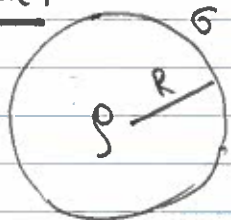


Problem 1


$$E_{out} \equiv 0.$$

$$a) |\vec{G}| \cdot 4\pi R^2 = \rho \cdot \frac{4\pi}{3} R^3 \rightarrow \boxed{\vec{G} = -\frac{\rho R}{3}}$$

$$b) \oint \vec{E} \cdot d\vec{A} = q_{enc}/\epsilon_0 \rightarrow$$

$$E_{in}(r) \cdot 4\pi r^2 = \frac{1}{\epsilon_0} \rho \cdot \frac{4\pi}{3} r^3 \rightarrow \boxed{E_{in}(r) = \frac{\rho r}{3\epsilon_0}}$$

$$\boxed{E_{out}(r) = 0} \quad - \text{given}$$

$$\Delta V = - \int_i^f \vec{E} \cdot d\vec{e} \rightarrow$$

$$\boxed{V_{out}(r) = 0}$$

Since $V_{\infty} = 0$
and $\vec{E}_{out} = 0$

$$\rightarrow V(R) = 0$$

$$V(R) - V_{in}(r) = - \int_r^R E_{in}(r) \cdot dr \rightarrow$$

$$V_{in}(r) = \int_r^R \frac{\rho r}{3\epsilon_0} dr = \frac{\rho}{3\epsilon_0} \frac{r^2}{2} \Big|_r^R \rightarrow V_{in}(r)$$

$$\boxed{V_{in}(r) = \frac{\rho}{6\epsilon_0} (R^2 - r^2)}$$

$$c) \text{ Way 1: } W = \frac{1}{2} \int \rho(r) V(r) d\tau =$$

$$= \frac{1}{2} \cdot 4\pi \int_0^R r^2 dr \cdot \rho \cdot \frac{\rho}{6\epsilon_0} (R^2 - r^2) =$$

$$= \frac{\pi \rho^2}{3\epsilon_0} \left(R^2 \frac{r^3}{3} \Big|_0^R - \frac{r^5}{5} \Big|_0^R \right) = \frac{\pi \rho^2}{3\epsilon_0} R^5 \left(\frac{1}{3} - \frac{1}{5} \right) =$$

$$= \frac{\pi \rho^2 R^5}{3\epsilon_0} \frac{2}{15} \rightarrow \boxed{W = \frac{2\pi \rho^2 R^5}{45\epsilon_0}}$$

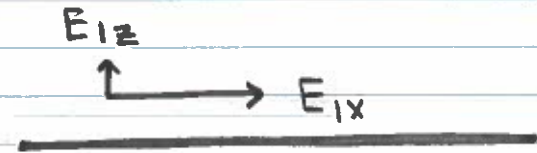
Way 2: $W = \frac{\epsilon_0}{2} \int E_{in}^2 d\tau =$

$$= \frac{\epsilon_0}{2} \cdot 4\pi \cdot \int_0^R r^2 dr \cdot \frac{\rho^2 r^2}{9\epsilon_0^2} = \frac{2\pi}{9\epsilon_0} \rho^2 \frac{r^5}{5} \Big|_0^R \rightarrow$$

$$\boxed{W = \frac{2\pi \rho^2 R^5}{45\epsilon_0}}$$

d) It does not include σ explicitly, since $V(r=R)=0$ and $\rho V=0$. However, the presence of σ is what makes $V(r>R) \equiv 0$, (if you use $W = \frac{1}{2} \int \rho V d\tau$) and $\vec{E}(r>R) \equiv 0$ (if you use $W = \frac{\epsilon_0}{2} \int E^2 d\tau$). Hence, σ does play a role in this calculation by reducing the integral to the volume of the sphere.

