

ELEC 342

Electromechanical Energy Conversion and Transmission

2025-26 Winter Term 2

Lecture 12

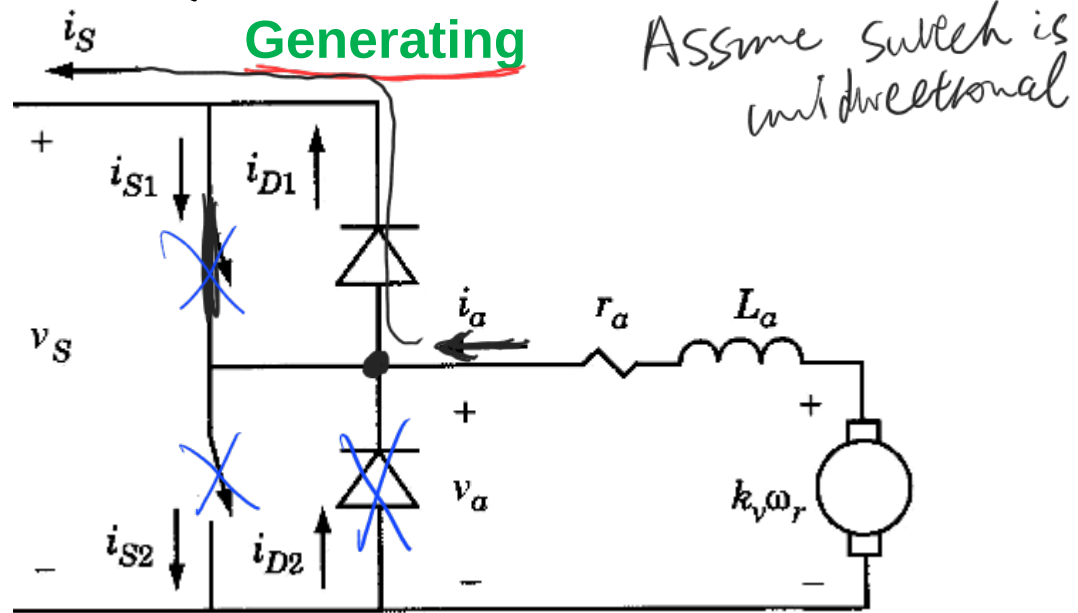
February 12, 2026

Zhi Jin (Justin) Zhang

Course Logistics

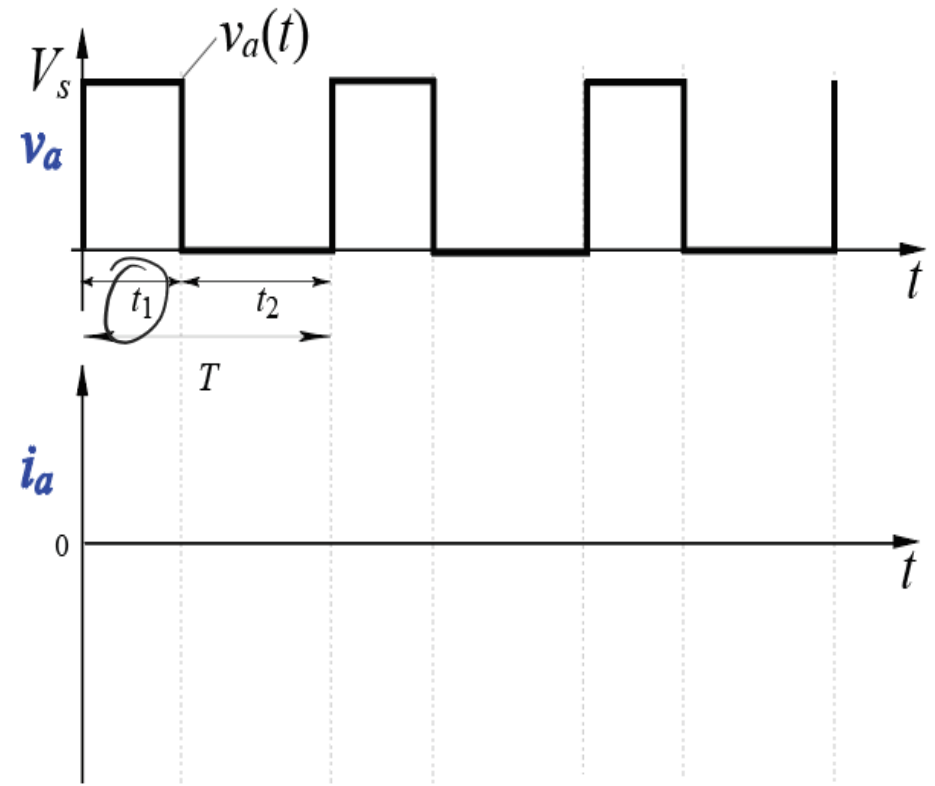
- **Labs:**
 - **Please be on time and come prepared**
 - **Each person needs to complete prelab and submit as a part of the final lab report**
 - **You need to submit all five (5) lab reports in order to write the final exam**
- Quiz 2 will take place on Feb. 13
- Midterm will take place on Feb. 26

