0$
I_a	$I_a > 0$	$I_a < 0$	$I_a < 0$	$I_a > 0$
T_e	Positive (CCW)	Negative (CW)	Negative (CW)	Positive (CCW)
T_m	Negative (CW)	Positive (CCW)	Positive (CCW)	Negative (CW)
ω_r	Positive (CCW)	Positive (CCW)	Negative (CW)	Negative (CW)
Example	Car in forward (drive) mode going uphill	Car in forward (drive) mode going downhill	Car in reverse mode going uphill	Car in reverse mode going downhill

Looking ahead...

- Continue **Module 4**