Problem 2.



$$a) \quad D_{1z} - D_{2z} = \sigma_f = 0 \rightarrow \boxed{\sigma_f = 0}$$

$$b) \quad E_{1x} = E_{2x} \rightarrow \frac{D_{1x}}{\epsilon_1} = \frac{D_{2x}}{\epsilon_2} \rightarrow$$

$$\epsilon_1 = \epsilon_2 \frac{D_{1x}}{D_{2x}} = \epsilon_2 \frac{3}{2} = 2\epsilon_0 \frac{3}{2} \rightarrow \boxed{\epsilon_1 = 3\epsilon_0}$$

$$c) \quad E_{1x} = E_{2x}; \quad D_{1z} = D_{2z} \rightarrow \epsilon_1 E_{1z} = \epsilon_2 E_{2z} \rightarrow$$

$$E_{1z} = E_{2z} \frac{\epsilon_2}{\epsilon_1} = E_{2z} \frac{2\epsilon_0}{3\epsilon_0} = \frac{2}{3} E_{2z}$$

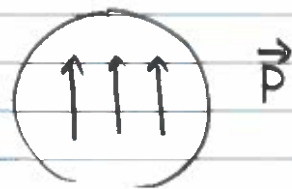
$$d) \quad E_{1z} - E_{2z} = \frac{\sigma}{\epsilon_0} = \frac{\sigma_b}{\epsilon_0} \quad (\text{since } \sigma_f = 0 \text{ from a)})$$

$$\sigma_b = \epsilon_0 (E_{1z} - E_{2z}) = \epsilon_0 \left(\frac{2}{3} E_{2z} - E_{2z} \right) = -\epsilon_0 \frac{E_{2z}}{3}$$

$$\boxed{\sigma_b = -\epsilon_0 E_0}$$

$$e) \quad \boxed{\rho_{b1} = \rho_{b2} = 0} \quad (\text{uniform linear dielectric})$$

Problem 3 $\vec{P} = P_0 \hat{z}$



a) $\rho_b = -\nabla \cdot \vec{P} = 0 \rightarrow \boxed{\rho_b = 0}$

$$\sigma_b = \vec{P} \cdot \hat{r} = P_0 \cdot \hat{z} \cdot \hat{r} = \boxed{P_0 \cos \theta = \sigma_b}$$

b) We will find $V(r)$ from the Laplace equation:

$$\nabla^2 V_{in}(r) = \nabla^2 V_{out}(r) = 0.$$

Boundary conditions:

(1) $V_{in}(r=0) = \text{finite}$ (2) $V_{out}(r=\infty) = \text{finite}$

(3) $V_{in}(r=R) = V_{out}(r=R)$ (V continuous)

(4) $-\left(\frac{\partial V_{out}}{\partial r}\right)_R - \left(-\frac{\partial V_{in}}{\partial r}\right)_R = \frac{\sigma_b}{\epsilon_0} \quad \left(\Delta E_{\perp} = \frac{\sigma}{\epsilon_0}\right)$

General form of $V(r)$:

$$V_{in}(r) = \sum_{l=0}^{\infty} \left(A_l^{in} r^l + \cancel{\frac{B_l^{in}}{r^{l+1}}} \right) P_l(\cos \theta)$$

$$V_{out}(r) = \sum_{l=0}^{\infty} \left(\cancel{A_l^{out} r^l} + \frac{B_l^{out}}{r^{l+1}} \right) P_l(\cos \theta)$$

$B_l^{in} \equiv 0$ from (1), $A_l^{out} \equiv 0$ from (2).

$$(3): \sum_{l=0}^{\infty} A_l^{\text{in}} R^l P_l(\cos\theta) = \sum_{l=0}^{\infty} \frac{B_l^{\text{out}}}{R^{l+1}} P_l(\cos\theta)$$

From orthogonality of $P_l(\cos\theta)$:

$$A_l^{\text{in}} R^l = \frac{B_l^{\text{out}}}{R^{l+1}} \rightarrow B_l^{\text{out}} = A_l^{\text{in}} \cdot R^{2l+1}$$

$$\begin{aligned} (4): \sum_{l=0}^{\infty} \left(l R^{l-1} A_l^{\text{in}} - B_l^{\text{out}} \frac{d}{dr} r^{-(l+1)} \Big|_R \right) P_l(\cos\theta) &= \\ &= \sum_{l=0}^{\infty} \left(l R^{l-1} A_l^{\text{in}} + A_l^{\text{in}} R^{2l+1} (l+1) \frac{1}{R^{l+2}} \right) P_l(\cos\theta) = \\ &= \sum_{l=0}^{\infty} A_l^{\text{in}} R^{l-1} (2l+1) \cdot P_l(\cos\theta) = \frac{P_0}{\epsilon_0} \cdot P_1(\cos\theta) \end{aligned}$$