Two-Quadrant DC-DC Converter



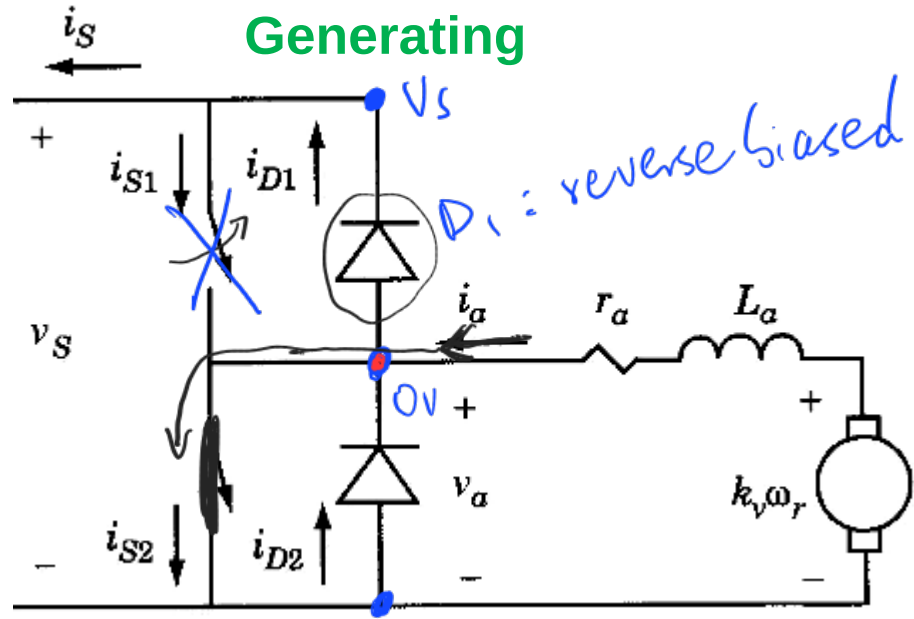
Pulse Width Modulation (PWM)

Assume complementary switching



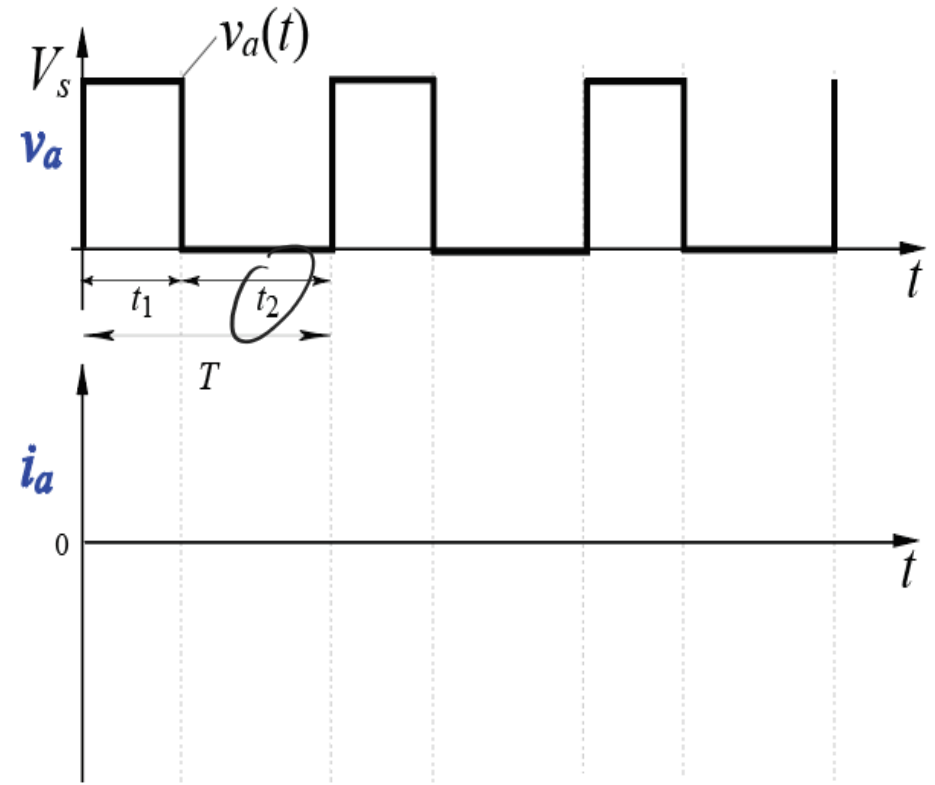
Duty cycle

Two-Quadrant DC-DC Converter



Pulse Width Modulation (PWM)