From orthogonality of $P_l(\cos\theta)$:

$$A_1^{\text{in}} \cdot 3 = \frac{P_0}{\epsilon_0} \rightarrow \boxed{A_1^{\text{in}} = \frac{P_0}{3\epsilon_0}, \quad A_{l \neq 1}^{\text{in}} = 0}$$

$$\boxed{B_1^{\text{out}} = \frac{P_0}{3\epsilon_0} \cdot R^3, \quad B_{l \neq 1}^{\text{out}} = 0}$$

$$\boxed{\begin{aligned} V_{\text{in}}(r) &= \frac{P_0}{3\epsilon_0} r \cos\theta = \frac{P_0 z}{3\epsilon_0} \\ V_{\text{out}}(r) &= \frac{P_0}{3\epsilon_0} \frac{R^3}{r^2} \cos\theta \end{aligned}}$$

$$\vec{E} = -\nabla V = -\frac{\partial V}{\partial z} \hat{z} = -\frac{\partial V}{\partial r} \hat{r} - \frac{1}{r} \frac{\partial V}{\partial \theta} \hat{\theta}$$

$$\vec{E}_{in}(\vec{r}) = -\frac{P_0}{3\epsilon_0} \cos\theta \hat{r} + \frac{P_0}{3\epsilon_0} \sin\theta \hat{\theta} = -\frac{P_0}{3\epsilon_0} \hat{z}$$

$$\vec{E}_{out}(\vec{r}) = \frac{2P_0}{3\epsilon_0} \frac{R^3}{r^3} \cos\theta \hat{r} + \frac{P_0}{3\epsilon_0} \frac{R^3}{r^3} \sin\theta \hat{\theta}$$

$$\vec{D}_{out} = \epsilon_0 \vec{E}_{out};$$

$$\vec{D}_{in} = \epsilon_0 \vec{E}_{in} + \vec{P}_{in} = -\frac{P_0}{3} \hat{z} + P_0 \hat{z} \rightarrow$$

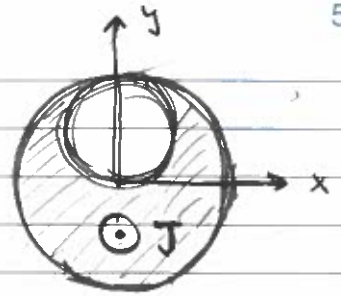
$$\vec{D}_{in} = \frac{2P_0}{3} \hat{z} = \frac{2P_0}{3} (\cos\theta \hat{r} - \sin\theta \hat{\theta})$$

$$\vec{D}_{out} = \frac{P_0}{3} \frac{R^3}{r^3} (2\cos\theta \hat{r} + \sin\theta \hat{\theta})$$

c) $Q_{net} = 0 \rightarrow$ no monopole $\rightarrow$

the leading term will be a dipole

It does not depend on the choice of coordinate system since $Q_{net} = 0$.

Problem 4.

Strategy: $\vec{B}_{\text{hole}} = \vec{B}_1 + \vec{B}_2 =$

superposition of $\vec{B}_1$ due to a whole cylinder with $\vec{B}_2$ due to a smaller cylinder with current in the opposite direction.

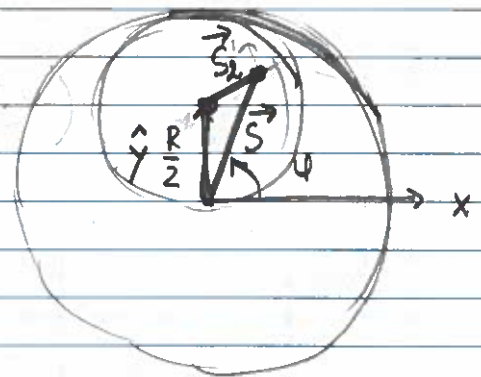
Calculation: $B_{\text{cyl}} = ?$ Way 1:

$$B_{\text{in}}(s) \cdot 2\pi s = \mu_0 I_{\text{encl}} = \mu_0 \cdot J \cdot \pi s^2 \rightarrow$$

$$\vec{B}_1(s) = \frac{\mu_0 J s}{2} \hat{\psi}$$

$$\vec{B}_2(s_2) = -\frac{\mu_0 J s_2}{2} \hat{\psi}_2 =$$

$$= -\frac{\mu_0 J}{2} \left(s \hat{\psi} + \frac{R}{2} \hat{x} \right)$$



$$\frac{R}{2} \hat{y} + \vec{S}_2 = \vec{S}$$

$$\vec{B}_{\text{hole}} = \frac{\mu_0 J}{2} \left(s \hat{\psi} - s \hat{\psi} - \frac{R}{2} \hat{x} \right)$$

$$\hat{\psi}_2 = \hat{z} \times \hat{S}_2 =$$

$$= \frac{\hat{z} \times (\vec{S} - R/2 \hat{y})}{S_2} \rightarrow$$

$$\vec{B}_{\text{hole}} = -\frac{\mu_0 J R}{4} \hat{x}$$

$$S_2 \hat{\psi}_2 = S \cdot \hat{\psi} + R/2 \hat{x}$$

Way 2: $\hat{\psi} = -\sin \psi \hat{x} + \cos \psi \hat{y}$

$$\vec{B}_1 = \frac{\mu_0 J S}{2} (-\sin \psi \hat{x} + \cos \psi \hat{y}) =$$

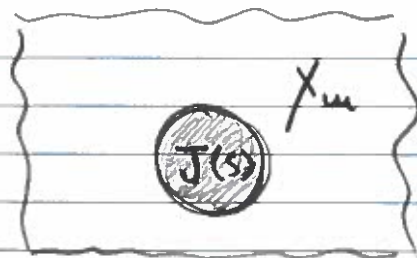
$$= \frac{\mu_0 J}{2} (-y \hat{x} + x \hat{y})$$

$$\vec{B}_2 = -\frac{\mu_0 J}{2} (-y_2 \hat{x} + x_2 \hat{y}) = \begin{cases} x_2 = x \\ y_2 = y - R/2 \end{cases}$$

$$= -\frac{\mu_0 J}{2} (-(y - R/2) \hat{x} + x \hat{y}) =$$

$$= \frac{\mu_0 J}{2} ((y - R/2) \hat{x} - x \hat{y})$$

$$\vec{B}_{\text{hole}} = \vec{B}_1 + \vec{B}_2 = \boxed{-\frac{\mu_0 J R}{4} \hat{x} = \vec{B}_{\text{hole}}}$$

Problem 5.

$$a) \oint \vec{H} \cdot d\vec{e} = \mu_0 I_{f, \text{encl}}$$

$$H \cdot 2\pi s = \mu_0 \int_{\text{loop area}} J(s') da' = \mu_0 \cdot 2\pi \cdot \int_0^s ds' \cdot s' \cdot J(s')$$

$$\vec{H}_w = \frac{1}{s} \int_0^s ds' \cdot s' \cdot J(s') \cdot \hat{\varphi}$$

$$B_w = \mu_0 H_w$$

$$\vec{H}_m = \frac{1}{s} \int_0^R ds' \cdot s' \cdot J(s') \cdot \hat{\varphi}$$

$$B_m = \mu_0 (1 + \chi_m) H_m$$

$$\vec{B}_w = \frac{\mu_0}{s} \int_0^s ds' \cdot s' \cdot J(s') \hat{\varphi}$$

$$\vec{B}_m = \frac{\mu_0 (1 + \chi_m)}{s} \int_0^R ds' \cdot s' \cdot J(s') \hat{\varphi}$$

$$b) \vec{J}_b = \nabla \times \vec{M} = \chi_m \nabla \times \vec{H}_m =$$

$$= \chi_m \cdot \frac{1}{s} \frac{\partial}{\partial s} (s \cdot H_{m, \varphi}) = \chi_m \cdot \frac{1}{s} \frac{\partial}{\partial s} (\text{const})$$

$$\boxed{\vec{J}_b = 0}$$

$$\vec{K}_b = \vec{M} \times \hat{n} = \chi_m \vec{H}_m \times (-\hat{S}) = \quad \rightarrow -\hat{z}$$