Assume complementary switching



Duty cycle

State Equations for DC Motor with Field Winding

State Equations -> ODEs

$$\frac{di_a}{dt} = -\frac{r_a}{L_a}i_a - \frac{1}{L_a}e_a + \frac{1}{L_a}v_a$$

$$\frac{di_f}{dt} = -\frac{r_f}{L_f}i_f + \frac{1}{L_f}v_f$$

$$\frac{d\omega_r}{dt} = -\frac{D_m}{J}\omega_r + \frac{1}{J}(T_e - T_m)$$

Coupling Terms

$$e_a = \omega_r L_{af} i_f$$

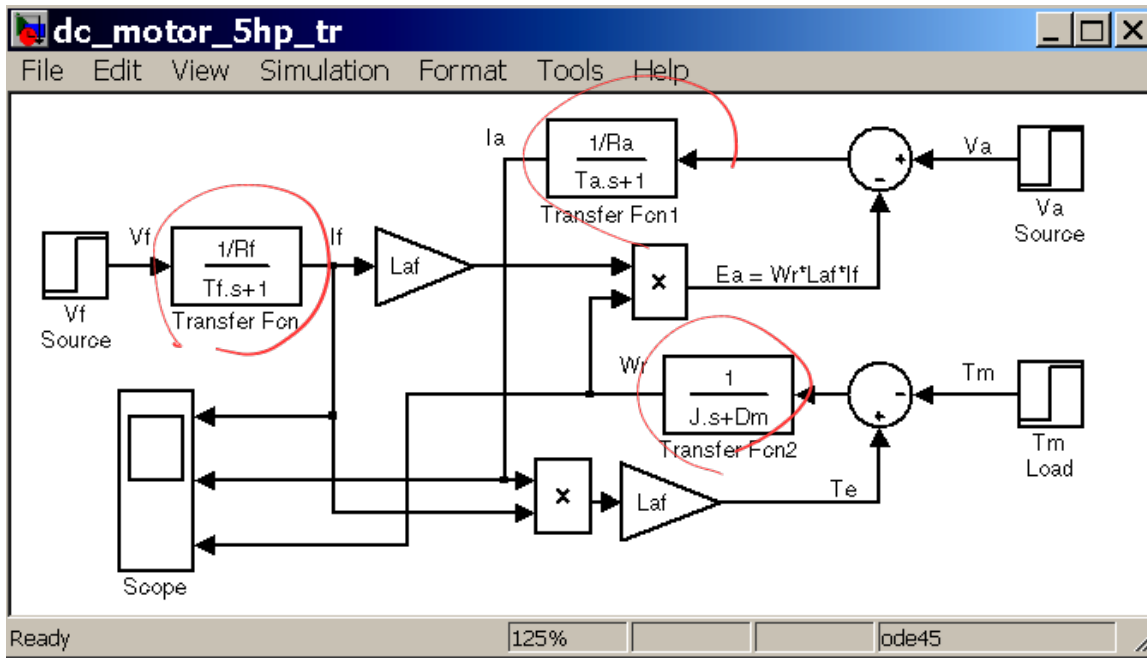
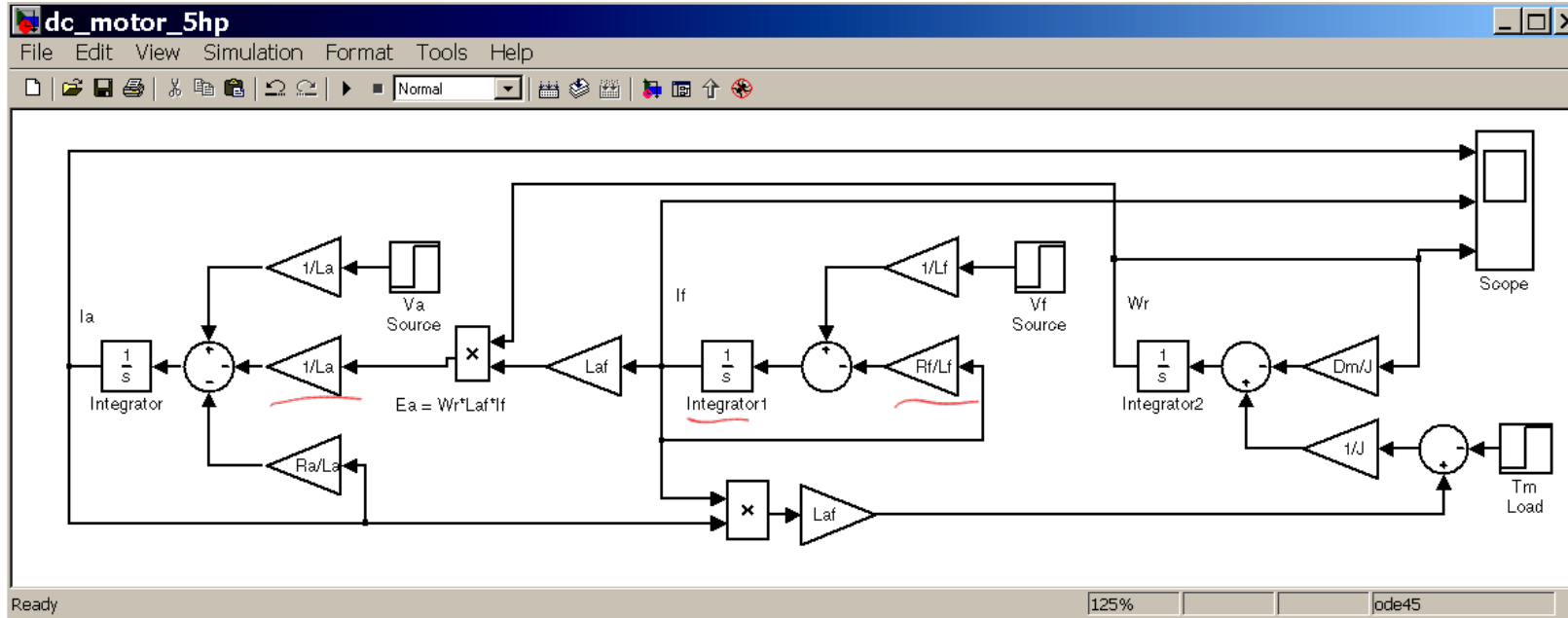
$$T_e = L_{af} i_f i_a$$

Are these equations coupled or decoupled ? *Coupled*

Are these equations linear or non-linear ? *Nonlinear*

How do we solve these equations ? *Difficult to solve analytically
numerical methods need to be used*

5-HP DC Motor (With Field Winding) Simulink Model



Try to do it yourself

- Both models are absolutely equivalent
- Models behave like “virtual” DC machine

Dynamic Response of a 5-HP DC Motor

Example: Motor parameters:

$V_a = V_f = 240$ V, $R_f = 240$ Ω , $L_f = 120$ H, $R_a = 0.6$ Ω , $L_a = 0.012$ H, $L_{af} = 1.8$ H, $J = 1$ kg*m², $D_m = 1e-4$ N*m*s, $T_m = 29.2$ N*m

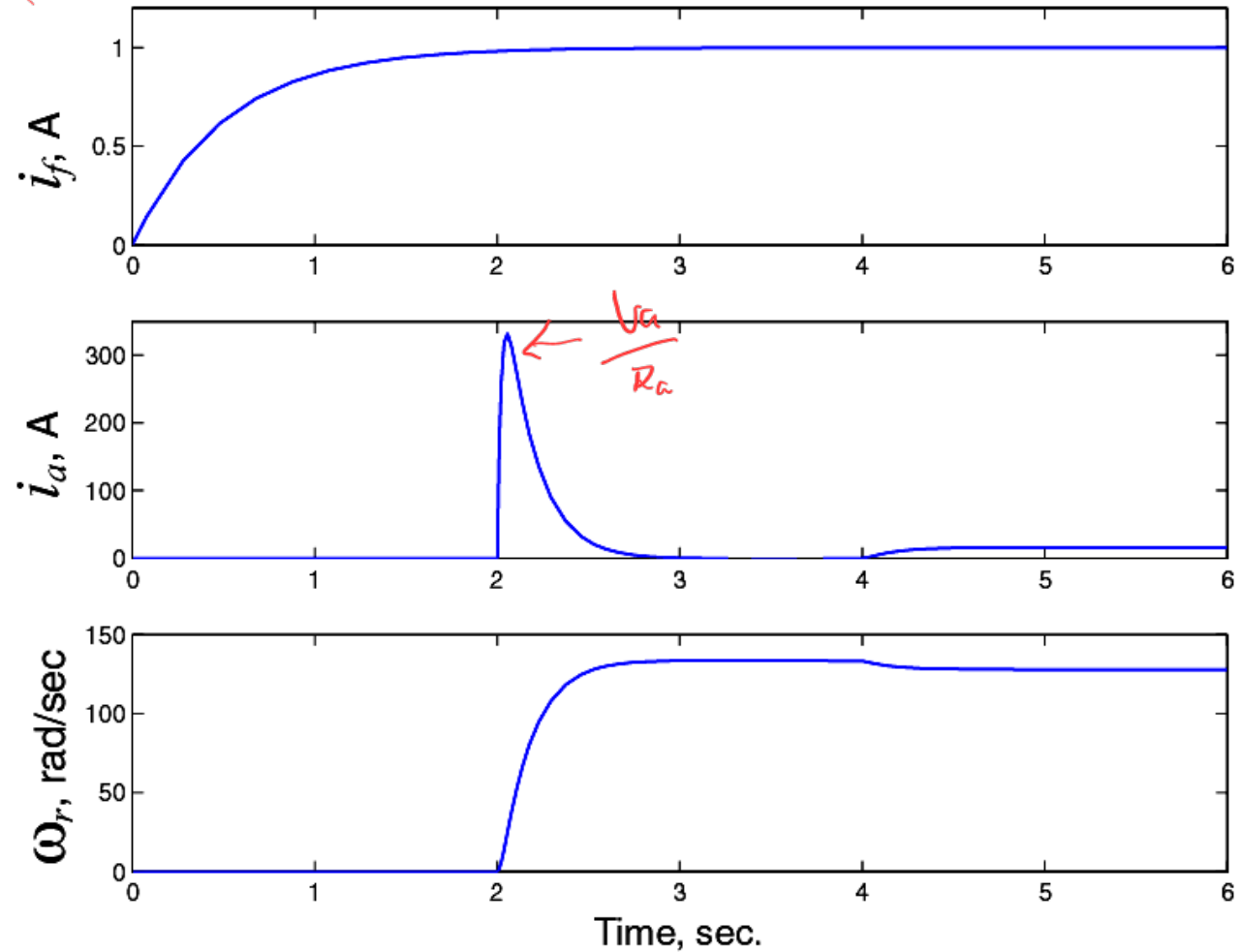
In this computer study:

Zero initial conditions assumed

Step-1: field winding is energized

Step-2: armature is energized

Step-3: load torque is applied



Dynamic Modeling of PM DC Machine *→ simpler*

State Equations

$$\frac{di_a}{dt} = -\frac{r_a}{L_a} i_a - \frac{1}{L_a} e_a + \frac{1}{L_a} v_a$$

$$\frac{d\omega_r}{dt} = -\frac{D_m}{J} \omega_r + \frac{1}{J} (T_e - T_m)$$

Coupling Terms

$$e_a = k_v \omega_r \quad T_e = k_v i_a$$

Are these equations coupled or decoupled? *Coupled*

Are these equations linear or non-linear? *Linear*

How do we solve these equations? *Analytically possible*

Standard State-Space Form

Lots of analytical tools

$$\frac{d}{dt} \begin{bmatrix} i_a \\ \omega_r \end{bmatrix} = \underbrace{\begin{bmatrix} -\frac{r_a}{L_a} & -\frac{k_v}{L_a} \\ \frac{k_v}{J} & -\frac{D_m}{J} \end{bmatrix}}_A \underbrace{\begin{bmatrix} i_a \\ \omega_r \end{bmatrix}}_x + \underbrace{\begin{bmatrix} \frac{1}{L_a} & 0 \\ 0 & -\frac{1}{J} \end{bmatrix}}_B \underbrace{\begin{bmatrix} v_a \\ T_m \end{bmatrix}}_u$$