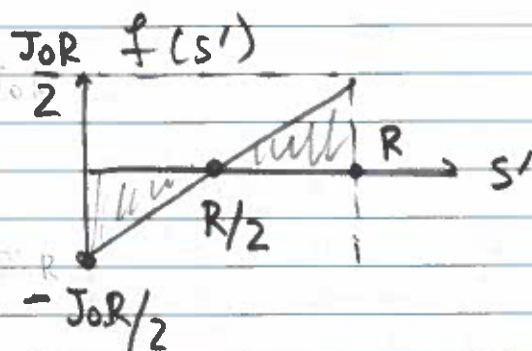
$$= -\chi_m \frac{1}{S} \int_0^R ds' s' J(s') \cdot (\hat{\psi} \times \hat{S}) \Rightarrow$$

$$\vec{K}_b = \left(\frac{\chi_m}{R} \int_0^R ds' s' J(s') \right) \hat{z}$$

c) Yes! We need:

$$\int_0^R ds' s' J(s') = 0$$

$$s' J(s') \equiv f(s')$$



We can take: s

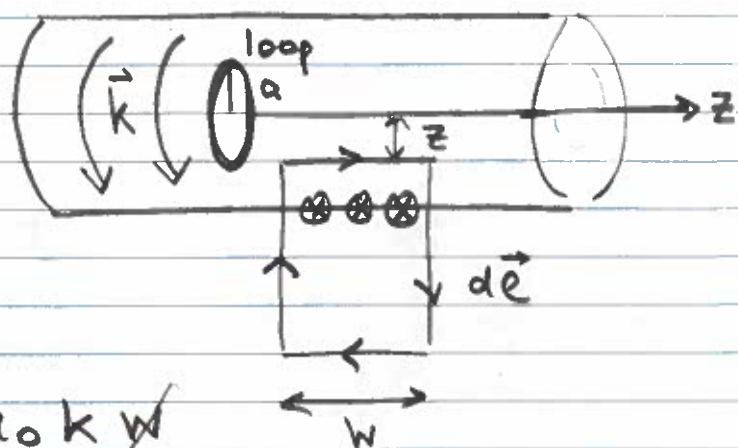
$$f(s') = s' J(s') = J_0 J_0 (s' - R/2) \rightarrow$$

$$J(s) = \frac{J_0 (s - R/2)}{s} \quad \text{would do the trick.}$$

Many other options are available!

Problem 6.

- a) By symmetry, inside the pipe $\vec{B} \parallel \vec{z}$



$$\oint_{\text{loop}} \vec{B} \cdot d\vec{\ell} = B(z) \cdot w = \mu_0 K w$$

$$\boxed{\vec{B}_{\text{pipe}} = \mu_0 K \cdot \hat{z}}$$

b) $\Phi_m = B \cdot A_{\text{loop}} = \boxed{\mu_0 K \pi a^2 = \Phi_m}$

c) $K(t) = K_0 e^{-t/\tau}$

$$\frac{d\Phi_m}{dt} = 0 \rightarrow K(t) a^2(t) = \text{const} =$$

$$= K_0 a_0^2 = K_0 e^{-t/\tau} \cdot a^2(t) \rightarrow$$

$$\boxed{a(t) = a_0 e^{-t/2\tau}}$$

d) $K(t) = K_0 \sin \omega t$, $a(t) = a_0 \sqrt{\cos \omega t}$

$$I_{\text{ind}} = -\frac{1}{R} \frac{d\Phi_m}{dt} = -\frac{\mu_0 \pi}{R} \frac{d}{dt} (\sin \omega t \cos \omega t) K_0 a_0^2$$

$$= -\frac{\mu_0 \pi}{2R} \cdot K_0 a_0^2 \frac{d}{dt} (\sin 2\omega t) =$$

$$= -\frac{\mu_0 \pi}{2R} \cdot 2\omega \cdot K_0 a_0^2 \cos 2\omega t$$

$$I_{\text{ind}} = -\frac{\mu_0 K_0 \omega \cdot \pi a_0^2}{R} \cos 2\omega t$$