$$\frac{dx}{dt} = \mathbf{Ax} + \mathbf{Bu}$$

State variables
 $\dot{x} = Ax + Bu$
input variable

Implementation of the state equations

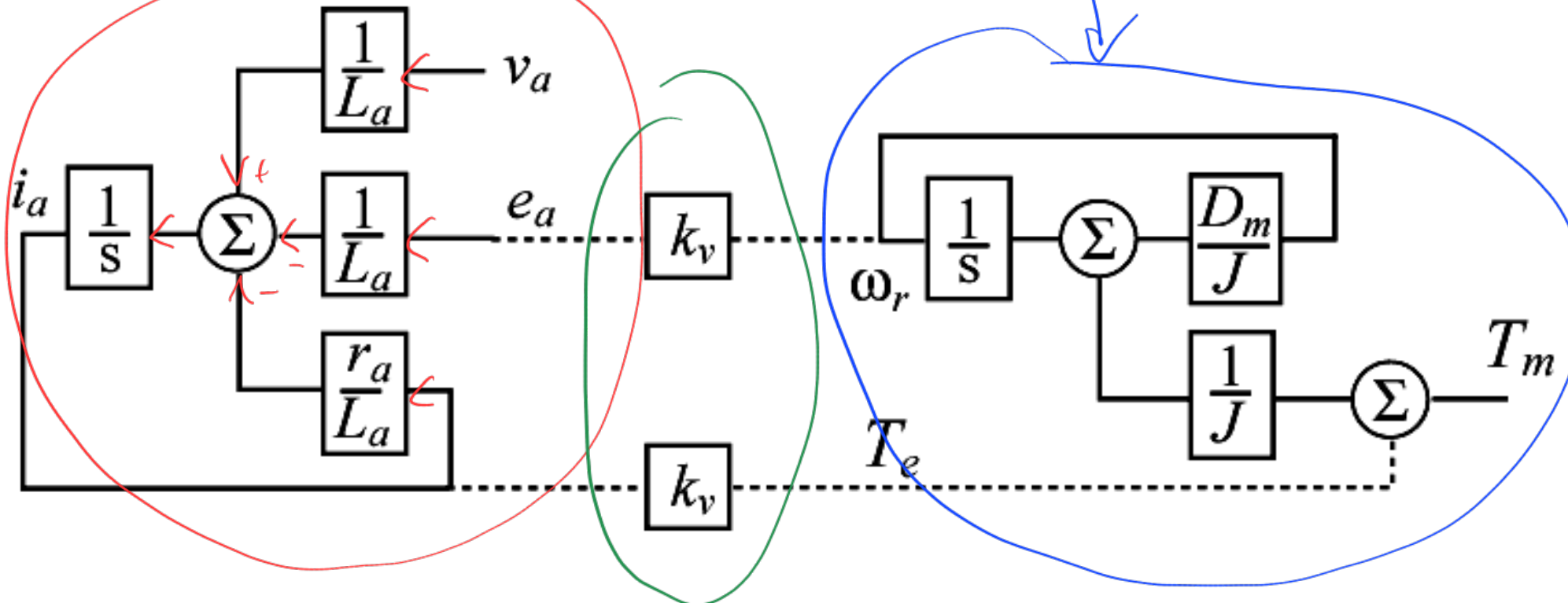
State Equations

$$\frac{di_a}{dt} = -\frac{r_a}{L_a}i_a - \frac{1}{L_a}e_a + \frac{1}{L_a}v_a$$

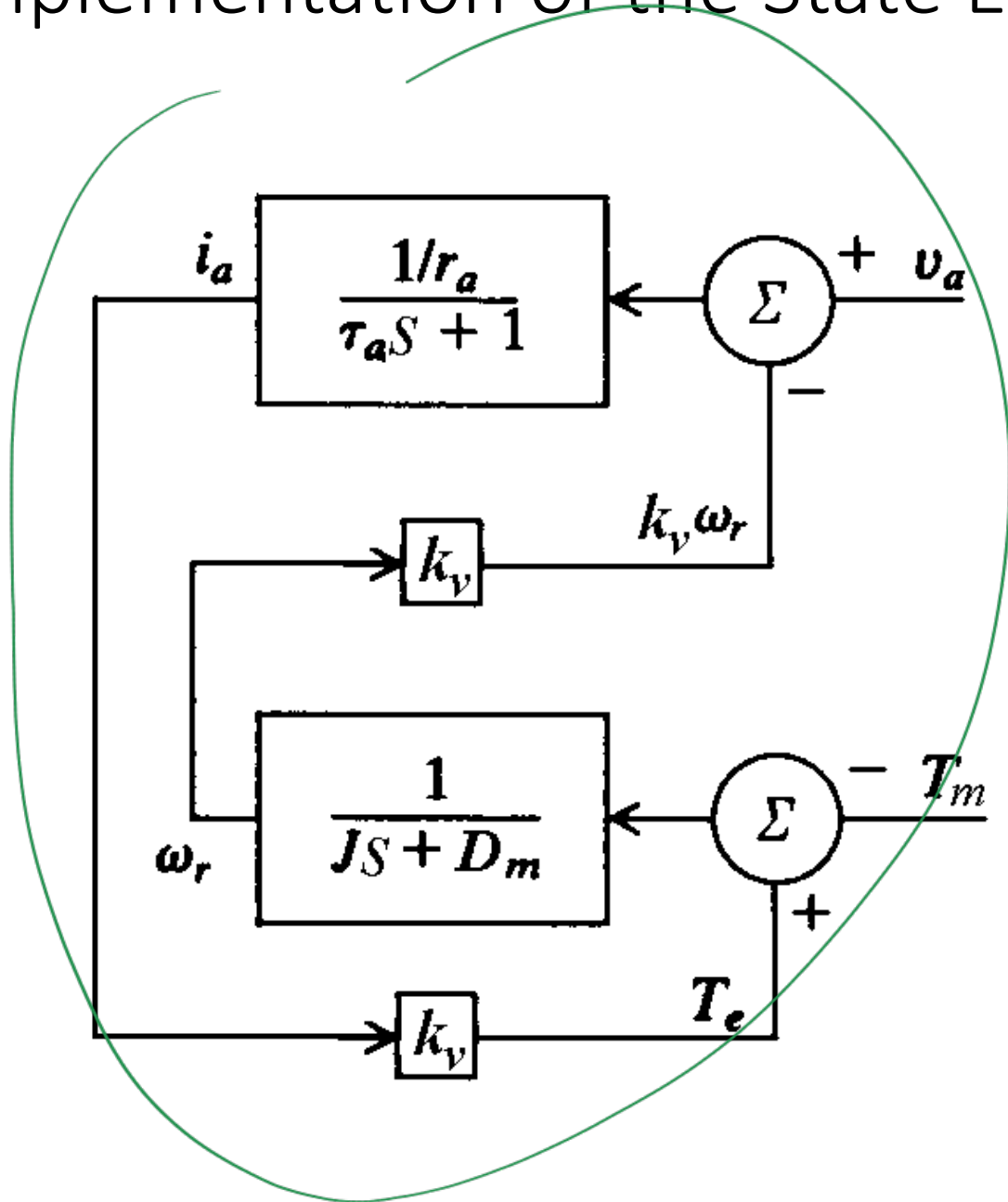
$$\frac{d\omega_r}{dt} = -\frac{D_m}{J}\omega_r + \frac{1}{J}(T_e - T_m)$$

Coupling Terms

$$e_a = k_v \omega_r \quad T_e = k_v i_a$$



Implementation of the State Equations



Re-write the equations in s-domain

$$v_a = r_a (1 + \tau_a s) i_a + e_a$$

$$e_a = k_v \omega_r$$

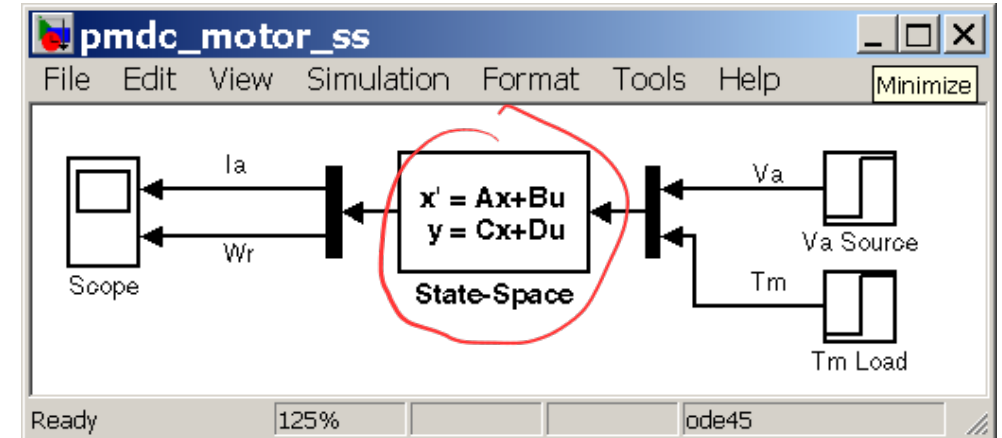
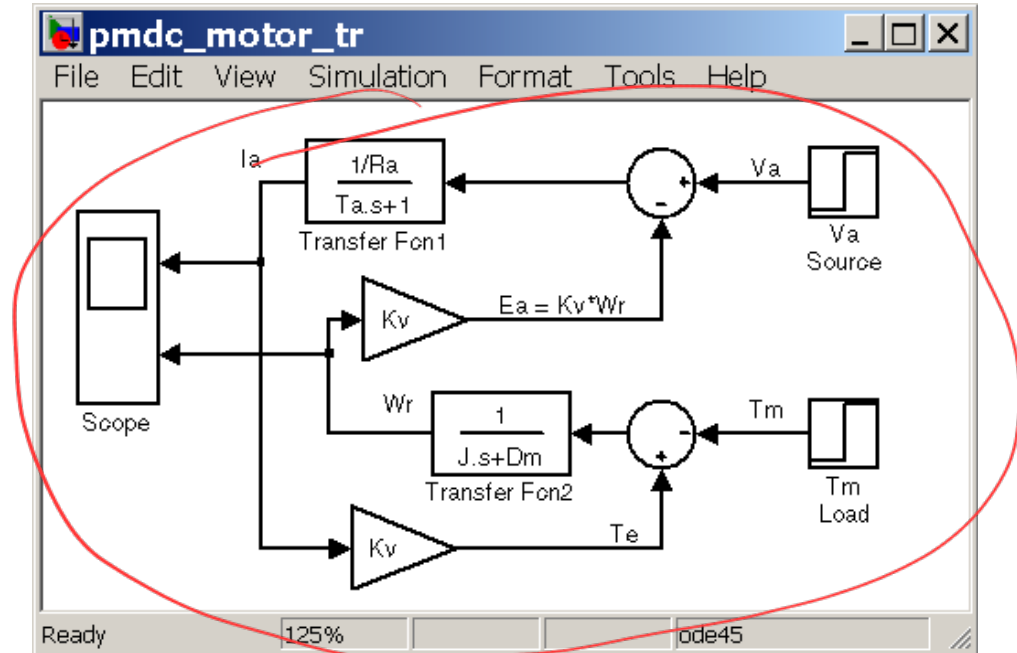
$$T_e - T_m = (D_m + Js) \omega_r$$

$$T_e = k_v i_a$$

Define time constant

$$\tau_a = \frac{L_a}{r_a}$$

Simulink Model of a PM DC Motor



$$i_a = \frac{1}{r_a(1 + \tau_a s)}(v_a - e_a)$$

$$e_a = k_v \omega_r$$

$$\omega_r = \frac{1}{D_m + Js}(T_e - T_m)$$

$$T_e = k_v i_a$$

State equation:

$$\frac{d}{dt} \begin{bmatrix} i_a \\ \omega_r \end{bmatrix} = \underbrace{\begin{bmatrix} -\frac{r_a}{L_a} & -\frac{k_v}{L_a} \\ \frac{k_v}{J} & -\frac{D_m}{J} \end{bmatrix}}_A \underbrace{\begin{bmatrix} i_a \\ \omega_r \end{bmatrix}}_x + \underbrace{\begin{bmatrix} \frac{1}{L_a} & 0 \\ 0 & -\frac{1}{J} \end{bmatrix}}_B \underbrace{\begin{bmatrix} v_a \\ T_m \end{bmatrix}}_u$$

Output equation: $y = Cx + Du$

$$\underbrace{\begin{bmatrix} i_a \\ \omega_r \\ T_e \end{bmatrix}}_y = \underbrace{\begin{bmatrix} 1 & 0 \\ 0 & 1 \\ k_v & 0 \end{bmatrix}}_C \underbrace{\begin{bmatrix} i_a \\ \omega_r \end{bmatrix}}_x + \underbrace{\begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}}_D \underbrace{\begin{bmatrix} v_a \\ T_m \end{bmatrix}}_u$$

Dynamic Response of a 6V PM DC Motor

Example: Motor parameters:

$V_a = 6\text{ V}$, $R_a = 7\ \Omega$, $L_a = 120\text{ mH}$, $K_v = 0.0141\text{ N}\cdot\text{A}/\text{m}$, $J = 1.06\text{e-}6\text{ kg}\cdot\text{m}^2$, $D_m = 6.01\text{e-}6\text{ N}\cdot\text{m}\cdot\text{s}$, $T_m = 3.53\text{e-}3\text{ N}\cdot\text{m}$

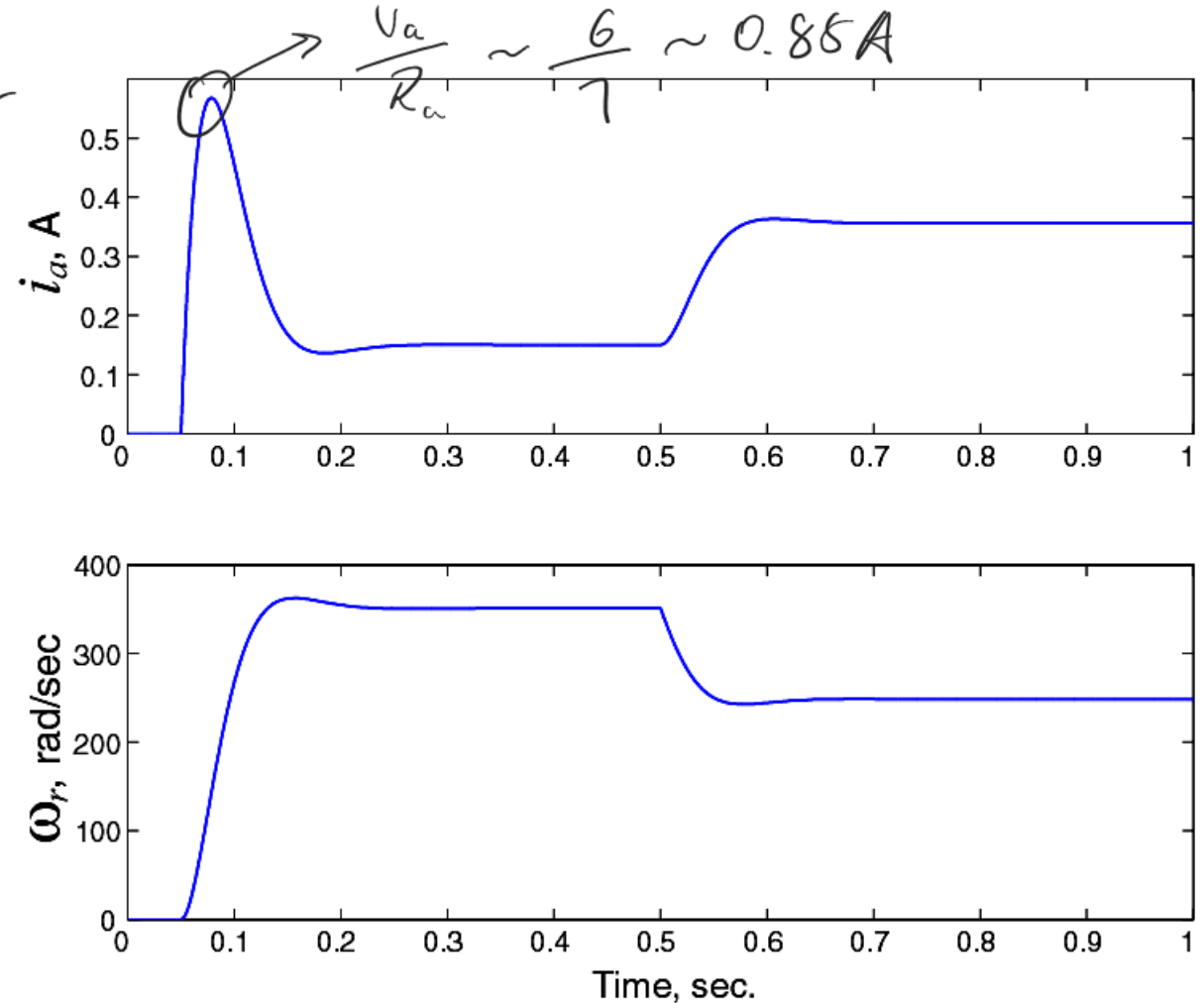
In this computer study:

Zero initial conditions assumed

Step-1: voltage is applied

Step-2: load torque is applied

Understand
Simulink files
↓
need for Lab 3
and Hwk 4



Example 1

SP3.3-1 When a 12-V, permanent-magnet dc motor is driven at 100 rad/s , the open-circuit voltage is 10 V. Calculate k_v . [$k_v = 0.1 \text{ V} \cdot \text{s/rad}$]



$$i_a = 0 \text{ A}$$

$$V_a = i_a R_a + E_a$$

$$V_a = E_a = k_v \omega_r$$

$$k_v = \frac{V_a}{\omega_r} = \frac{10 \text{ V}}{100 \text{ rad/s}} = 0.1 \text{ V} \cdot \text{s/rad}$$

$$k_v = k_t$$

Example 2

SP3.3-3 Calculate the no-load speed ($T_L = 0$) for the permanent-magnet dc motor in SP3.3-1 when rated voltage (12 V) is applied to the armature. $[\omega_r = 120 \text{ rad/s}]$

$$k_v = k_t = 0.1$$

$$V_a = i_a R_a + E_a = i_a R_a + k_v \omega_r, \quad T_e = 0 = k_t i_a \Rightarrow i_a = 0$$

$$V_a = k_v \omega_r$$

$$12 \text{ V} = 0.1 \omega_r \Rightarrow \boxed{\omega_r = 120 \text{ rad/s}}$$

Example 3

SP3.4-1 A 12-V, permanent-magnet dc motor has an armature resistance of $12\ \Omega$ and $k_v = 0.01\ \text{V} \cdot \text{s}/\text{rad}$. Calculate the steady-state stall torque (T_e with $\omega_r = 0$). [$T_e = 0.01\ \text{N} \cdot \text{m}$]

$k_v = 0.01\ \text{V}/\text{rpm} \rightarrow$ needs conversion to $\text{V} \cdot \text{s}/\text{rad}$

$\downarrow$
 $E_a = k_v \omega_r = 0\ \text{V}$

$$V_a = R_a i_a + \cancel{E_a}^0 \Rightarrow 12\ \text{V} = 12\ \Omega \cdot i_a \Rightarrow i_a = 1\ \text{A}$$

$$T_e = k_t i_a = 0.01 \cdot 1 = 0.01\ \text{N} \cdot \text{m}$$

$\downarrow$
 $k_t = k_v$

$\left\{ \begin{array}{l} \text{DC generator} = \\ \text{DC motor} = \end{array} \right.$

$$V_a + R_a i_a = E_a$$

$$V_a = R_a i_a + E_a$$

Example 4

A permanent magnet dc motor drives a mechanical load requiring a constant torque of $25 \text{ N} \cdot \text{m}$. The motor produces $10 \text{ N} \cdot \text{m}$ with an armature current of 10 A . The resistance of the armature circuit is 0.2Ω . A 200 V dc supply is applied to the armature terminals. Determine the speed of the motor.

Hint at k_t : $T_e = k_t i_a \Rightarrow 10 \text{ N} \cdot \text{m} = k_t \cdot 10 \text{ A} \Rightarrow \underline{k_t = 1 \text{ V} \cdot \text{s} / \text{rad}}$

$$R_a = 0.2 \Omega$$

$$V_a = 200 \text{ V}$$

$$T_m = T_e = \underline{25 \text{ N} \cdot \text{m}} \quad (\text{ignore friction})$$

$$\omega_r = ?$$

$$\hookrightarrow \underline{E_a} = \underline{k_v} \cdot \omega_r$$

$$\textcircled{1} \quad i_a = \frac{T_e}{k_t} = \frac{25 \text{ N} \cdot \text{m}}{1} = 25 \text{ A}$$

$$\textcircled{2} \quad V_a = R_a i_a + E_a$$
$$200 \text{ V} = 0.2 \cdot 25 \text{ A} + k_v \cdot \omega_r$$

$$\omega_r = \frac{200 - 0.2 \times 25}{1}$$
$$= 195 \text{ rad/s}$$

Example 5

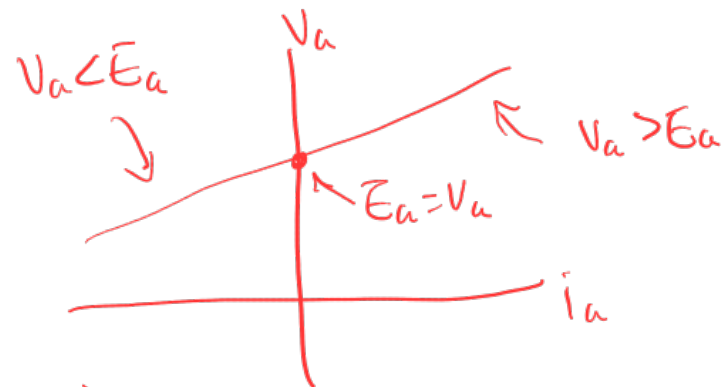
A dc machine is connected across a 240-volt line. It rotates at 1200 rpm and is generating 230 volts. The armature current is 40 amps.

Handwritten notes above the text:
- E_a (pointing to 230 volts)
- V_a (pointing to 240-volt)
- I_a (pointing to 40 amps)
- W_r (pointing to 1200 rpm, with note "needs conversion")

- (a) Is the machine functioning as a generator or as a motor?
- (b) Determine the resistance of the armature circuit. $\rightarrow R_a$
- (c) Determine power loss in the armature circuit resistance and the electromagnetic power.
 $\rightarrow P_e$
 $\hookrightarrow \frac{V^2}{R} \rightarrow I^2 R$
- (d) Determine the electromagnetic torque in newton-meters.
 $\rightarrow T_e$
- (e) If the load is thrown off, what will the generated voltage and the rpm of the machine be

Example 5

(a) $V_a = 240\text{V}$, $E_a = 230\text{V}$, $I_a = 40\text{A}$, $\omega_r = 1200\text{ rpm}$



$V_a > E_a \Rightarrow \text{motoring}$

(b) $V_a = R_a I_a + E_a$ (motoring) $\Rightarrow 240 = R_a \cdot 40 + 230 \Rightarrow R_a = 0.25\ \Omega$

(c) Power loss: $R_a I_a^2 = 40^2 \times 0.25 = 400\text{W}$

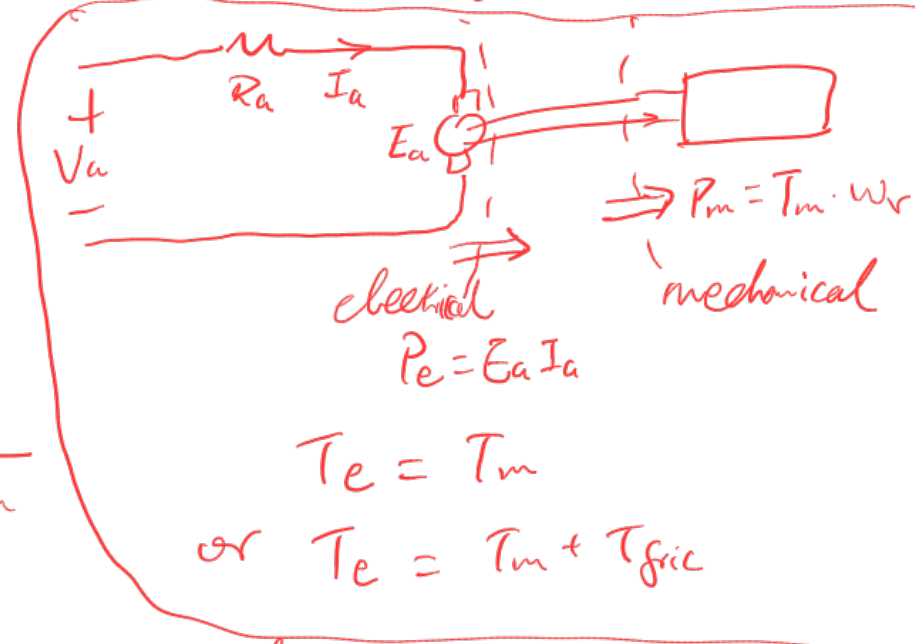
$P_e = E_a \cdot I_a = 230\text{V} \times 40\text{A} = 9200\text{W}$

(d) $T_e = \frac{P_e}{\omega_r} = \frac{9200\text{W}}{125.7} = 73.19\text{ N}\cdot\text{m}$

$\omega_r = 1200 \frac{\text{rev}}{\text{min}}$
 $= \frac{1200}{60 \text{ sec/min}} \times \frac{2\pi \text{ rad}}{\text{rev}}$

$= \frac{1200}{60} \times 2\pi = 125.7 \text{ rad/sec}$

(e) You need k_t



Looking ahead...

- Start **Module 5**